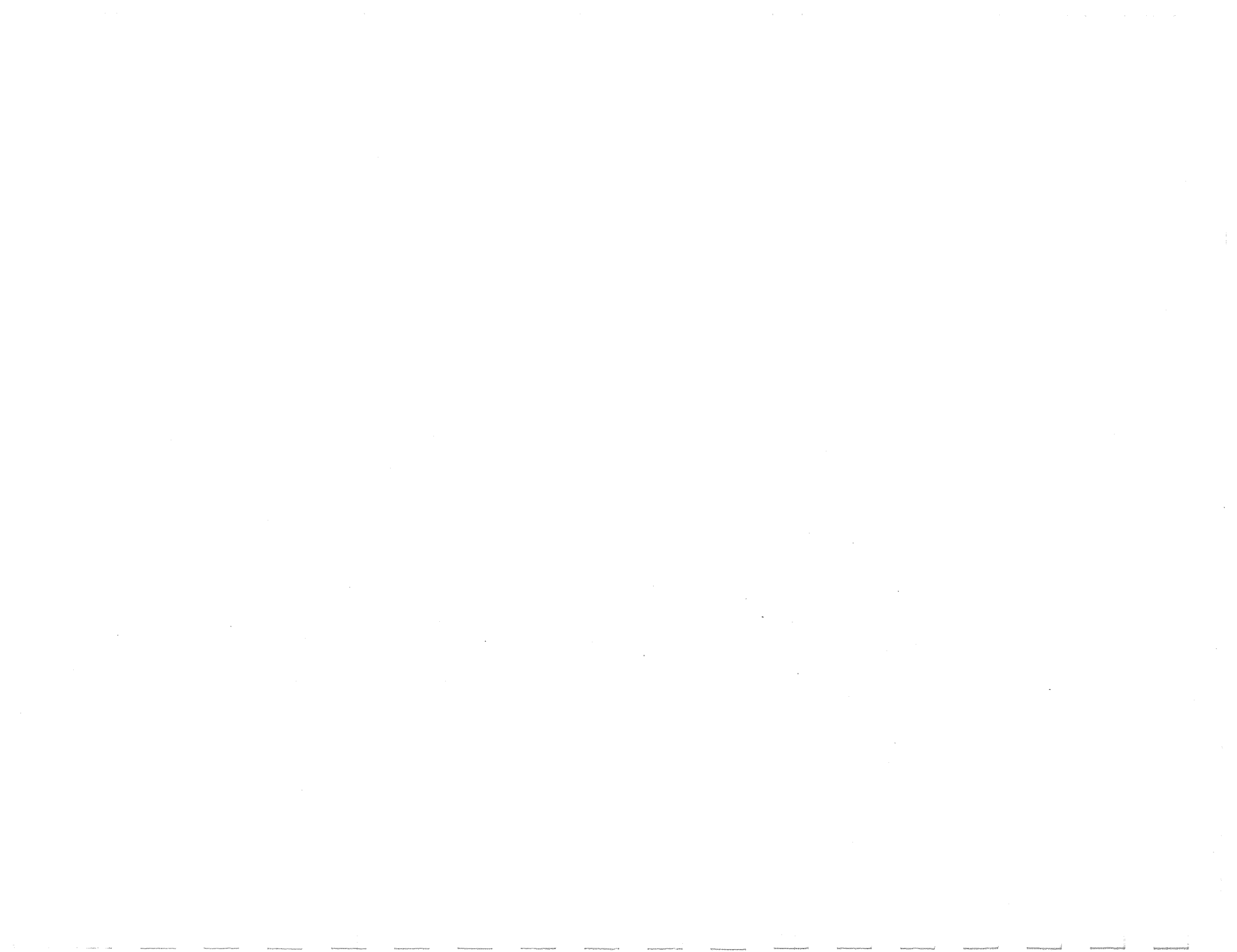


VOLUME I
DOCUMENTATION
FOR
THE VIRGINIA STATE CORPORATION COMMISSION'S
PRODUCTION COST SIMULATION MODEL

Prepared by
The National Regulatory Research Institute
The Ohio State University
Columbus, Ohio

October 1979



FOREWORD

This report was prepared for the Virginia State Corporation Commission. Any opinions expressed herein are solely those of the authors and do not necessarily reflect the opinions nor the policies of the National Regulatory Research Institute or the Virginia State Corporation Commission.

The NRRRI is making this report available to those concerned with state utility regulatory issues, since the subject matter presented here is believed to be of timely interest to regulatory agencies and to others concerned with utilities regulation.

The NRRRI appreciates the cooperation of the staff of the Virginia State Corporation Commission with the authors in preparing this study.

Dr. Douglas N. Jones
Director

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PREFACE

Pursuant to recent legislation (code of Virginia, Section 55-249.6) the staff of the Virginia State Corporation Commission (VSCC) has been developing a reporting and monitoring system in order to evaluate the fuel purchase costs and fuel usage practices of the electric utilities serving the Commonwealth of Virginia.

Part of the development of this system has been carried out under contract with The National Regulatory Research Institute (NRRI). A portion of the work performed by the Institute has been the development of a Production Cost Simulation (PCS) computer mode. This manual contains a description and the documentation for the PCS model.

The PCS model projects energy production by generating unit as a function of the unit's equivalent availability, capacity, loading position and the energy supply demands on the system. From the projected energy generation values parameters such as thermal energy consumption, fuel expense, average heat rate, capacity factor and average fuel expense are calculated for each unit and totaled or averaged for the system. The results of these calculations are reported on a monthly, quarterly and study period basis.

The documentation for the PCS model is provided in two volumes.

Volume I is divided into two sections. The first section gives a description of the model. It is designed to provide the reader with an overview of the model's calculation methodology and uses. The second section provides a detailed description of the programming aspects of the model. It is designed for the user and programmer. Volume II contains three of five appendices to this manual.

Further information about the model can be obtained from:

NRRI
2130 Neil Avenue
Columbus, Ohio 43210

ACKNOWLEDGEMENT

The developers of the PCS model wish to acknowledge the Virginia State Corporation Commission staff for their valuable assistance.

The support of Commissioners Preston C. Shannon, Junie L. Bradshaw and Thomas P. Harwood, Jr., is gratefully acknowledged.

PART I
DESCRIPTION OF THE PCS MODEL

Introduction

The PCS model is comprised of three separate operating modules. The main module, which is referred to as the PCS module, calculates the projected energy generation of each unit as a function of the unit's equivalent availability, capacity, dispatching order and the energy demands on the generating system. These factors as well as heat rate and fuel costs are provided as input to the module⁺. The other two modules are used to calculate input information for the PCS module. One module, DISPATCH, is a dispatching routine which develops a loading order for the generating system so as to minimize cost subject to a minimum load demand value and a spinning reserve margin constraint*. The other module, LOADPROB, is used to calculate a load probability curve from hourly load data.

Figure 1 shows the inputs and their sources for the PCS model and the outputs from the model. Contained in the balance of this section are descriptions of each module and the data files necessary to operate the model.

⁺ Contained within most production cost simulation models is the development of a dispatching order. The PCS module requires an input dispatching order. By separating the production projection from the dispatching calculation, the model is easier to use and less expensive to operate.

*The intent of the DISPATCH module is to provide the analyst with a first order dispatching sequence if the utility does not provide one or an alternative loading order.

INPUTS

FUEL COSTS

- provided by company
- developed independently

DISPATCHING ORDER

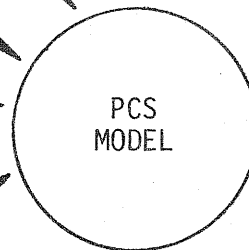
- provided by company
- calculated by DISPATCH
- developed independently

UNIT CHARACTERISTICS

- three-point heat rate curve
- capacity
- equivalent operating availabilities

LOAD DATA

- project load probability curve
- actual load probability curve calculated from hourly load by LOADPROB



OUTPUTS

BY UNIT

- generation
- thermal energy
- capacity factor
- average fuel cost per production unit
- average fuel cost per thermal input unit
- total fuel cost

BY FUEL TYPE

- total generation
- total thermal consumption
- average cost per output

SYSTEM

- reserve margin
- system reliability

FIGURE 1 PCS Inputs and Outputs

PCS Module

The PCS module can be viewed as having four major operation sections. They are the following:

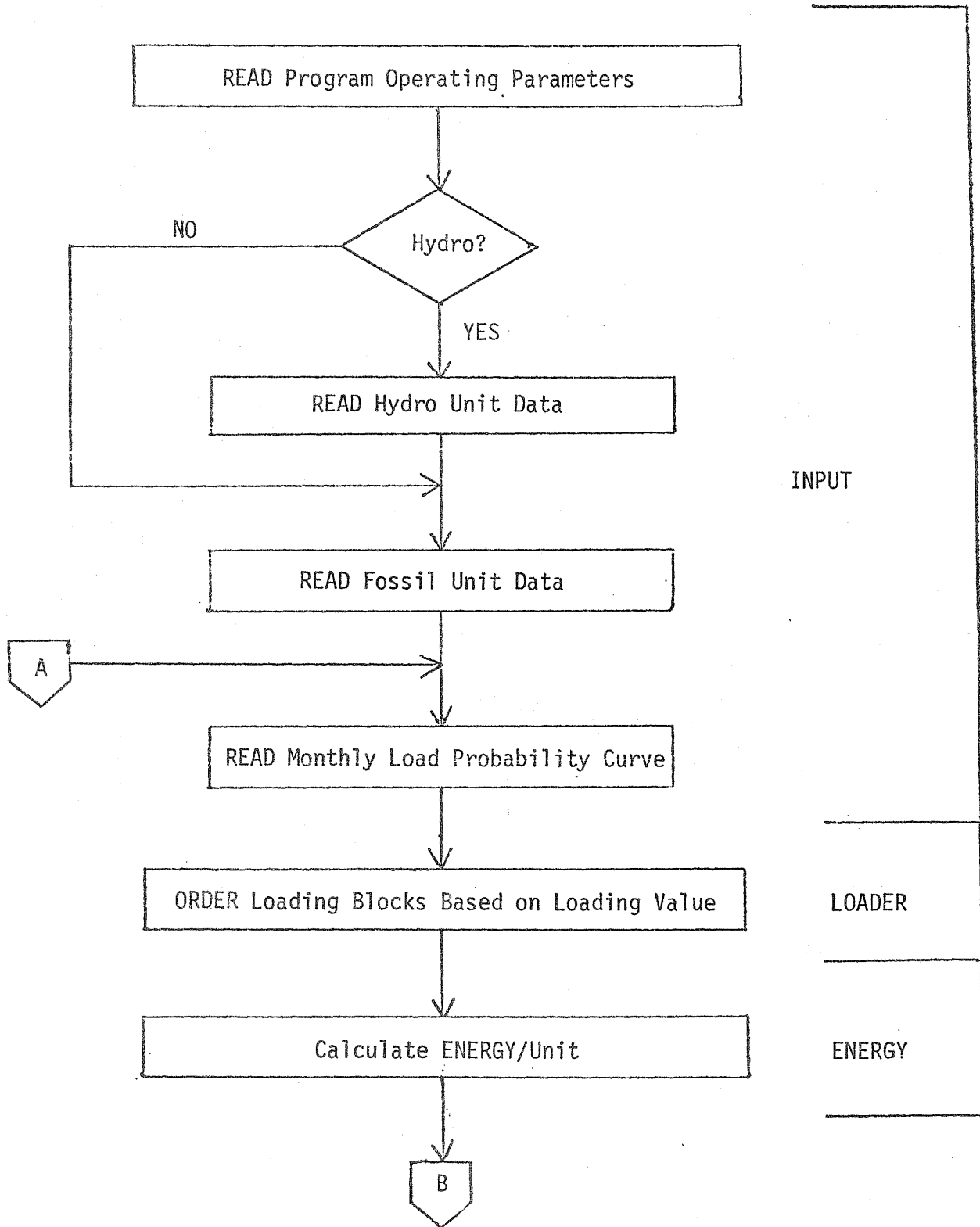
1. INPUT Section -- unit operational and fuel data and system load data are accessed by the program through this section.
2. LOADING Section - the dispatching order of the units is established in this section.
3. ENERGY Section - the projection calculation is performed in this section using a probabilistic technique which is described later in this text.
4. REPORT Section - the output from the model is reported on a monthly, quarterly and study period basis.

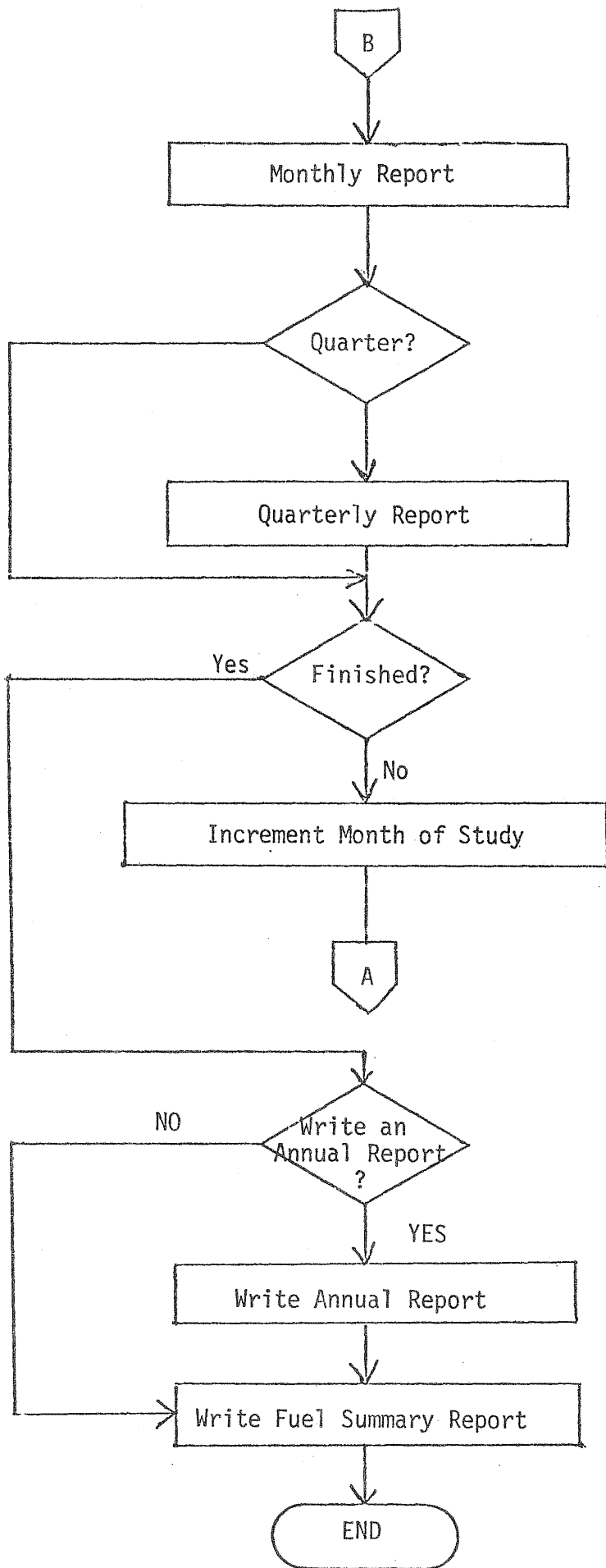
Figure 2 shows the generalized flow diagram of this module with the four operational sections identified.

The data necessary to operate the PCS model is organized into four groups. They are:

1. Unit Operational and Fuel Data for Fossil and Nuclear Units - this file contains unit operational data and fuel cost information data. The data are reported on a monthly basis.
2. Unit Operational Data for the Hydro Units - this file contains monthly capacity and projected generation for hydro units.
3. Load Data - the model requires monthly load data in the form of a load probability curve.

Figure 2: Flow Diagram of the PCS Module





REPORT

4. User Supplied Data - the model has operational options which the user chooses during execution.

INPUT Section

This section reads the operational and fuel data for each unit for the twelve months of the year. It then stores these values in the appropriate computer variable locations.

In order to calculate the energy generation of each unit the monthly load probability curve is entered into the program through this section.

The user specified operating parameters are also specified through this section.

LOADER Section

The LOADER section of the module orders the loading blocks of each unit by ascending dispatching number. The PCS model is designed to handle unit dispatching with up to three loading steps. That is, each unit can be dispatched in one, two or three loading steps. When a unit is single step dispatched it is put on line at full power. When it is dispatched in two steps it is first loaded to a minimum load capacity then to full capacity. Three step loading is accomplished by first dispatching the unit to a minimum capacity, then to an intermediate capacity and finally to full power.

In this section, the loading order of each generating unit is established. This is accomplished by the loading of each loading step based on an order determined externally to the model and supplied as input to the model as part of the unit operational and fuel data file. This allows the utility company to specify the expected loading order of the units. At times, placing higher cost units earlier in the loading order may better model physical constraints on the system such as environmental consideration.

The use of the DISPATCH module to establish a loading order is discussed in a later section.

ENERGY Section

The purpose of the ENERGY section is to calculate the expected megawatt-hour generation of each unit on line during the month. This calculation is the essence of the PCS model. Also calculated in ENERGY are the loss-of-load probability (LOLP) and the amount of expected energy that the generating system cannot supply to meet the demand.

The energy generated by each unit is calculated by the probabilistic simulation method, which is essentially the same as that developed by Booth⁺ and then adapted for use in the WASP program*, except that the load probability curves are expressed by piecewise linear functions rather than Fourier series. A simplified derivation of the calculation method follows.

The generating units of the utility being studied are dispatched to meet the required generation needs of the system as expressed by the load probability curve shown in Figure 3. Assume that the generating system under consideration has N units which are dispatched in one load step in order of their unit numbers to meet the energy demands on the system. Figure 4 illustrates this situation. Suppose, also, for illustrative purposes that each unit is available at all times during the study period.

⁺ Booth, R. R., "Power System Simulation Model Based on Probability Analysis," IEEE Trans. on Power Apparatus and Systems, Vol. PAS-91, No. 1, pp 62-69 (Jan.-Feb. 1972).

* Jenkins, R. T., and D. S. Joy, "Wien Atomic System Planning Package (WASP) - An Electric Utility Optimal Generation Expansion Planning Computer Code," ORNL 4945, Oak Ridge National Laboratory, Oak Ridge Tennessee, July 1974.

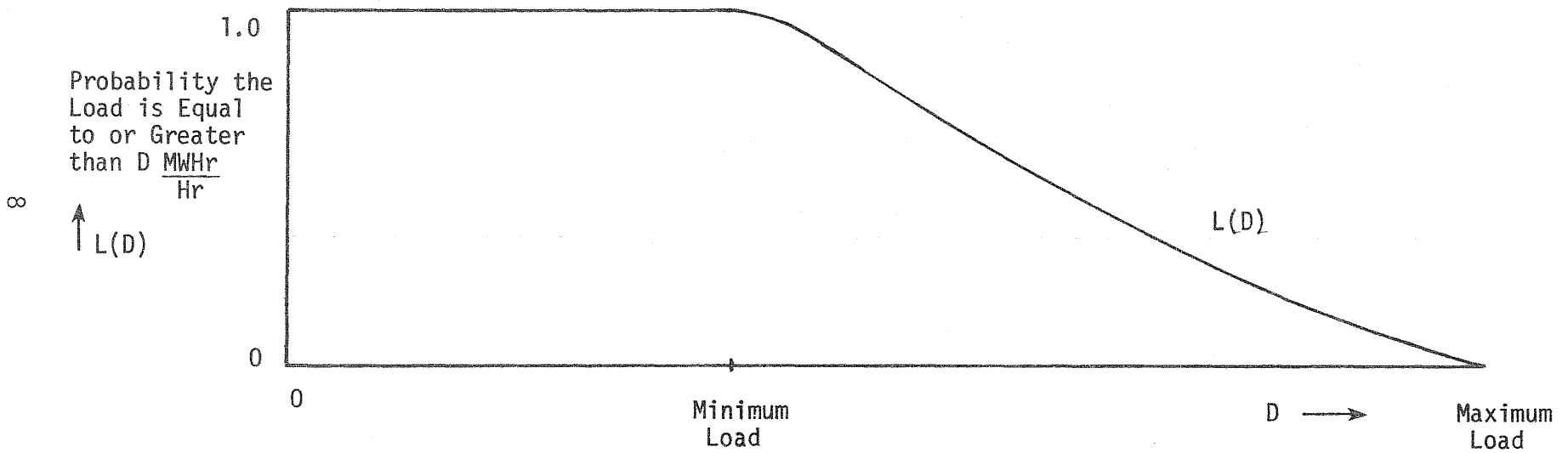


Figure 3 Load Probability Curve

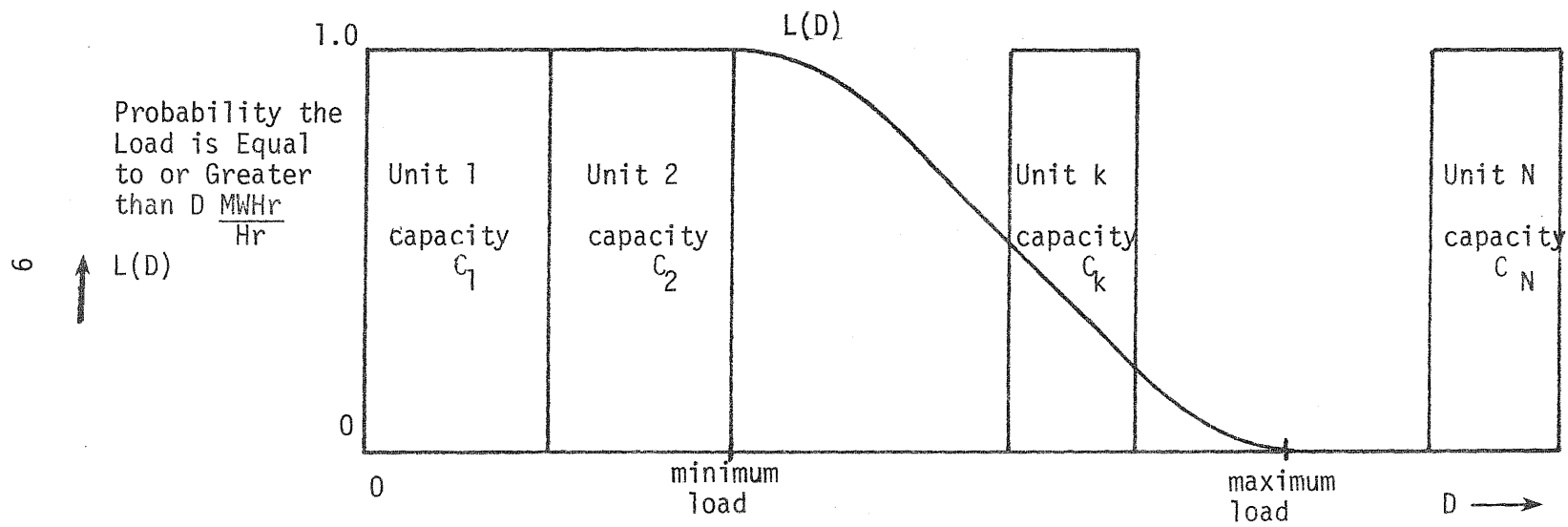


Figure 4 Load Probability Curve with Generating Units Dispatched to Meet the Load

The expected energy output of each unit is the area of intersection of the unit's location in the loading order and the load probability curve. Expressed in mathematical terms the expected energy generation of each unit is

$$ENG_k = T_p p_k \int_{\sum_{j=1}^{k-1} C_j}^{\sum_{j=1}^k C_j} L_o(D) dD \quad (1)$$

where p_k is the availability of the k^{th} unit (for this case $p_k=1.0$), ENG_k is the expected generation of the k^{th} unit, T_p is the number of the hours in the study period, and C_j is the megawatt capacity of the j^{th} unit in the loading order.

If all units in an operating system were available 100% of the time the calculation of expected generation would be straightforward and simple. However, units are available less than 100% during a study period. This effect must be accounted for.

Assume that the availability of Unit 1 becomes zero. Physically the other operating units would shift up (to the left) in the loading order to compensate for the lost generation from Unit 1. The expected generation of the remaining units, assuming a 100% availability, can be calculated using Equation 1 with the modification to the limits of integration based on the fact that Unit 1 is not available. Mathematically the unavailability of Unit 1 can be accounted for in two ways. The first involves removing Unit 1 from the loading order, then dispatching the

remaining units against the load probability curve. The second method is to shift the load probability curve to the right by the capacity of Unit 1. This is illustrated in Figure 5. The expected generation of the remaining units can be calculated by integrating the curve $L_0(D-C_1)$ over their loading range.

In reality all units have an availability range between zero and 100%. To account for this an equivalent load probability curve is defined which weights the percentage of time that a unit is on- and off-line. In the case of Unit 1 the equivalent load probability curve is defined by

$$L_1(D) = p_1 L_0(D) + (1-p_1) L_0(D-C_1) \quad (2)$$

where p_1 is the availability of Unit 1 expressed as a fraction, $L_0(D)$ is the original load probability curve, and $L_1(D)$ is the equivalent load probability curve which is created because of the unavailability of Unit 1. Figure 6 illustrates this curve.

The expected energy generation for Unit 2 is calculated using the equivalent load probability curve $L_1(D)$ in Equation 1.

The equivalent load probability curve, which expresses the effect of the absence of Unit 2 on the expected generation of units in the loading order after Unit 2, is

$$L_2(D) = p_2 L_1(D) + (1-p_2) L_1(D-C_2) \quad (3)$$

Equation 3 can be written in the general form which expresses the k^{th} equivalent load probability curve as

$$L_k(D) = p_k L_{k-1}(D) + (1-p_k) L_{k-1}(D-C_k) \quad (4)$$

The expected energy generation of the k^{th} units is the area of intersection of the k^{th} unit's position in the loading order with the $L_{k-1}(D)$

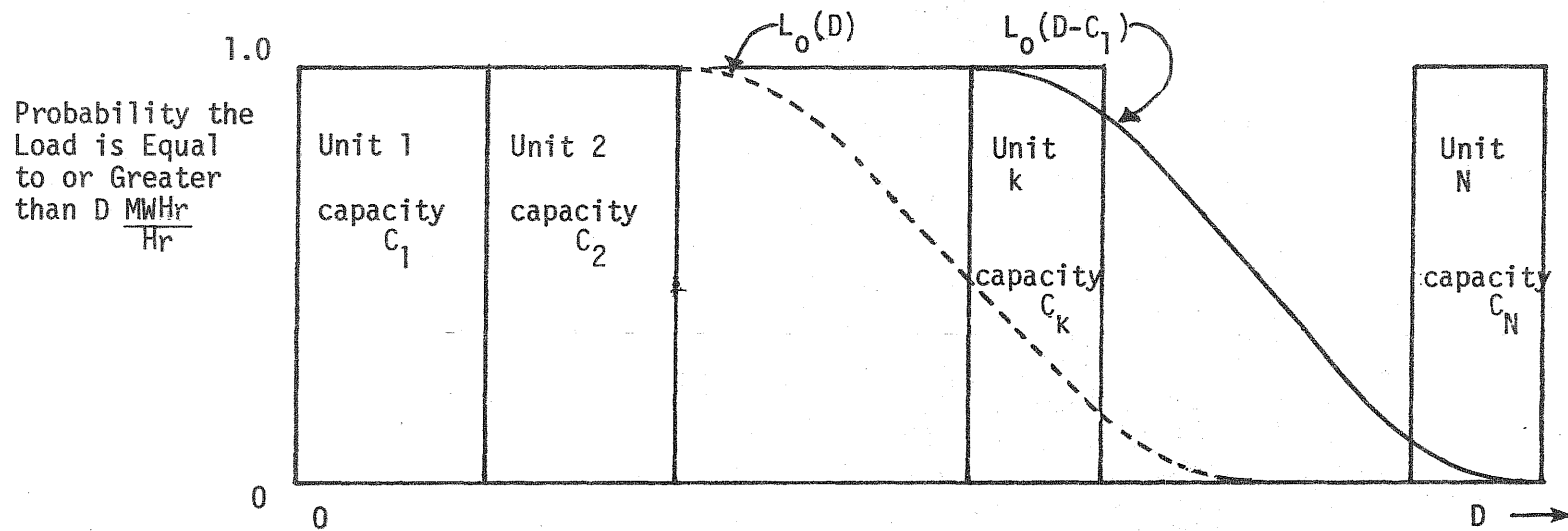


Figure 5 Load Probability Curve Shifted by the Capacity of Unit 1

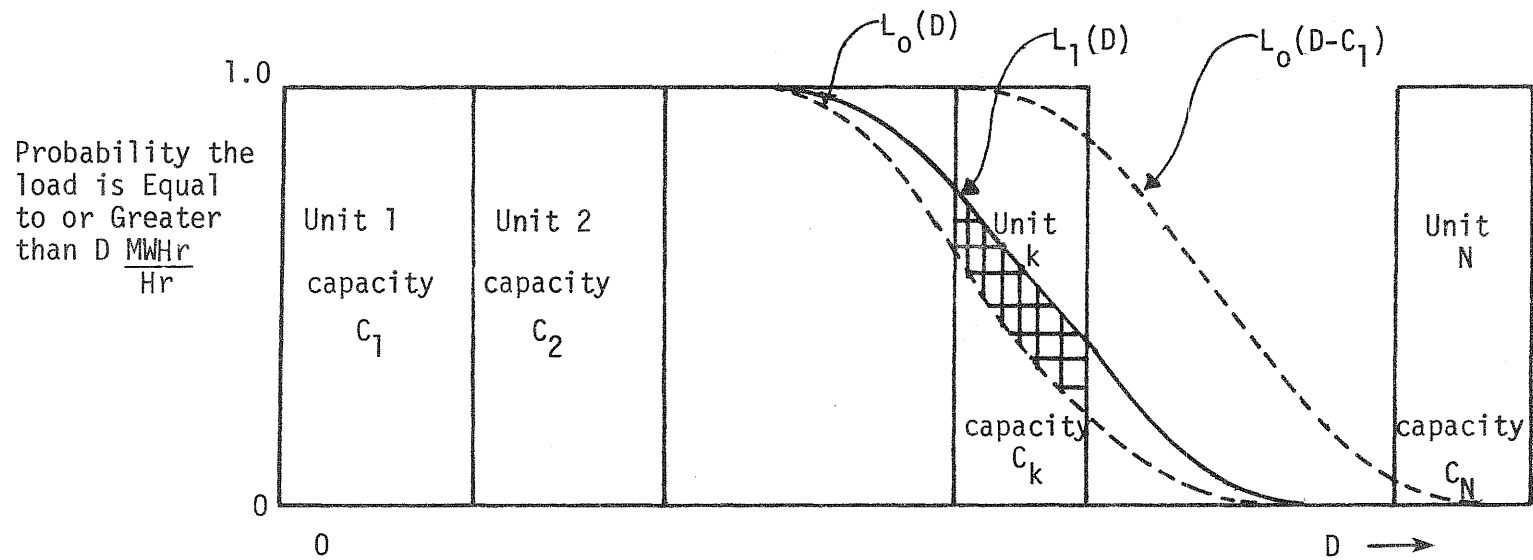


Figure 6 Equivalent Load Probability Curve

equivalent load probability curve times the availability of the k^{th} unit, P_k , and times the number of hours in the period. Expressed mathematically this is

$$ENG_k = T_p P_k \int_{\sum_{j=1}^{k-1} C_j}^{\sum_{j=1}^k C_j} L_{k-1}(D) dD \quad (5)$$

Using the equivalent load probability curve for the N^{th} unit, the amount of expected unserved energy and the loss-of-load probability are calculated as shown in Figure 7. The shaded area of the curve $L_N(D)$ is the area of the curve which does not intersect with any of the units in the generating system. This then is the energy which is to be supplied by the utility but cannot be supplied by the generating system. The loss-of-load probability is the value of $L_N(D)$ at D equal to system generating capacity.

The unserved energy can be calculated from

$$UNENG = T_p \int_{SYSCAP}^{\infty} L_N(D) dD \quad (6)$$

or more simply from

$$UNENG = T_p \int_0^{\infty} L_0(D) dD - \sum_{j=1}^N ENG_j \quad (7)$$

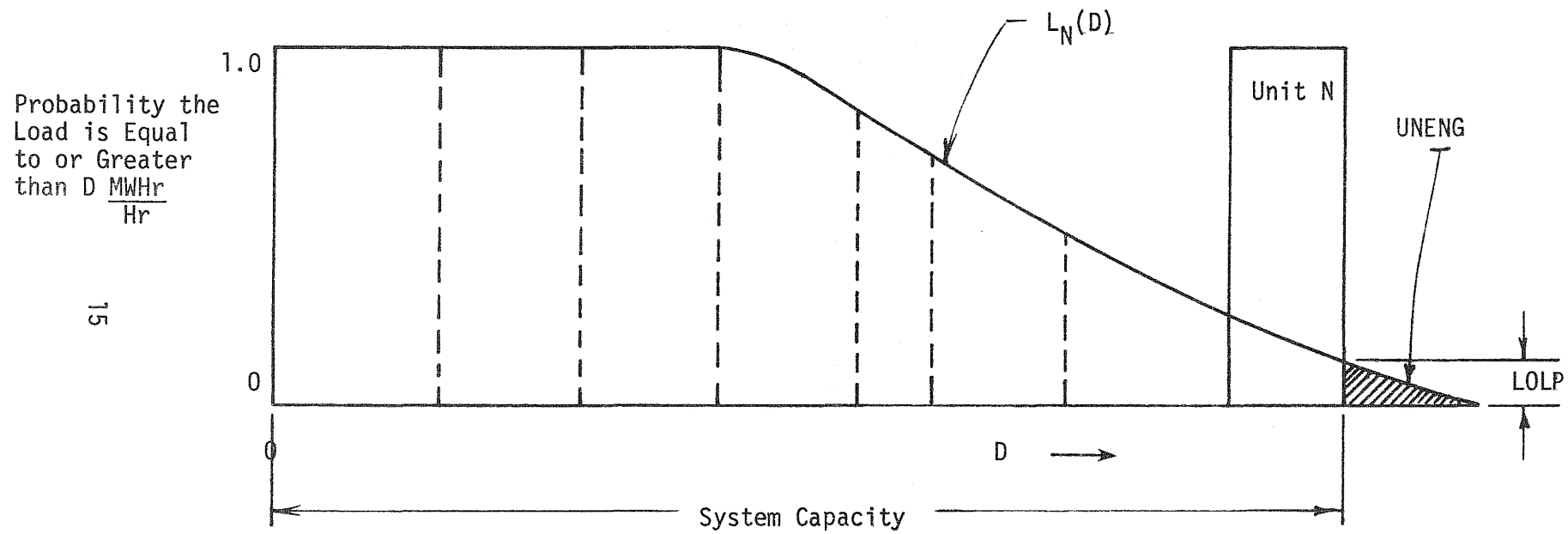


Figure 7 Unserved Energy and LOLP

Where the first term in Equation 7 is the total energy the system must supply and the second term is the total energy generated by the N generating units. The PCS model calculates unserved energy using Equation 7.

The above derivation lacks completeness in that each unit is dispatched in one load step. The method as presented can be applied to multiple loading steps if one assumes that the availability of any loading block is independent of any other block. In reality this is not the case. In order to model reality a deconvolution technique is utilized. A detailed derivation of the deconvolution technique and the total technique is given in Appendix A.

REPORT Section

The REPORT section provides the model's output information to the user. The parameters printed by the REPORT section consist of echoing some operational parameters and fuel cost parameters that were read into the model by the INPUT section as well as parameters which can be calculated as a multiple of energy generation.

Reports are printed on a monthly, quarterly and period of study basis. The user can select the frequency of reports. Figures 8 and 9 show sample output reports. Figure 10 shows the default report which is a summary for the study period of fuel usage by month.

THE VIRGINIA STATE CORPORATION COMMISSION'S
PRODUCTION COST SIMULATION (PCS) MODEL

STUDY TITLE: LOADING-3B 3C 3P 1H VEPCO 1979 PLANT AND REVISED LOAD DATA

VIRGINIA ELECTRIC POWER CO.

EXPECTED UNIT OPERATING CHARACTERISTICS DURING
JAN, 1979

UNIT NAME	LOAD TYPE	FUEL TYPE	AVERAGE TOTAL		THERMAL ENERGY (MMBTU)	ELECTRIC GENERATION (MWH)	AVERAGE HEAT RATE (BTU/KWH)	CAPACITY FACTOR (PCT)	OPERATING AVAILABILITY (PCT)	UNIT CAPACITY (MW)	WEIGHTED AVERAGE FUEL COST (CTS/MMBTU)	LAMDAS		
			FUEL COST (\$/MWH)	FUEL COST (\$000)								HL	3Q	FL
CUSHAW HYDRO	HYDR	HYDR	0.0	0.0	0.	714.	0.	24.0	100.0	4.	0.0	0	0	1
NORTH ANNA 1	BASE	NUCL	4.76	2532.3	6206566.	531604.	11675.	78.8	78.9	907.	40.80	4	15	16
SURRY 1	BASE	NUCL	3.93	2040.3	6004349.	519214.	11564.	90.0	90.5	775.	33.98	5	17	18
SURRY 2	BASE	NUCL	4.98	2766.1	6428365.	555664.	11569.	96.4	97.8	775.	43.03	6	22	23
MT. STORM 3	BASE	COAL	12.25	3807.4	3369372.	310858.	10839.	74.6	77.3	560.	113.00	7	24	27
MT. STORM 1	BASE	COAL		0.0	0.	0.			0.0	553.				
MT. STORM 2	BASE	COAL	11.91	3524.5	3118986.	295867.	10542.	71.9	75.2	553.	113.00	9	26	29
PURCHASE POWER AEP	HYDR	HYDR	0.0	0.0	0.	415950.	0.	69.9	100.0	800.	0.0	0	0	10
BREMO 4	BASE	COAL	15.68	1666.0	1067975.	106252.	10051.	87.1	92.4	164.	156.00	11	30	31
BREMO 3	CYCL	COAL	18.83	915.4	586800.	48626.	12068.	90.8	97.2	72.	156.00	12	32	34
CHESTERFIELD 6	CYCL	COAL	20.04	3038.0	1651049.	151572.	10893.	31.0	35.3	658.	184.00	13	36	37
CHESTERFIELD 5	CYCL	COAL	20.83	696.0	378274.	33416.	11320.	13.5	14.9	333.	184.00	14	33	35
YORKTOWN 1	BASE	HOIL	20.21	2228.7	1125615.	110256.	10209.	89.3	100.0	166.	198.00	21	38	39
ROANOKE RAPIDS	HYDR	HYDR	0.0	0.0	0.	58755.	0.	79.0	100.0	100.	0.0	0	0	30
GASTON	HYDR	HYDR	0.0	0.0	0.	55181.	0.	33.0	100.0	225.	0.0	0	0	35
YORKTOWN 3	BASE	HOIL	20.12	4494.7	2270077.	223406.	10161.	36.7	54.0	818.	198.00	40	41	42
PORTSMOUTH 3	BASE	HOIL	18.16	949.9	524796.	52297.	10035.	43.4	78.3	162.	181.00	43	44	59
PORTSMOUTH 4	BASE	HOIL	18.87	28.7	15859.	1521.	10424.	0.9	1.7	233.	181.00	45	46	58
POSSUM POINT 4	BASE	HOIL	17.77	1806.7	1032420.	101653.	10156.	58.6	97.9	233.	175.00	47	48	49
POSSUM POINT 5	CYCL	HOIL	24.38	6172.6	2529773.	253235.	9990.	42.3	97.0	805.	244.00	50	51	52
YORKTOWN 2	CYCL	HOIL	22.15	485.4	245127.	21914.	11186.	17.3	60.4	170.	198.00	53	54	63
CHESTERFIELD 4	BASE	HOIL		0.0	0.	0.			0.0	166.				
POSSUM POINT 3	BASE	HOIL	18.65	360.1	205790.	19313.	10655.	25.7	93.6	101.	175.00	60	61	62
PORTSMOUTH 1	BASE	HOIL	22.05	354.7	195951.	16087.	12181.	21.4	88.3	101.	181.00	64	65	66
CHESTERFIELD 3	BASE	HOIL	20.92	312.6	168987.	14943.	11309.	20.1	91.4	100.	185.00	67	68	69
PORTSMOUTH 2	CYCL	HOIL	20.12	277.3	153212.	13783.	11116.	18.3	92.7	101.	181.00	70	71	72
POSSUM POINT 2	CYCL	HOIL	22.80	192.0	109699.	8421.	13026.	16.4	92.4	69.	175.00	73	74	77
POSSUM POINT 1	CYCL	HOIL	22.27	202.8	115912.	9107.	12728.	16.5	99.6	74.	175.00	75	76	81
CHESTERFIELD 2	CYCL	HOIL	26.46	193.0	104344.	7295.	14303.	13.4	86.2	73.	185.00	78	79	80
CHESTERFIELD 1	CYCL	HOIL	30.31	127.8	69072.	4216.	16383.	10.1	71.2	56.	185.00	82	83	84
MT. STORM ICEN 1	PEAK	GASO		0.0	0.	0.			0.0	12.				
LOWMOOR ICEN 1-4	PEAK	LOIL	47.85	183.0	61204.	3824.	16005.	8.6	63.6	60.	299.00	94	95	96
NORTHERN NECKICEN1-4	PEAK	LOIL	47.84	185.1	61913.	3869.	16001.	8.1	63.6	64.	299.00	97	98	99
SURRY ICEN 1,2	PEAK	LOIL	50.85	109.7	36685.	2157.	17008.	7.8	63.6	37.	299.00	100	101	102
POSSUM POINT ICEN1-6	PEAK	LOIL	46.10	197.4	66004.	4281.	15419.	7.4	63.6	78.	299.00	103	104	105
PORTSMOUTH ICEN 1346	PEAK	LOIL	50.89	155.4	51981.	3054.	17020.	6.8	63.6	60.	299.00	106	111	112
PORTSMOUTH ICEN 7-10	PEAK	LOIL	50.89	209.2	69981.	4112.	17020.	6.6	63.6	84.	299.00	107	113	114
KITTY HAWK ICEN 1,2	PEAK	LOIL	54.66	110.6	36975.	2023.	18280.	6.2	63.6	44.	299.00	115	116	117
TOTALS			11.74	40323.4	38062880.	3964396.	11085.	55.4		9615.	105.94			
UNSERVED ENERGY (MWH)			39442.											
TOTAL ENERGY REQUIRED (MWH)			4003838.											

Figure 8 Unit Projected Generation and Fuel Cost Information

JAN ,1979--DEC ,1979 PROJECTED GENERATION AND FUEL USE SUMMARY
FOR VIRGINIA ELECTRIC POWER CO.

SYSTEM PARAMETERS BY FUEL TYPE:

	THERMAL ENERGY (MMBTU)	ELECTRIC ENERGY (MWH)	FUEL COST (\$000)	AVERAGE HEAT RATE (BTU/KWH)	AVERAGE COST (\$/MWH)
COAL	165022688.	14971061.	236365.	11023.	15.79
NUCL	167947552.	14450350.	66249.	11622.	4.58
LOIL	9310090.	558942.	30669.	16660.	54.88
HOIL	108123952.	10543981.	264253.	10255.	25.06
GASO	235787.	12866.	789.	18327.	61.36
HYDR		817760.			
TOTALS	450636288.	41354576.	598325.	11117.	14.76

SYSTEM PARAMETERS BY LOAD TYPE:

	THERMAL ENERGY (MMBTU)	ELECTRIC ENERGY (MWH)	FUEL COST (\$000)	AVERAGE HEAT RATE (BTU/KWH)	AVERAGE COST (\$/MWH)
BASE	353598464.	31964608.	372348.	11062.	11.65
CYCL	87495408.	8000725.	194518.	10936.	24.31
PEAK	9545877.	571707.	31458.	16697.	55.03
HYDR		817760.			
TOTALS	450636288.	41354576.	598325.	11117.	14.76

SYSTEM GENERATION PARAMETERS:

TOTAL THERMAL ENERGY	(MMBTU)	450636288.
TOTAL ELECTRICAL GENERATION	(MWH)	41354576.
TOTAL FUEL COST	(\$000)	598325.
TOTAL UNSERVED ENERGY	(MWH)	1404350.
TOTAL ENERGY REQUIRED	(MWH)	42758912.

Figure 9 System Projected Generation and Fuel Information

JAN, 1979 -- DEC, 1979 MONTHLY FUEL USAGE SUMMARY
FOR VIRGINIA ELECTRIC POWER CO.

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTL
COAL													
ENERGY (GWH)	947.	950.	1090.	1138.	1090.	1006.	1413.	1297.	1242.	899.	845.	1163.	13080.
COST (KILO\$)	13647.	15086.	17435.	15098.	14799.	14921.	19965.	18431.	17963.	12301.	11703.	16995.	188345.
COST (\$/MWH)	14.42	15.88	15.99	13.26	13.57	14.83	14.13	14.21	14.47	13.68	13.85	14.62	14.40
NUCL													
ENERGY (GWH)	1606.	1052.	830.	0.	562.	597.	600.	498.	484.	905.	1299.	1820.	10252.
COST (KILO\$)	7339.	4603.	3744.	0.	2675.	2846.	2858.	2272.	2208.	3798.	5664.	8311.	46317.
COST (\$/MWH)	4.57	4.37	4.51	0.0	4.76	4.76	4.76	4.57	4.57	4.20	4.36	4.57	4.52
LOIL													
ENERGY (GWH)	23.	59.	36.	47.	31.	66.	42.	82.	72.	25.	17.	9.	509.
COST (KILO\$)	1150.	3046.	2058.	2759.	1929.	5168.	3227.	6272.	5313.	1866.	1319.	707.	34816.
COST (\$/MWH)	49.33	51.38	57.13	58.16	63.19	77.79	77.51	76.73	73.98	76.02	77.30	79.05	68.42
HOIL													
ENERGY (GWH)	857.	1325.	955.	1215.	797.	1064.	1113.	1203.	745.	731.	595.	334.	10934.
COST (KILO\$)	18187.	28835.	23471.	31964.	21050.	31542.	38090.	43182.	24568.	26662.	21913.	12540.	324003.
COST (\$/MWH)	21.21	21.76	24.57	26.32	26.42	29.64	34.22	35.91	35.67	36.49	36.82	37.49	29.63
GASO													
ENERGY (GWH)	0.	0.	0.	2.	1.	2.	1.	2.	2.	1.	1.	0.	12.
COST (KILO\$)	0.	0.	0.	112.	82.	202.	128.	173.	153.	57.	41.	22.	969.
COST (\$/MWH)	0.0	0.0	0.0	71.03	77.75	97.34	96.95	69.51	68.64	68.64	69.80	71.41	77.77
HYDR													
ENERGY (GWH)	531.	337.	332.	592.	630.	520.	586.	633.	611.	637.	623.	618.	6648.
COST (KILO\$)	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
COST (\$/MWH)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTALS FOR FUELS: GENERATED													
ENERGY (GWH)	3964.	3724.	3243.	2994.	3110.	3256.	3755.	3714.	3155.	3197.	3379.	3944.	41435.
COST (KILO\$)	40323.	51570.	46708.	49933.	40535.	54679.	64267.	70330.	52206.	44685.	40639.	38576.	594450.
COST (\$/MWH)	11.74	15.23	16.04	20.79	16.34	19.98	20.28	22.83	20.52	17.46	14.74	11.60	17.09
UNSERVED													
ENERGY (GWH)	39.	142.	77.	87.	50.	204.	116.	286.	234.	43.	30.	15.	184.
TOTAL													
ENERGY (GWH)	4004.	3866.	3320.	3081.	3160.	3460.	3870.	4000.	3389.	3240.	3410.	3959.	41619.

Figure 10 Fuel Usage Summary by Month for the Study Period

DISPATCH Module

The DISPATCH module is a separate program which to a first order approximation develops an economic dispatching order subject to a minimum capacity on-line constraint. This module is used to provide the user with an alternative loading to that provided as part of the generating unit files or an initial loading order.

A flow diagram of the DISPATCH model is shown in Figure 11. The module uses the hydro and fossil/nuclear plant files as input. Information contained in these files is used to calculate a dispatching cost for each fossil and nuclear unit loading step. If hydro units exist in the generating system, additional costing information is requested by the programs for each month.

For each month, the program requests the minimum amount of capacity that is to be on-line. This value is used to simulate the backing off of base loaded units to meet night-time loads (minimum) loads. The program loads the first loading blocks of the least costly units until the minimum load is reached.

If a unit has zero equivalent availability for the month its capacity is not included in the capacity on-line which meets the minimum loading requirements. However, that unit is positioned in the loading order based on its cost.

Having met the minimum loading requirement, the program proceeds to load the remaining loading steps. This is accomplished by first combining the information contained in the loading array by load step into one cost array, one unit array and one load step array. The unit array and the load step array are ordered by increasing cost using the cost array.

At this point the remaining load steps are ordered by cost; however, the loading order may now imply the physically impossible situation where the loading steps for a single unit are not in numerical sequence. The program adjusts the cost-ordered loading sequence to ensure that the physical loading sequence is correct.

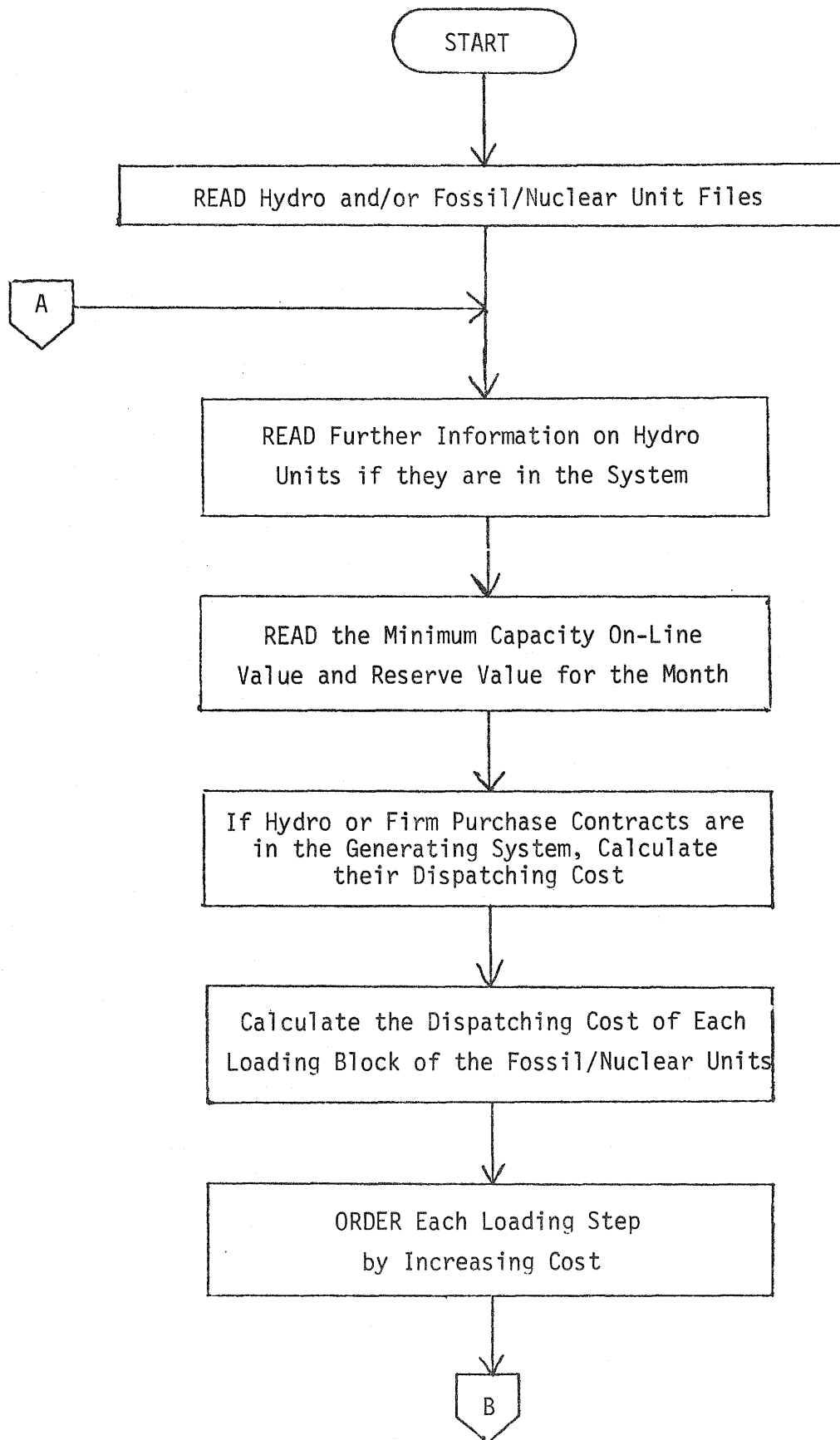
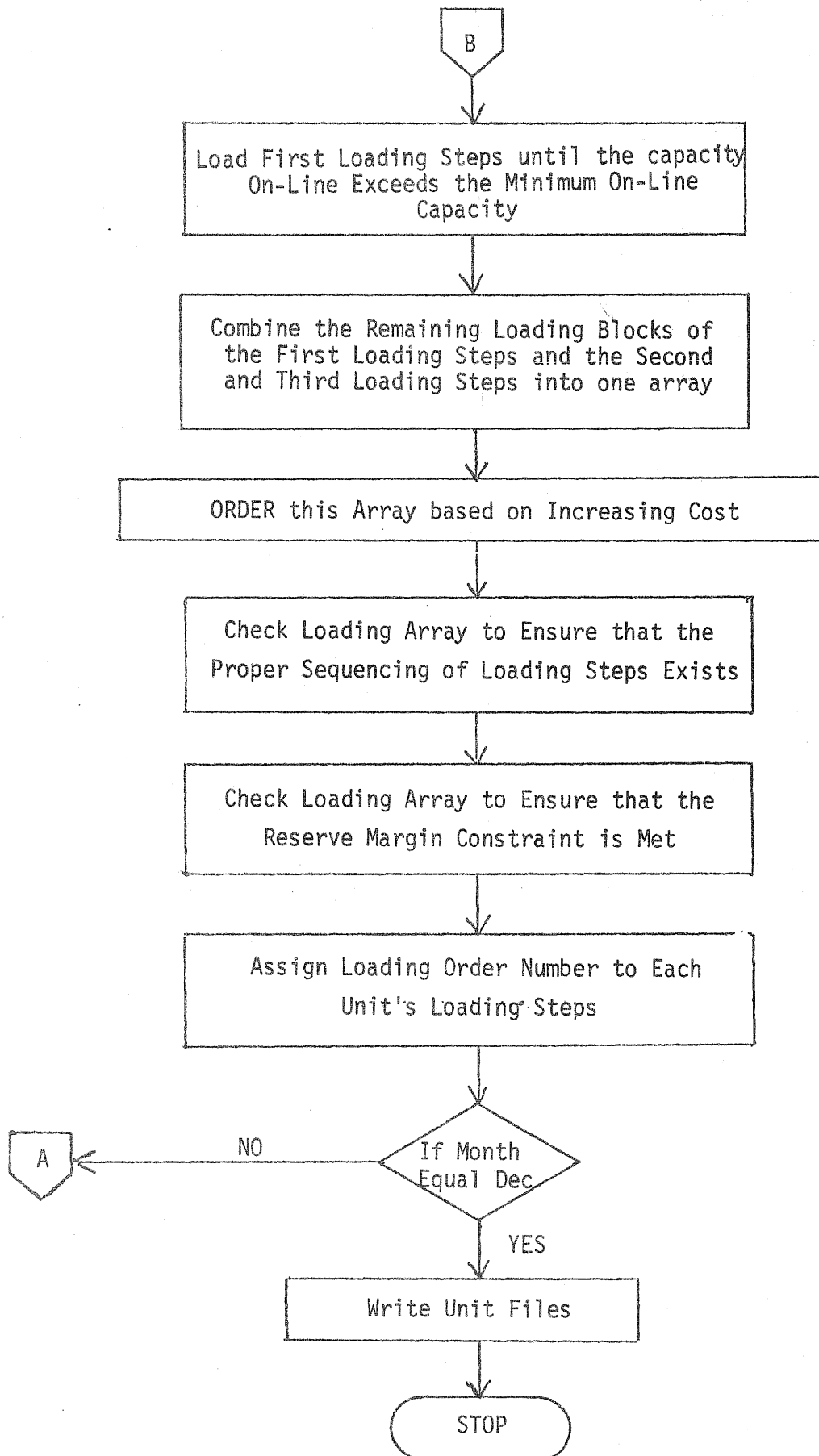


Figure 11 Flow Diagram of the DISPATCH Module



Finally, the loading order is adjusted subject to the reserve margin constraint. This constraint is designed to keep the available generating reserve on-line above the reserve margin value entered by the user. When the available reserve value drops below the reserve constraint the program searches the loading order to find the first loading block of a unit. This block is then loaded to increase the available reserve. If all the first loading steps have been dispatched, this constraint cannot be met and, the remaining load steps are then dispatched without regard to reserve.

The loading of each step having been completed, loading positive numbers are assigned to each load step of each unit. The first block loaded is assigned the number five. The second is assigned the number ten. Subsequent steps are incremented by five. Avoiding consecutive numbers allows for ease of adjusting load positions at the user's discretion.

The above process is carried out for each month of the year. After this is accomplished the fossil/nuclear file and the hydro file are written to disk space as new files. This allows the user to maintain the old files with their loading orders.

LOAD PROBABILITY Module

The purpose of the LOAD PROBABILITY module is to calculate a load probability curve for each month from hourly load data. This module is to be used when the utility can supply the hourly load data in the format defined by the Edison Electric Institute.

The flow diagram of the module is shown in Figure 12. The module reads the hourly loads for the period. These load values are stored in an array which views the year as twelve months, each having 31 days. Days which do not exist have zero loads which the program bypasses.

Having read the hourly loads the program calculates the load probability curve for each month in the study period. The load probability curve provides the information on the portion of time the load represented by the hourly loads meets or exceed a given value. Representative load probability curves are shown in the section of this manual which describes the PCS module.

When the load probability curve is calculated it is written to disk space for use in the PCS module.

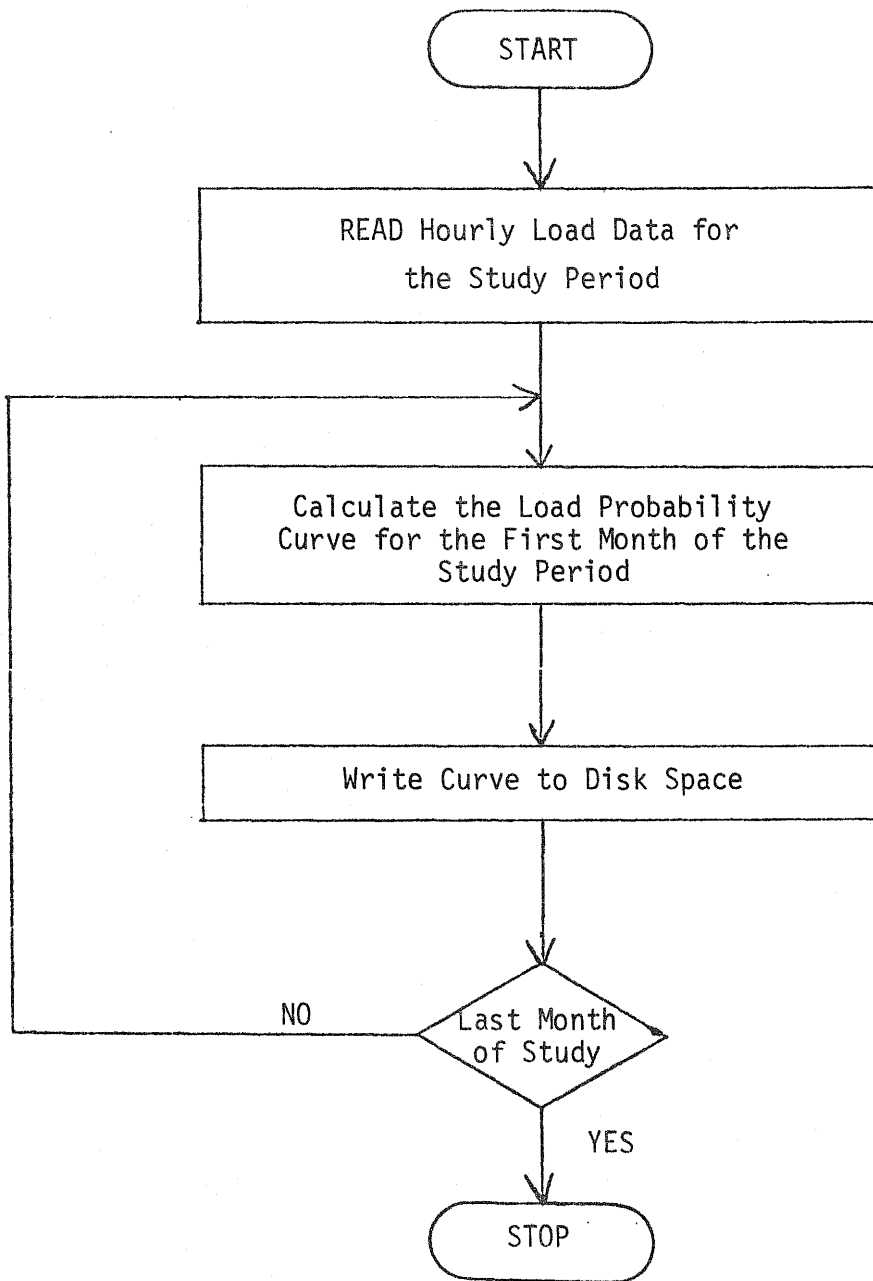


Figure 12 Flow Diagram of the LOAD PROBABILITY Module

INPUT Files

Unit Operational and Fuel Data Files

These data are divided into two separate files, one for fossil and nuclear units and the other for hydro units.

Each file contains unit operation data. The data in this file is used by the LOADER, ENERGY and REPORT sections of the PCS module. For each generating unit there are 13 records or computer cards containing information. The first record contains information about the unit, which does not change from month to month. The following 12 records contain monthly operating information. One record is used for each month.

Figure 13 shows the format for the fossil unit file. Figure 14 shows the format for the hydro unit file. Appendix B contains a description of the data elements.

Load Data Files

The PCS module requires that the load data be presented in the format of a load probability curve. This curve expresses the fraction of time the load meets or exceeds a given load value. The LOADPROB module is used to calculate the load probability curve from hourly loads in the format used to report these loads to the Edison Electric Institute.

VIRGINIA STATE CORPORATION COMMISSION'S PRODUCTION COST SIMULATION (PCS) MODEL REPORTING FORM

COMPANY
UNIT NAME
DATE

NUCLEAR AND FOSSIL UNIT DATA FILE

		VSOC		UNIT NAME		FRAC.		FUELS			ON-LINE		OFF-LINE		ANNUAL	CAPACITY		CAPACITY	
CN	NUMBER					OWNED	UT	LT	P	A	I	MO	YEAR	MO	YEAR	EQUIV.	COST	WIN	SUM
*	X	X		X		X	X	X	X	X	X	X	X	X	X	X	X	X	X
		CAPACITY AND HEAT RATE BY LOADING BLOCK										MONTHLY		FRAC.	DISPATCHING ORDER				
		VSOC	BLOCK 1		BLOCK 2		BLOCK 3		EQUIV.		FUEL COST		GEN.	BY LOADING BLOCK					
MO	YR	NUMBER	MW1	HTRT1	MW2	HTRT2	MW3	HTRT3	AVAIL.	PRIMARY	SECONDARY	BY PRI	BK1	BK2	BK3				
*	1	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	2	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	3	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	4	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	5	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	6	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	7	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	8	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	9	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	10	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	11	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	
*	12	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	

27

* Key punch only the lines marked with an asterisk.

X Represents a blank.

Figure 13 Nuclear and Fossil Unit Data File Format

The load probability information is provided on a monthly basis in the format shown in Figure 15. The first record for each month gives the month, year, minimum load, maximum load, number of data points to follow and the total generation expressed by the curve. The following records list the y-axis data points, where the first value of 1.000000 corresponds to the minimum load. The last value corresponds to the peak maximum demand during the month. All y-axis values between the first and last are based on uniformly spaced x-axis values. The load spacing is calculated from

$$\text{DELTA} = \frac{(\text{MAXLOAD} - \text{MINLOAD})}{\text{POINTS} - 1} \quad (8)$$

where MAXLOAD is the maximum load for the month, MINLOAD is the minimum load for the month and POINTS is the number of points in the curve. For example, the x-axis load spacing (DELTA) for January as shown in Figure 11 is 88.69 MW. The PCS model uses the calculated value of DELTA to calculate the x-axis values of the load probability curve.

User Supplied Data

The user must supply information to the PCS model in order to specify calculation options and provide headings for tables. Listed below is the information the PCS module requires.

```

ENTER THE STUDY TITLE
ENTER COMPANY NAME
ENTER FIRST MONTH OF STUDY (1-12)
ENTER FIRST YEAR OF STUDY
ENTER LAST MONTH OF STUDY (1-12)
ENTER LAST YEAR OF STUDY
ARE THERE HYDRO UNITS ? (T OR F)
ENTER # LOADING STEPS FOR BASE, CYCLE, & PEAK
ENTER FILE NUMBER FOR OUTPUT REPORTS
REPORT OPTION ? (1-3)
  1 ALL REPORTS
  2 QUARTERLY AND ANNUAL REPORTS
  3 ANNUAL REPORT AND MONTHLY FUEL SUMMARY
  4 MONTHLY FUEL SUMMARY ONLY

```

A B C D E F G

1 79 50 3024. 7370. 744. 3951534.

H { 1.000000.9946236.9919354.9892473.9838709.9811828.9717742.9623656.9502688.9435484
.9381720.9274193.9166666.9032258.8790323.8534946.8239247.8010752.7674731.7338709
.7096774.6854838.6545699.6276882.5994623.5698925.5322580.4784946.4422043.4045699
.3709677.3319892.2836021.2500000.2190860.1774193.1451613.1182795.0940860.0793011
.0524194.0430108.0322581.0201613.0188172.0147849.0120968.0040323.0013441.0013441

A - Month

E - Maximum load

B - Year

F - Number of hours in the month

C - Number of Points in the
Load probability curve

G - Megawatt hours represented by
the curve

D - Minimum Load

H - Load probability values

Figure 15. Load Probability Curve Data

PART II PCS Model Programs

PCS Module Execution

The PCS module was developed on the Ohio State University's Amdahl 470 computer system, where it was compiled using Fortran H extended. The IBM-compatible operating system allows either batch processing or on-line execution using the Time-Sharing Option (TSO). A representative set of batch-processing instructions is shown in Figure 16, while the corresponding interactive commands are shown in Figure 17. Note that interactive users may wish to allocate FT04F001 to their terminal's keyboard for direct control over the execution parameters, in lieu of allocating it to a disk file. For the logical record length, field definitions, and data content of the other three input files (HYDRO.UNIT.DATA, FOSSIL.NUCLEAR.UNIT.DATA, and LOAD.PROB.DATA), please refer to the file descriptions in Part I of this manual.

DISPATCH Module Execution

The DISPATCH module can be executed either in batch or interactive mode. Figure 18 lists the JCL used at The Ohio State University computer center. Figure 19 lists the TSO commands needed to operate the module.

LOAD PROBABILITY Module Execution

As with the PCS and DISPATCH module the LOAD PROBABILITY module can be executed in batch or interactively. The JCL and TSO command for this module are shown in Figures 20 and 21.

```

PCS.CNTL
// MSGCLASS=A,REGION=256K,TIME=2
/*JOBPARM DISKIO=4000,LINES=12000,COPIES=1
//S1 EXEC PROC=FOR TXCLG,PARM.FORT='XREF,NODECK,OPT(0)',TIME.GO=(1,15)
//SYSPRINT DD SYSOUT=A
//FORT.SYSIN DD DSN=PCS.FORT,DISP=SHR
//GO.FT06F001 DD SYSOUT=A,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=665,BUFNO=1)
//GO.FT04F001 DD DSN=USER.INPUT.DATA,DISP=SHR
//GO.FT11F001 DD DSN=HYDRO.UNIT.DATA,DISP=SHR
//GO.FT12F001 DD DSN=FOSSIL.NUCLEAR.UNIT.DATA,DISP=SHR
//GO.FT13F001 DD DSN=LOAD.PROB.DATA,DISP=SHR
//

```

Figure 16 JCL for PCS Module

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```

PCS.CLIST
PROC 0 TIME(,5)
TIME
FREE F(FT04F001 FT06F001 FT11F001 FT12F001 FT13F001)
ALLOC F(FT04F001) DA(USER.INPUT.DATA) SHR
ALLOC F(FT06F001) DA(*)
ALLOC F(FT11F001) DA(HYDRO.UNIT.DATA) SHR
ALLOC F(FT12F001) DA(FOSSIL.NUCLEAR.UNIT.DATA) SHR
ALLOC F(FT13F001) DA(LOAD.PROB.DATA) SHR
FORT PCS.FORT
LOADGO PCS.OBJ FORTLIB

```

Figure 17 TSO Commands for PCS Module

```

FORT.CNTL(DISPATCH)
00010 // MSGCLASS=A,REGION=256K
00020 /*JOBPARM DISKIO=4000,LINES=12000
00030 //S1 EXEC PROC=FORTXCLG,PARM.FORT='XREF,NODECK,OPT(0)'
00040 //FORT.SYSIN DD DSN=DISPATCH.FORT,DISP=SHR,
00050 //   DCB=(RECFM=FB,LRECL=80,BLKSIZE=400)
00060 /* UNIT 5 IS FOR USER SUPPLIED DATA */
00070 //GO.FT05F001 DD DSN=DISPATCH.USER.INPUT.DATA,DISP=SHR
00080 /* UNITS 11 AND 12 ARE FOR INPUT FROM EXISTING UNIT FILES
00090 //GO.FT11F001 DD DSN=OLD.HYDRO.DATA,DISP=SHR,
00100 //   DCB=(RECFM=FB,LRECL=80,BLKSIZE=400)
00110 //GO.FT12F001 DD DSN=OLD.FOSSIL.NUCLEAR.DATA,DISP=SHR,
00120 //   DCB=(RECFM=FB,LRECL=80,BLKSIZE=400)
00130 /* UNITS 20 AND 21 ARE FOR THE OUTPUT OF THE NEW UNIT FILES
00140 //GO.FT20F001 DD DSN=NEW.HYDRO.DATA,DISP=NEW,
00150 //   DCB=(RECFM=FB,LRECL=80,BLKSIZE=400)
00160 //GO.FT21F001 DD DSN=NEW.FOSSIL.NUCLEAR.DATA,DISP=NEW,
00170 //   DCB=(RECFM=FB,LRECL=80,BLKSIZE=400)
00180 //

```

Figure 18 JCL for DISPATCH Module

```

DISPATCH.TSO.CLIST
00010 FREE F(FT05F001,FT11F001,FT12F001,FT20F001,FT21F001)
00020 ATTRIB ONE LRECL(80) RECFM(F,B) BLKSIZE(400)
00030 ALLOC F(FT05F001) DA(DISPATCH.USER.INPUT.DATA)
00040 ALLOC F(FT11F001) DA(OLD.HYDRO.DATA)
00050 ALLOC F(FT12F001) DA(OLD.FOSSIL.NUCLEAR.DATA)
00060 ALLOC F(FT20F001) DA(NEW.HYDRO.DATA) NEW USING(ONE)
00070 ALLOC F(FT21F001) DA(NEW.FOSSIL.NUCLEAR.DATA) NEW USING(ONE) -
00080   TRACKS SPACE(1,1) CATALOG
00090 FORT DISPATCH.FORT
00100 LOADGO DISPATCH.OBJ FORTLIB

```

Figure 19 TSO Commands for DISPATCH Module

```

LOADPROB.CNTL
00010 // MSGCLASS=A,REGION=256K
00020 /*JOBPARM DISKIO=2000
00030 //S1 EXEC PROC=FORTXCLG,PARM.FORT='XREF,NODECK,OPT(0) '
00040 //FORT.SYSIN DD DSN=LOADPROB.FORT,DISP=SHR
00050 /* UNIT 10 IS FOR HOURLY LOAD DATA
00060 //GO.FT10F001 DD DSN=HOURLY.LOAD.DATA,DISP=SHR
00070 /* UNIT 15 IS FOR THE LOAD PROB OUTPUT
00080 //GO.FT15F001 DD DSN=LOAD.PROB.OUTPUT.DATA,DISP=NEW,
00090 //      DCB=(RECFM=FB,LRECL=80,BLKSIZE=400)
00100 //

```

Figure 20 JCL for LOAD PROBABILITY Module

```

LOADPROB.TSO.CLIST
00010 FREE F(FT15F001,FT10F001)
00011 ATTRIB ONE LRECL(80) RECFM(F,B) BLKSIZE(400)
00030 ALLOC F(FT10F001) DA(HOURLY.LOAD.DATA) OLD
00040 ALLOC F(FT15F001) DA(LOAD.PROB.OUTPUT.DATA) NEW TRACKS SPACE(1,1) -
00041      USING(ONE) CATALOG
00050 FORT LOADPROB.FORT
00060 LOADGO LOADPROB.OBJ FORTLIB

```

Figure 21 TSO Commands for LOAD PROBABILITY Module

PCS Module Routines

The PCS module contains a Main routine and 27 subroutines. Figure 22 shows the name of each subroutine in their calling sequence.

This section contains a description of each subroutine, a list of variables and their definitions, and a flow chart for each one. Appendix C contains a complete source listing of the PCS module.

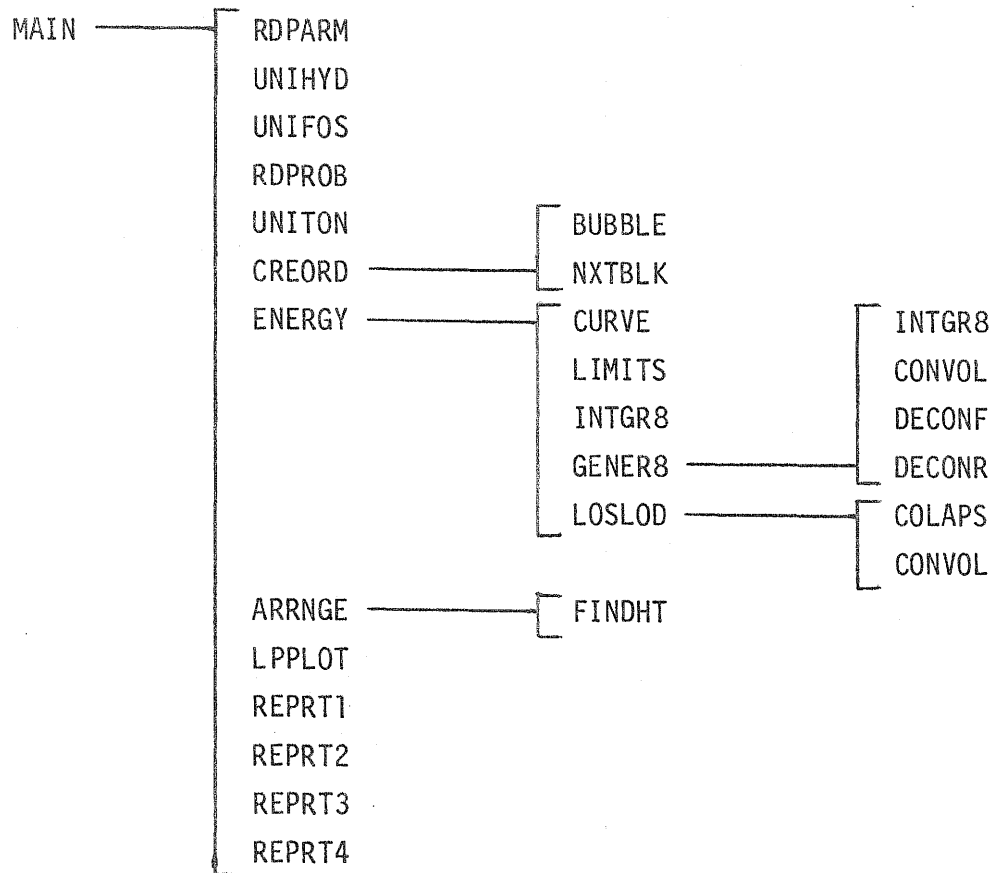


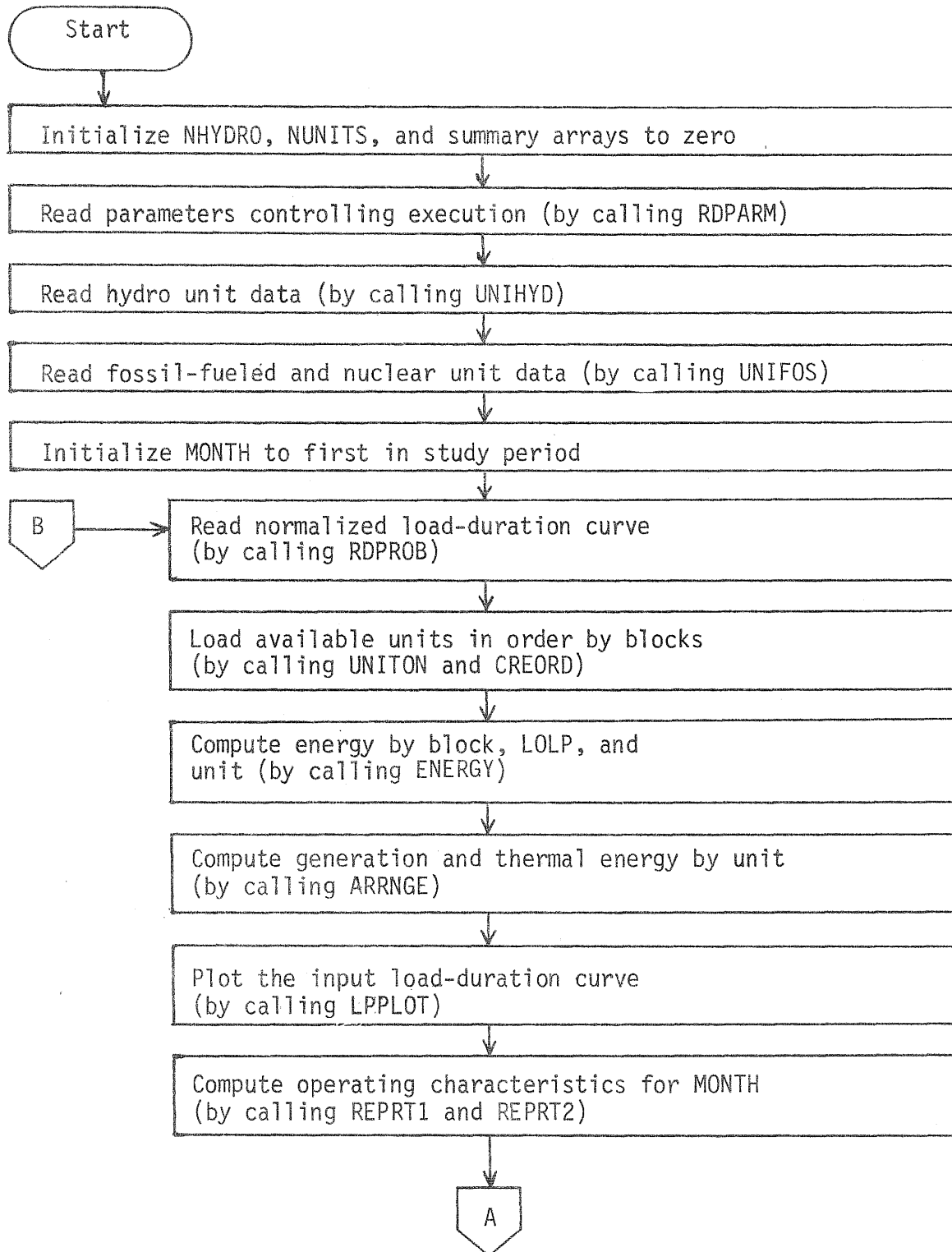
Figure 22 PCS Module Subroutines in the Sequence Called

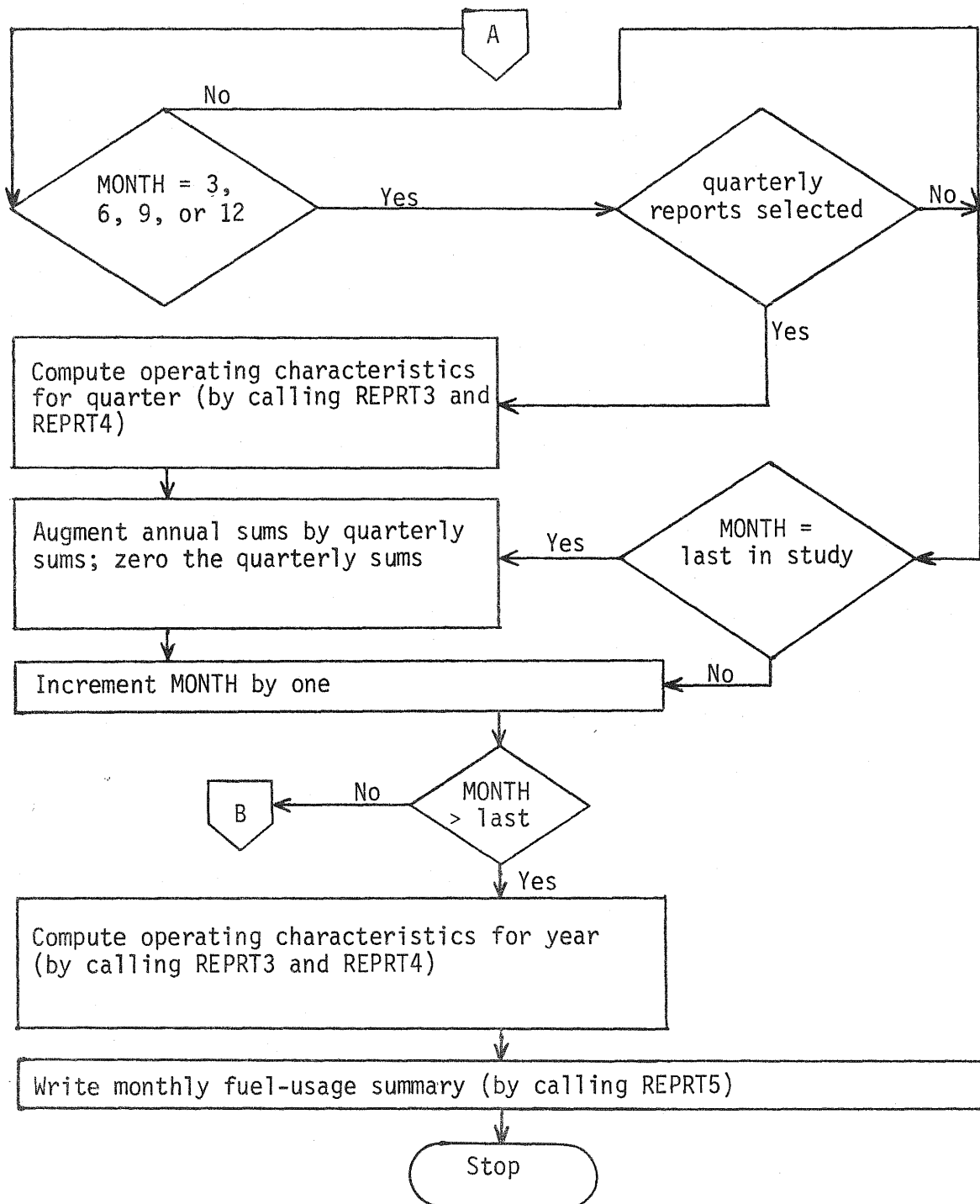
MAIN Routine

This program serves to structure the execution of computation in a concise, straightforward sequence. Following the definition of each global variable's type and dimension, summary variables are initialized and operating characteristics are read for each generating unit. The monthly loop controls the computation and reporting of each unit's operating characteristics. The annual reports and monthly fuel-usage summary are generated once at the conclusion of the study period.

Since the annual sums are initialized only once, and the generating units' input data are read for only twelve months, the program in its present configuration is not appropriate for study periods spanning more than one calendar year. With care taken to control the amount of generation-unit data read each year, a multi-year loop could be added if longer study periods are desired.

MAIN





```

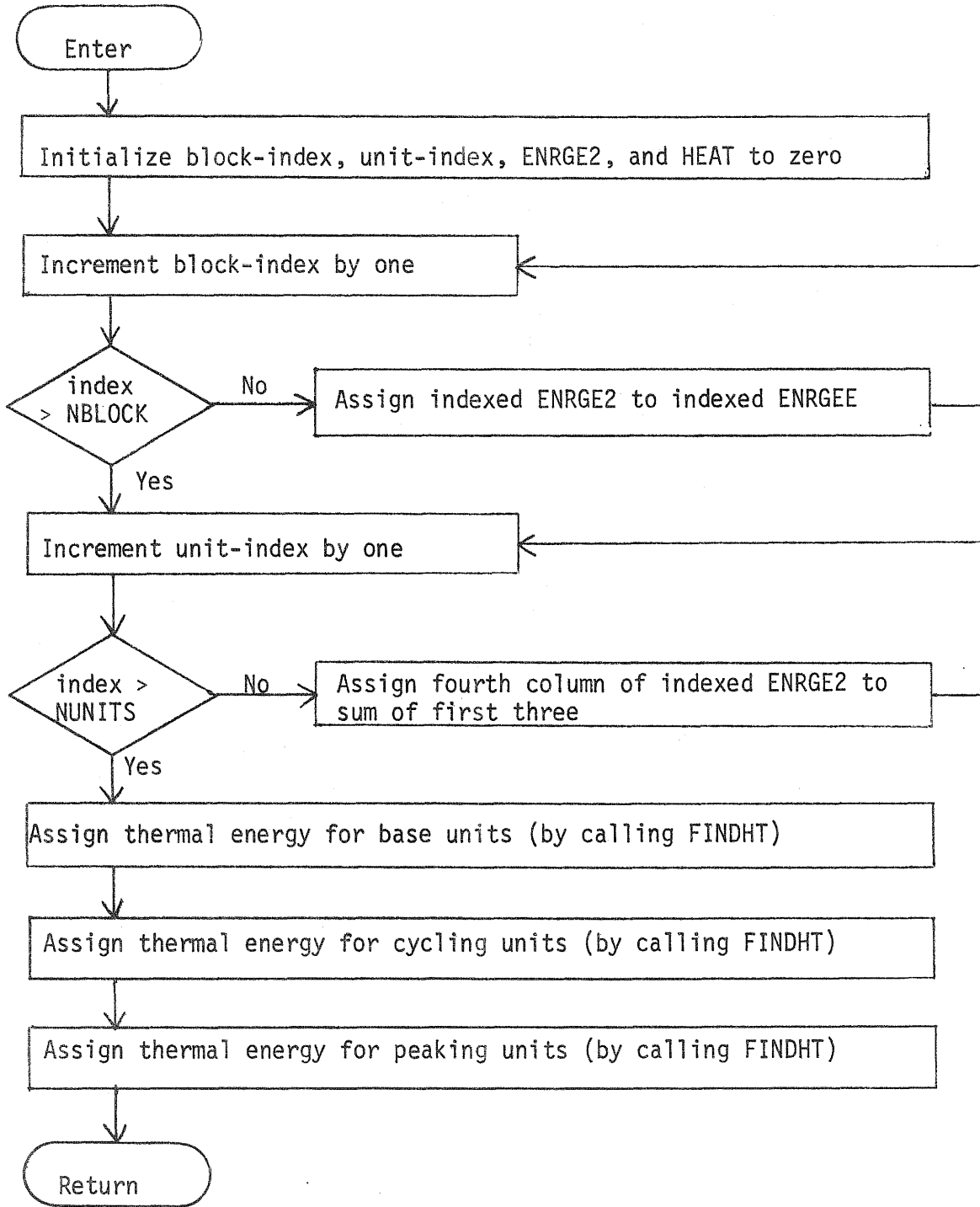
=====
C
C ROUTINE:          **** M A I N ****
C
C REQUIREMENTS:
C   I/O UNITS TO BE ALLOCATED BY JOB CONTROL:
C   HYUNIT  LOGICAL UNIT (11) FROM WHICH TO READ HYDRO INFO
C   PFUNIT  LOGICAL UNIT (12) FROM WHICH TO READ FOSSIL INFO
C   PBUNIT  LOGICAL UNIT (13) FROM WHICH TO READ LOAD-PROBABILITIES
C   SUNIT   LOGICAL UNIT TO WHICH TO WRITE ALL REPORTS SELECTED
C           ACCORDING TO OPTION IN ROUTINE RDPARM;
C           LOGICAL UNITS MUNIT, QUNIT, AND AUNIT ARE SET EITHER
C           TO ZERO OR TO SUNIT ACCORDING TO OPTION
C
C ROUTINES CALLED:
C   RDPARM  UNIHVD  UNIFOS  RDPROB
C   UNITON  CREORD  ENERGY  ARRNGE  LPPLOT
C   REPRT1  REPRT2  REPRT3  REPRT4  REPRT5
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, MARCH 1979
C
C LAST REVISED:  10/79
=====

```

ARRNGE Routine

This routine rearranges the generation (ENRGEE) from a single-column array by order of block loaded, to a three-column representation (ENRGE2) with columns ordered by block-level and rows ordered by unit-number. The fourth column of ENRGE2 is reserved for the total generation by unit. Preparatory to writing reports, the thermal energy input requirements are calculated for each of the categories of thermal units: base, cycling, and peaking.

ARRNGE



```

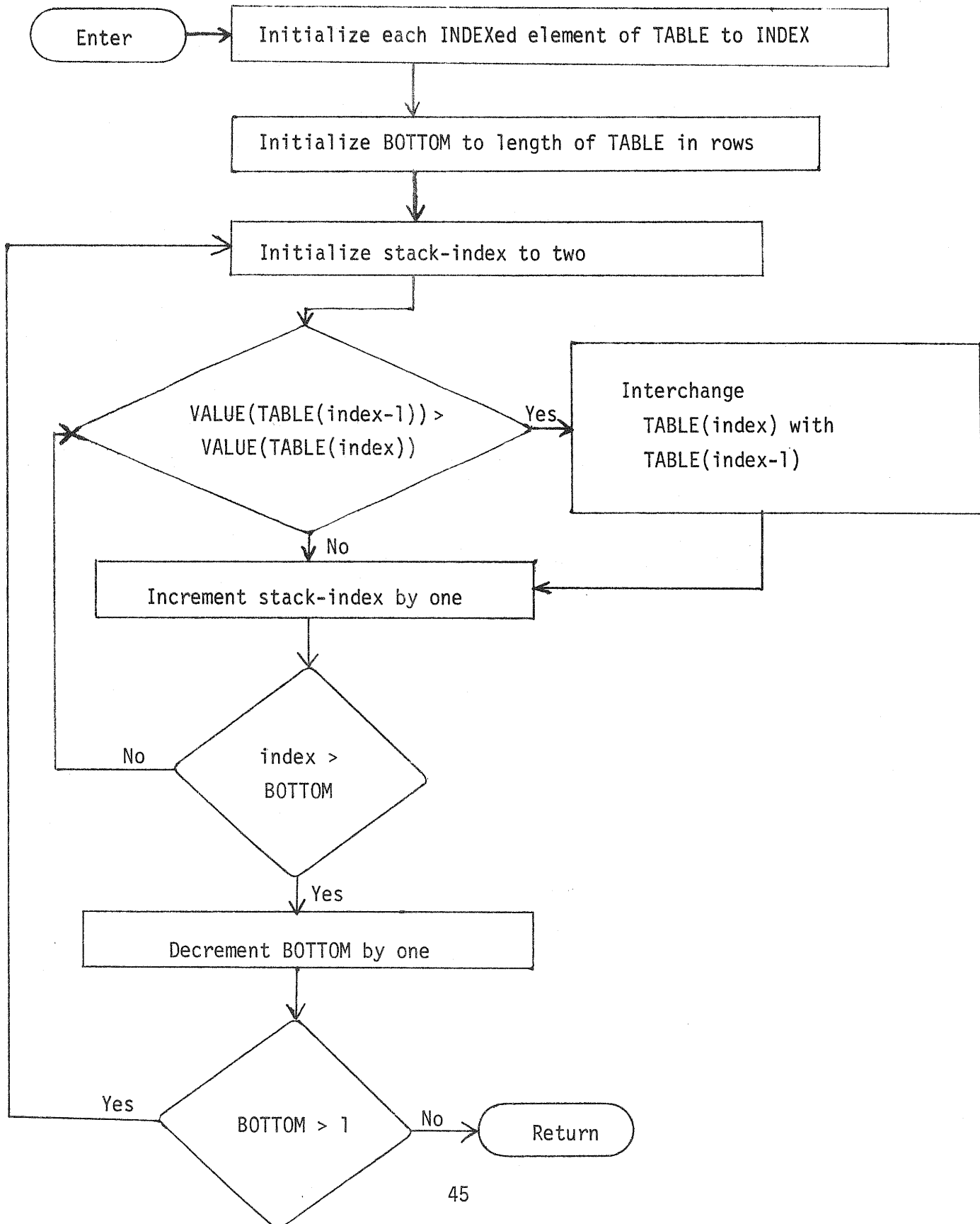
C=====
C
C ROUTINE:          **** A R R N G E ****
C
C PURPOSE:
C   TO ARRANGE THE GENERATED ENERGY (WHICH IS IN ORDER BY LOADING BLOCK
C   IN ARRAY ENRGE) BY UNIT IN ORDER OF LOADING, AND TO COMPUTE THE
C   THERMAL ENERGY REQUIREMENTS OF EACH BLOCK LOADED
C
C INPUT VARIABLES:
C   NBLOCK          NUMBER OF BLOCKS LOADED
C   UNIT            LOADING ORDER OF UNITS
C   BLOCK           LOADING ORDER OF BLOCKS
C   ENRGE           ENERGY GENERATED BY EACH BLOCK, IN MWH
C   NUNITS          NUMBER OF UNITS LOADED
C   IDBASE          INDEX OF BASE-LOADED UNITS, IN THE ORDER READ
C   NBASE           NUMBER OF BASE-LOADED UNITS LOADED
C   NBSTEP          NUMBER OF LOADING-STEPS USED FOR BASE UNITS
C   IDCYCL          INDEX OF CYCLING UNITS, IN THE ORDER READ
C   NCYCL           NUMBER OF CYCLING UNITS LOADED
C   NCSTEP          NUMBER OF LOADING-STEPS USED FOR CYCLING UNITS
C   IDPEAK          INDEX OF PEAKING UNITS, IN THE ORDER READ
C   NPEAK           NUMBER OF PEAKING UNITS LOADED
C   NPSTEP          NUMBER OF LOADING-STEPS USED FOR PEAKING UNITS
C   HEATR1          HEAT RATE IN BTU/KWH OF FIRST BLOCK, BY UNIT
C   HEATR2          HEAT RATE IN BTU/KWH OF SECOND BLOCK, BY UNIT
C   HEATR3          HEAT RATE IN BTU/KWH OF THIRD BLOCK, BY UNIT
C
C OUTPUT VARIABLES:
C   ENRGE2          ENERGY GENERATED BY UNITS, BY COLUMNS: 1-FIRST BLOCK,
C                   2-SECOND BLOCK, 3-THIRD BLOCK, 4-TOTAL FOR UNIT
C   HEAT            THERMAL ENERGY REQUIREMENTS BY UNITS, BY COLUMNS:
C                   1-FIRST BLOCK, 2-SECOND BLOCK, 3-THIRD BLOCK,
C                   4-TOTAL FOR UNIT
C
C ROUTINES CALLED:
C   FINDHT
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====

```

BUBBLE Routine

As implied by its name, this routine performs a bubble-sort on the elements of array VALUES. By using an index array TABLE for the manipulations of order, the sorting operation leaves VALUES intact. Upon initialization, TABLE contains the ordered set of integers (1, 2, 3, ... , LENGTH); upon exit, it contains the set of row-indices ordered by ascending value of elements in VALUE. Thus the first element of TABLE is the row index of the smallest element in VALUE, and the last is the row index of the largest.

BUBBLE

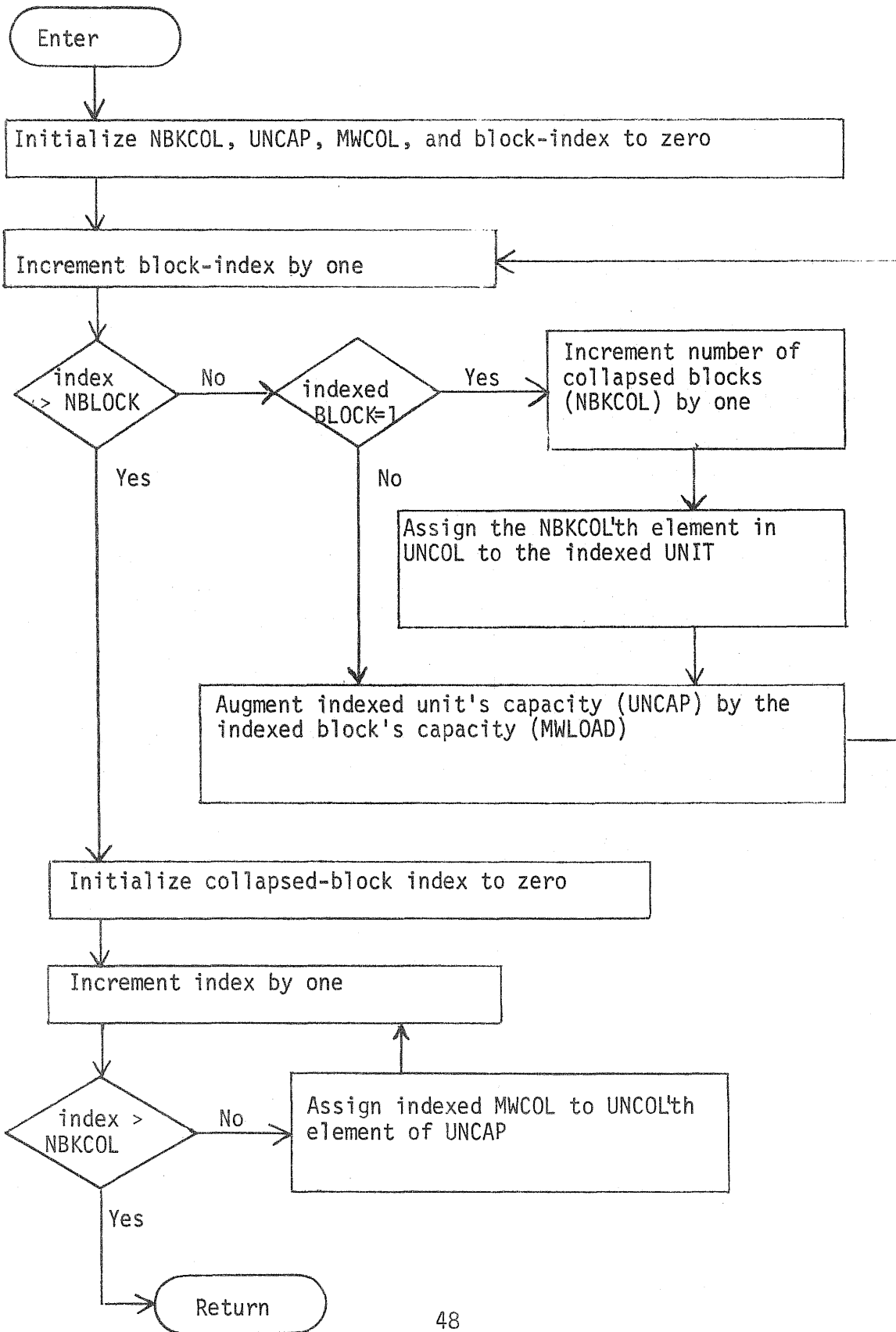


```
C=====
C
C ROUTINE:          **** B U B B L E ****
C
C PURPOSE:
C   GIVEN THE ARRAY VALUES, BUBBLE CREATES AN ARRAY TABLE,
C   WHICH IS A POINTER TO EACH LOCATION IN THE VALUE ARRAY
C
C-----
C INPUT VARIABLES:
C   VALUES      LAMBDA-VALUES TO BE SORTED
C   LENGTH       NUMBER OF VALUES
C   COL          COLUMN OF TABLE TO USE
C   MONTH        MONTH OF STUDY
C
C OUTPUT VARIABLES:
C   TABLE       INDICES SHOWING SORTED ORDER OF THE ARRAY VALUES
C                (RANGES FROM 1 TO LENGTH)
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====
```


COLAPS Routine

This routine adds generation capacities across blocks of each unit, returning the sums in the collapsed capacity (MWCOL) array. The array elements are ordered by considering only the lambda-values of the first block of each unit; higher-blocks' lambdas are ignored.

COLAPS

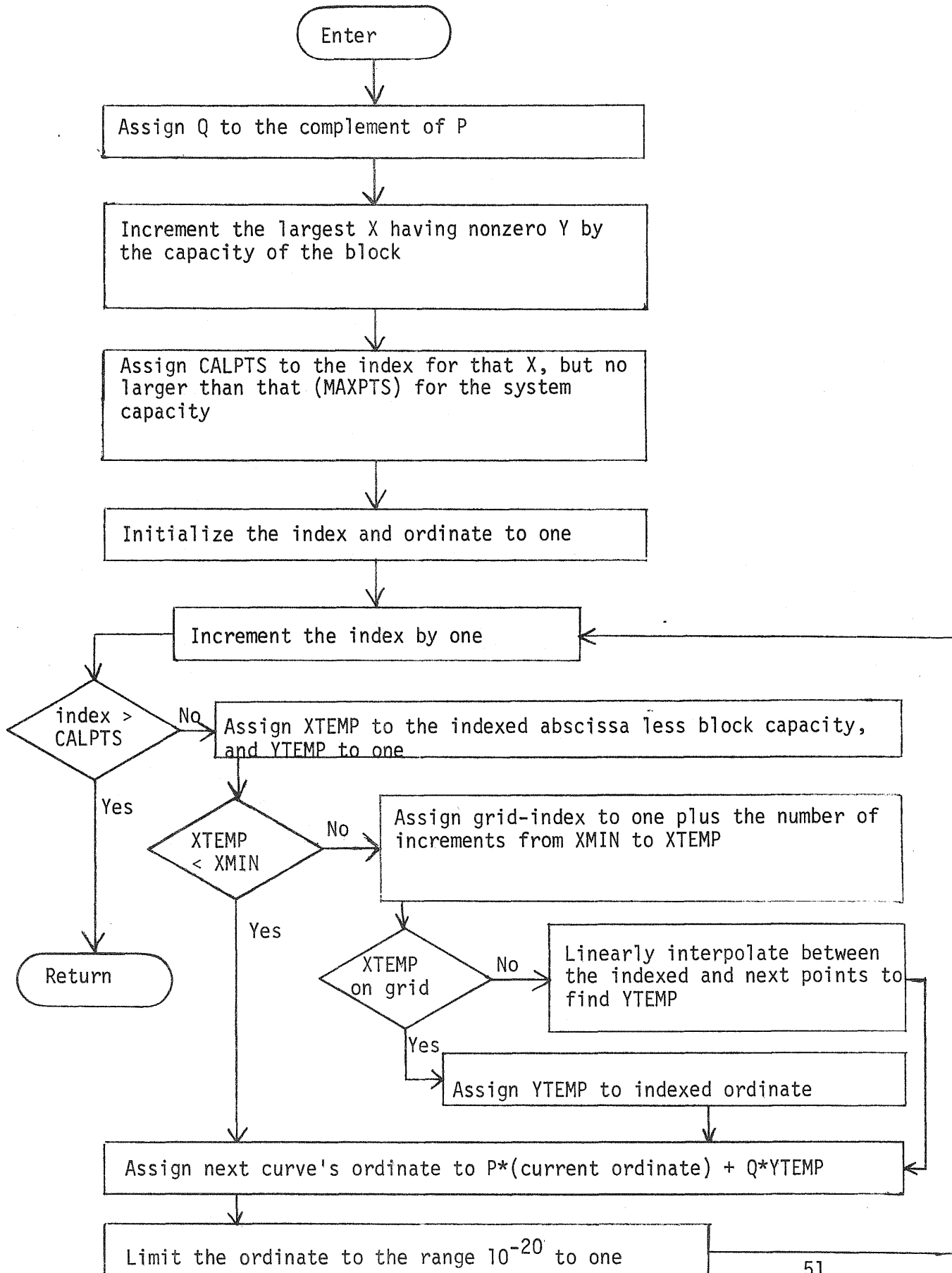


```
C=====
C
C ROUTINE:          **** C O L A P S ****
C
C INPUT VARIABLES:
C   MWBLOK   CAPACITY BY BLOCKS LOADED
C   UNIT     LOADING ORDER OF UNITS
C   BLOCK    LOADING ORDER OF BLOCKS
C   NBLOCK   NUMBER OF BLOCKS TO LOAD
C
C OUTPUT VARIABLES:
C   UNCOL    COLLAPSED LOADING ORDER ARRAY
C   NBKCOL   NUMBER OF BLOCKS IN THE COLLAPSED ORDER
C   SYSCAP   TOTAL SYSTEM CAPACITY IN MW
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, MAY 1979
C
C LAST REVISED:  10/79
C=====
```

CONVOL Routine

This routine performs the convolution of two cumulative probability distribution functions, one of which is the current normalized equivalent load-duration curve. It is normalized in that ordinates (duration) are on the range from zero to one, inclusive. The other function is the capacity outage distribution, which has discontinuous jumps of P at zero capacity and $1-P$ at a capacity (abscissa) of CAP . The simplification afforded by the outage distribution's derivative vanishing at all but two points, is evident in the routine's algorithm: at any abscissa X , the ordinate Y (NEXT) after convolution is the sum of P times the ordinate Y (CURRNT) before convolution, and $(1-P)$ times the ordinate Y (CURRNT) evaluated at that abscissa less the capacity CAP . For negative abscissas, the current curve is defined with unit ordinates. Since a single ordinate may be the result of multiple convolutions, each involving the product of numbers less than one, underflow is possible; it is avoided by rounding all ordinates less than 10^{-10} to zero.

CONVOL



```

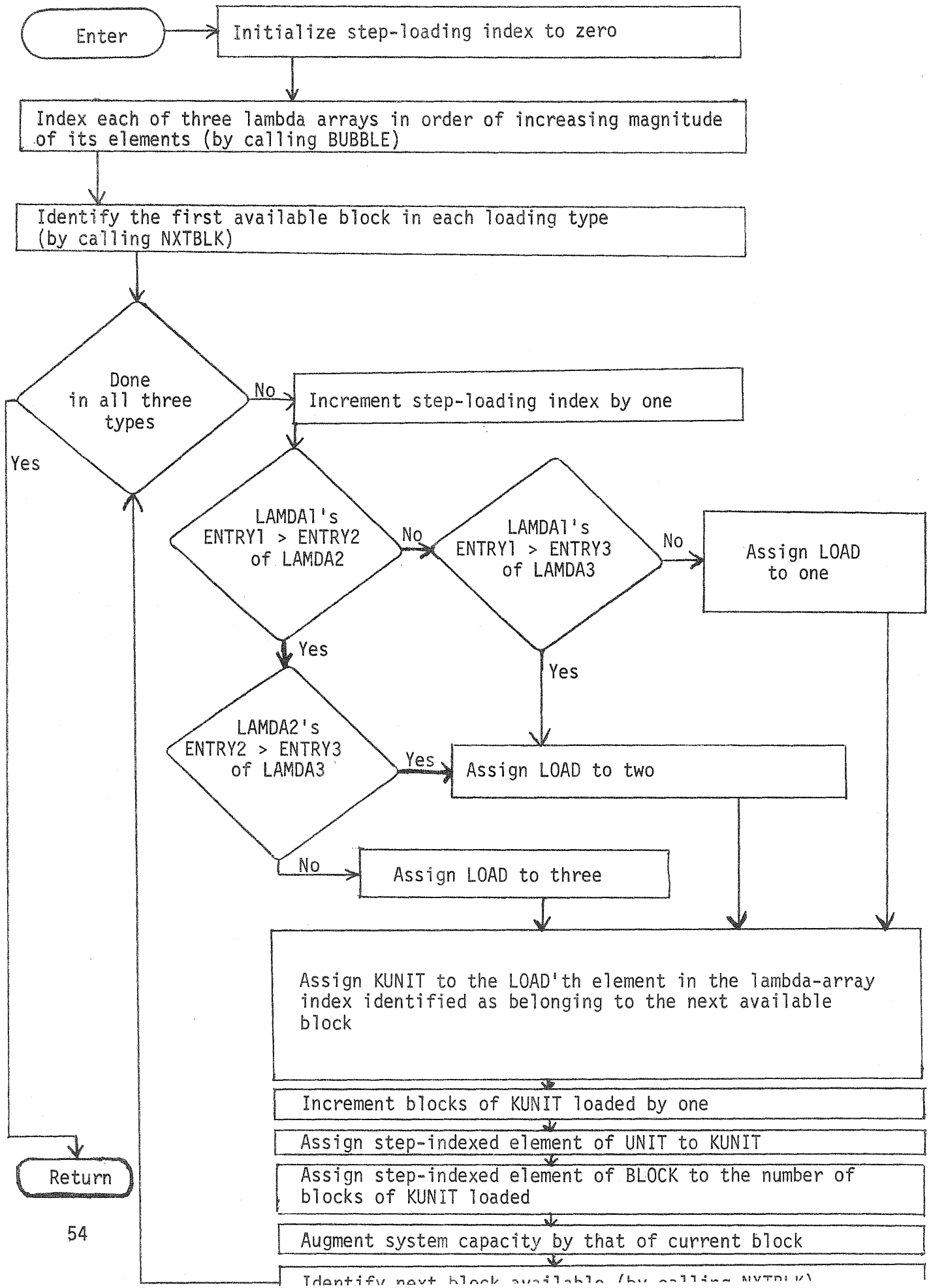
=====
C
C ROUTINE:          **** C O N V O L ****
C
C PURPOSE:
C   TO FORM A NEW EQUIVALENT LOAD-DURATION CURVE (Y) BY CONVOLUTION
C
C INPUT VARIABLES:
C   *Y              ORDINATES OF THE LOAD-PROBABILITY CURVE
C   X               ABSCISSAS OF THE LOAD-PROBABILITY CURVE
C   XMIN            MAXIMUM VALUE OF X FOR WHICH Y=1
C   XNZERO          MAXIMUM VALUE OF X FOR WHICH Y IS NON-ZERO
C   NPTS            LENGTH OF COLUMNS IN ARRAY Y
C   DELTA           STEP-SIZE FOR THE X-AXIS
C   CURRNT          1 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,1)
C                   2 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,2)
C   NEXT            1 IF NEXT COLUMN OF ORDINATES IS IN Y(*,1)
C                   2 IF NEXT COLUMN OF ORDINATES IS IN Y(*,2)
C   CAP             CAPACITY OF BLOCK INVOKING THE CONVOLUTION, IN MW
C   PAVAIL          AVAILABILITY PROBABILITY OF UNIT
C   MAXPTS          MAXIMUM NUMBER OF ORDINATES TO COMPUTE FOR NEXT CURVE
C
C   *VARIABLE IS BOTH INPUT/OUTPUT
C
C ALGORITHM:
C   CHRISTOS POSEIDON
C   CHAPTER 4 OF PHD DISSERTATION (UNPUBLISHED 1979)
C   THE OHIO STATE UNIVERSITY
C   DEPARTMENT OF NUCLEAR ENGINEERING
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, 2/16/79
C
C LAST REVISED: 10/79
=====

```

CREORD Routine

This routine steps through all available blocks in order of successive loading. At each step of the loading, one available block is identified from each of the three load-level categories. That block of the three having the lowest-value lambda is counted as loaded, and the next available block of the same load-level category is identified by the call to NXTBLK. When each of the three columns of lambdas is exhausted, the loading loop is complete.

CREORD




```

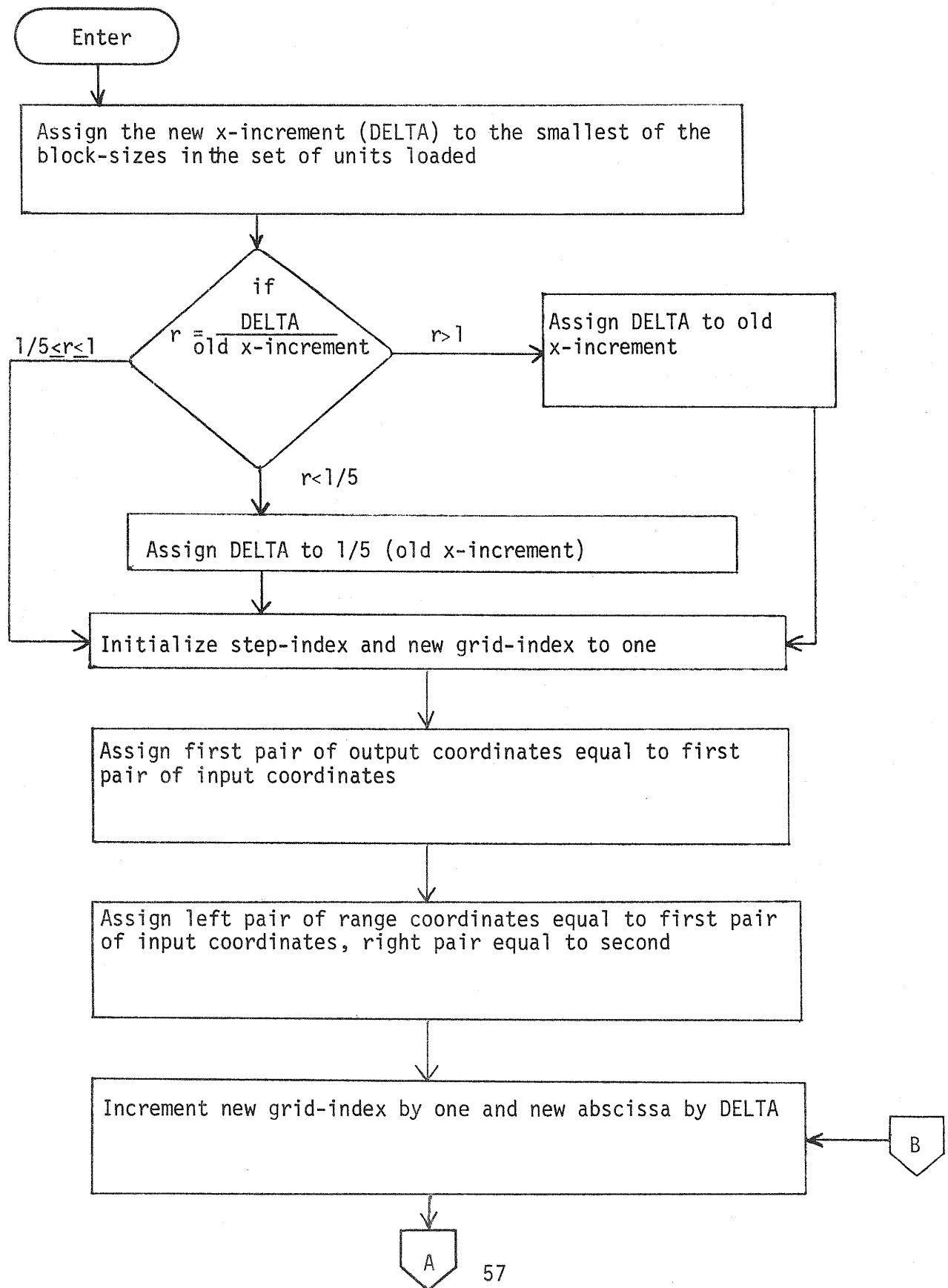
C=====
C
C ROUTINE:          **** C R E O R D ****
C
C PURPOSE:
C   TO CREATE A LOADING ORDER FOR THE SYSTEM AND TO FIND THE SYSTEM
C   CAPACITY.  THE LOADING ORDER IS CREATED BY LOADING THE NEXT
C   UNIT WHICH CORRESPONDS TO THE SMALLEST UNUSED LAMBDA VALUE.
C   AS BLOCKS OF UNITS ARE LOADED, THE UNIT LOADED IS RECORDED,
C   AN ARRAY OF BLOCK LOADING ORDER IS FORMED, THE BLOCK CAPACITY IS
C   RECORDED, AND THE TOTAL SYSTEM CAPACITY IS INCREMENTED.
C
C INPUT VARIABLES:
C   AVAIL           .TRUE. IF UNIT IS AVAILABLE TO GO ON-LINE
C                   .FALSE. IF UNIT IS NOT AVAILABLE TO GO ON-LINE
C   LAMDA1          FIRST BLOCK'S ORDINAL FOR LOADING
C   LAMDA2          SECOND BLOCK'S ORDINAL FOR LOADING
C   LAMDA3          THIRD BLOCK'S ORDINAL FOR LOADING
C   NUNITS          LENGTH OF LAMDA1, LAMDA2, LAMDA3 & AVAIL
C   MONTH           MONTH OF STUDY PERIOD
C   BLKCAP          CUMULATIVE BLOCK CAPACITIES FOR EACH UNIT, IN MW
C
C OUTPUT VARIABLES:
C   UNIT           UNIT LOADING ORDER
C   BLOCK          BLOCK LOADING ORDER
C   MWBLOK         CAPACITY OF BLOCKS LOADED, IN MW
C   K              NUMBER OF LOADING STEPS
C   SYSCAP         SYSTEM CAPACITY IN MW
C
C ROUTINES CALLED:
C   BUBBLE        NXTBLK
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====

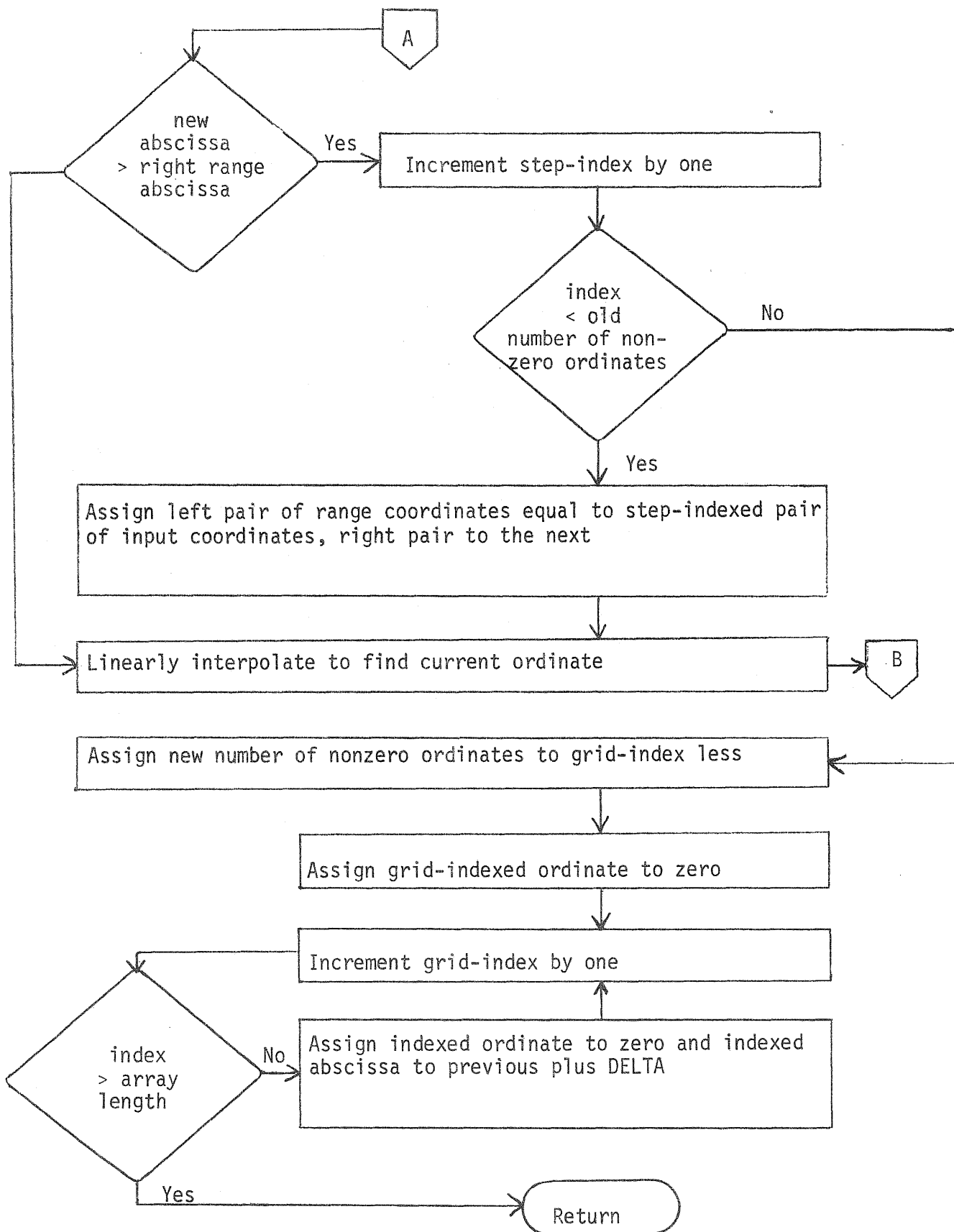
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CURVE Routine

This routine simply transfers the input load-duration curve (with x, y coordinates XAXIS1, ELC) to a new grid of coordinate pairs (XAXIS, ELCSVE). The grid increment DELTA is chosen as the smallest of the block capacities, and is further restricted to be in the range 20% to 100% of the spacing between abscissas of the input curve. Linear interpolation is used to assign ordinates to the new grid of points. Beyond the first zero on the input curve, corresponding output ordinates are assigned zero values. The number of non-zero ordinates (NZPNTS) is revised to describe the output array ELCSVE.

CURVE





```

C=====
C
C ROUTINE:          **** C U R V E ****
C
C PURPOSE:
C   GIVEN THE LOAD-PROBABILITY CURVE ELC, TO CREATE THE CURVE
C   ELCSVE WHICH IS UNIFORMLY SPACED ON THE X-AXIS BASED ON THE
C   SMALLEST LOADING BLOCK IN ARRAY MWBLOK
C
C INPUT VARIABLES:
C   ELC             ORDINATES OF UNMODIFIED LOAD-PROBABILITY CURVE
C   XAXIS           VALUES FOR LOAD-PROBABILITY CURVE ABSCISSAS
C   MWBLOK          CAPACITY OF BLOCKS LOADED, IN MW
C   NBLOCK          NUMBER OF BLOCKS TO LOAD
C   ELDCPT          NUMBER OF POINTS IN ARRAYS ELCSVE AND XAXIS
C   *NZPNTS        NUMBER OF NON-ZERO ORDINATES IN ELCSVE
C
C   *VARIABLE IS BOTH INPUT/OUTPUT
C
C OUTPUT VARIABLES:
C   ELCSVE          LOAD-PROBABILITY ORDINATES ON THE NEW GRID,
C                   FOR ABSCISSAS BETWEEN BASE LOAD AND PEAK LOAD (INCL)
C   XAXIS           LOAD-PROBABILITY ABSCISSAS ON THE NEW GRID
C   DELTA           STEP-SIZE FOR XAXIS ARRAY
C
C INTERNAL VARIABLES:
C   XLEFT,XRIGHT   X-AXIS INTERPOLATION END-POINTS
C   YLEFT,YRIGHT   Y-AXIS INTERPOLATION END-POINTS
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, MAY 1979
C
C LAST REVISED:  10/79
C=====

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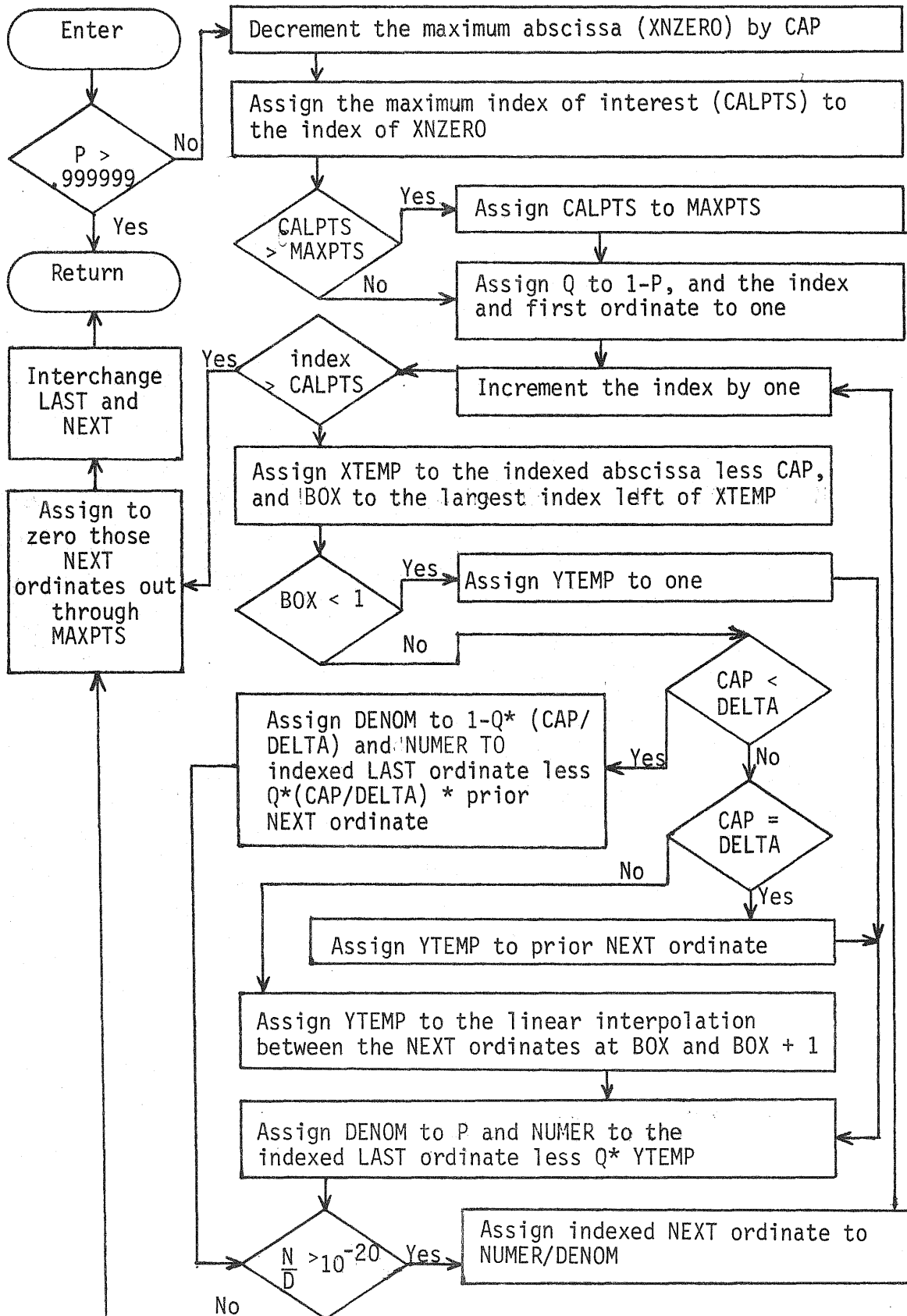
DECONF Routine

This routine performs the deconvolution of an aggregate capacity outage distribution function from the cumulative load probability distribution function stored in the LAST column of array Y. The aggregation is over blocks which operate or fail as a unit. Ordinates of the resultant function are stored in the NEXT column. The general equation used is that derived for the convolution process, but solved explicitly for the ordinates prior to convolution. Since the NEXT ordinates are computed recursively in ascending (forward) sequence of abscissas, errors due to roundoff in the early steps of the recursion process propagate with coefficient $-Q/P$; hence the process is unstable for availabilities (P) less than one-half. Use of double-precision merely delays the onset of significant error. The deconvolution of blocks with low availability is properly handled in a numerically stable manner by rearranging the equation such that the error propagates with coefficient $-P/Q$, as in the DECONR routine.

Those aggregate blocks having capacity (CAP) less than the grid-increment (DELTA) require the solution of an implicit equation for the NEXT ordinate. In all cases, ordinates are restricted to fall between unity and a positive threshold large enough to preclude underflow. The computation loop is aborted at the first violation of this threshold, and all remaining points are assigned to zero. To preserve the non-increasing characteristic of a valid load-probability distribution, each ordinate is restricted to be no greater than that to its left.

Each non-trivial execution of this routine causes the interchange of the numeric values in the LAST and NEXT variables, so that the ordinates just computed will be considered by the calling routine as the currently appropriate load-probability function.

DECONF



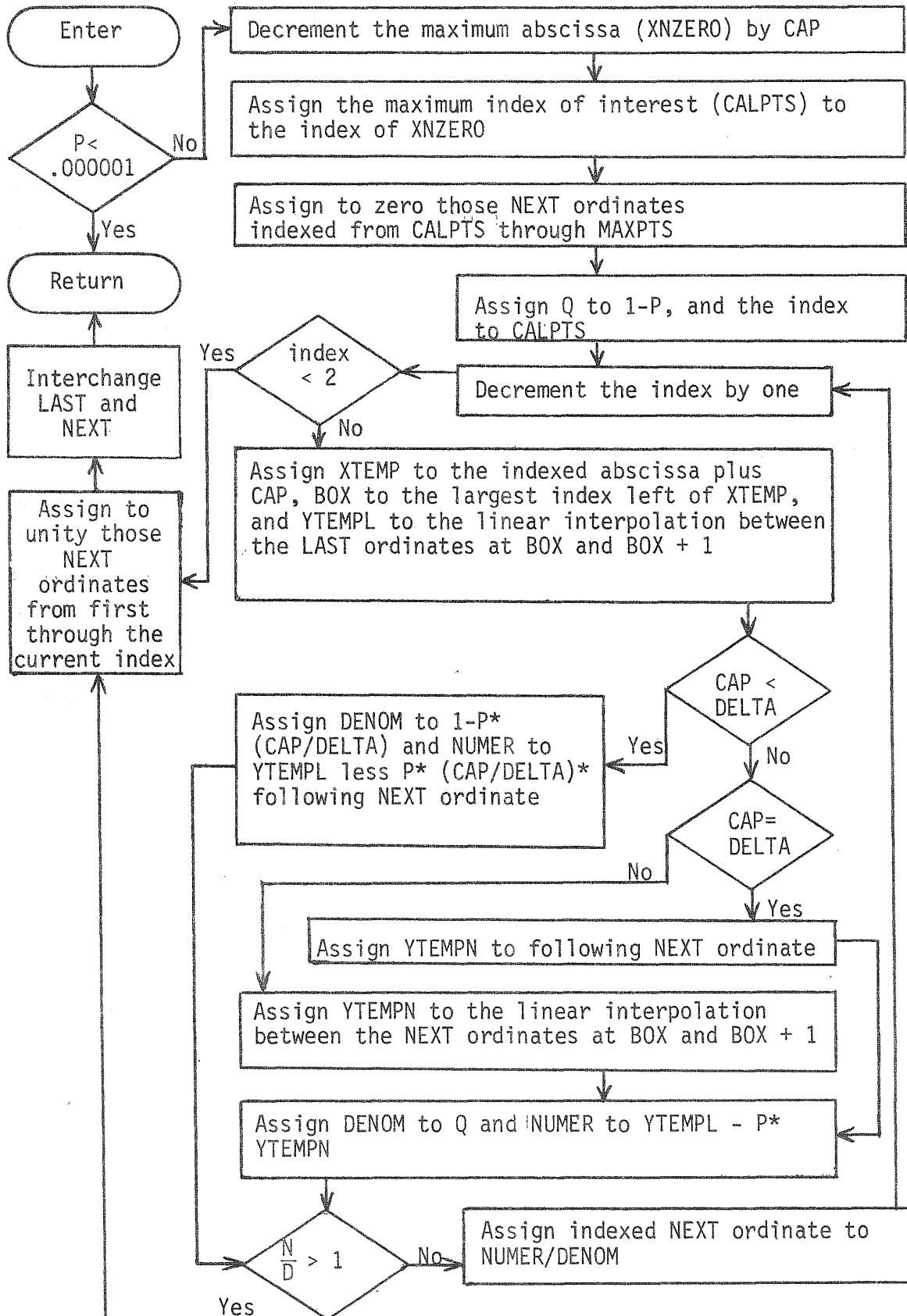
```

C=====
C
C ROUTINE:          **** D E C O N F ****
C
C PURPOSE:
C   TO REMOVE THE EFFECTS OF PRIOR-LOADED BLOCKS OF THE SAME
C   UNIT ON THE SHAPE OF THE LOAD-PROBABILITY CURVE, BY DECONVOLUTION
C   FROM LEFT TO RIGHT USING  $YNEXT(X)=(YLAST(X)-Q*YNEXT(X-CAP))/P$ 
C
C INPUT VARIABLES:
C   *Y              ORDINATES OF THE LOAD-PROBABILITY CURVE
C   X               ABSCISSAS OF THE LOAD-PROBABILITY CURVE
C   XMIN            MAXIMUM VALUE OF X FOR WHICH Y=1
C   DELTA           STEP-SIZE FOR THE X-AXIS
C   LAST           1 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,1)
C                 2 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,2)
C   NEXT           1 IF NEXT COLUMN OF ORDINATES IS IN Y(*,1)
C                 2 IF NEXT COLUMN OF ORDINATES IS IN Y(*,2)
C   CAP             CAPACITY OF PREVIOUS BLOCKS TO BE DECONVOLVED
C   P              AVAILABILITY OF UNIT
C   NPTS           LENGTH OF COLUMNS OF ARRAY Y
C   MAXPTS         MAXIMUM NUMBER OF ORDINATES TO COMPUTE FOR NEXT CURVE
C   XNZERO         MAXIMUM VALUE OF X FOR WHICH Y IS NON-ZERO
C
C   *VARIABLE IS BOTH INPUT/OUTPUT
C
C ALGORITHM:
C   (NUMERICALLY STABLE FOR  $P>0.5$ )
C   CHRISTOS POSEIDON
C   CHAPTER 4 OF PHD DISSERTATION (UNPUBLISHED 1979)
C   THE OHIO STATE UNIVERSITY
C   DEPARTMENT OF NUCLEAR ENGINEERING
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====

```


DECONR Routine

This routine is syntactically similar to DECONF, as it performs deconvolution according to the same basic equation. Here, however, the NEXT ordinates are computed recursively in descending (reverse) sequence of abscissas so that roundoff errors do not propagate; this routine is called only when the propagation coefficient ($-P/Q$) is of fractional magnitude. The reversed processing order implies the following differences from the forward order: no check is needed for negative indices, since the aggregate block capacity is added to indexed abscissas instead of subtracted; the loop is aborted at the first computed ordinate greater than unity; and each ordinate is restricted to be no less than that to its right.



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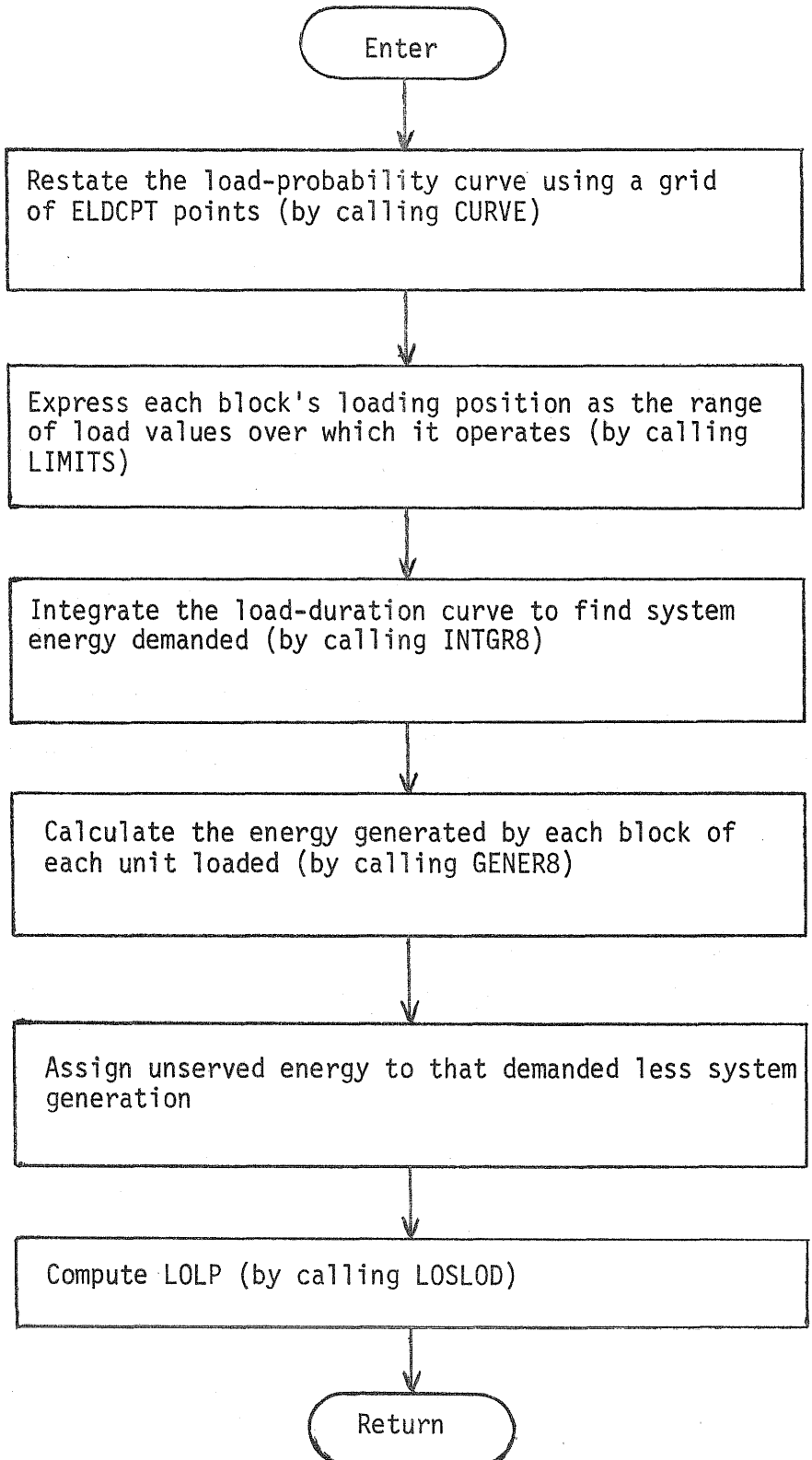
C=====
C
C ROUTINE:          **** D E C O N R ****
C
C PURPOSE:
C   TO REMOVE THE EFFECTS OF PRIOR-LOADED BLOCKS OF THE SAME
C   UNIT ON THE SHAPE OF THE LOAD-PROBABILITY CURVE, BY DECONVOLUTION
C   FROM RIGHT TO LEFT USING YNEXT(X)=(YLAST(X+CAP)-P*YNEXT(X+CAP))/Q
C
C INPUT VARIABLES:
C   *Y             ORDINATES OF THE LOAD-PROBABILITY CURVE
C   X              ABSCISSAS OF THE LOAD-PROBABILITY CURVE
C   XMIN           MAXIMUM VALUE OF X FOR WHICH Y=1
C   DELTA          STEP-SIZE FOR THE X-AXIS
C   LAST           1 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,1)
C                  2 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,2)
C   NEXT           1 IF NEXT COLUMN OF ORDINATES IS IN Y(*,1)
C                  2 IF NEXT COLUMN OF ORDINATES IS IN Y(*,2)
C   CAP            CAPACITY OF PREVIOUS BLOCKS TO BE DECONVOLVED
C   P              AVAILABILITY OF UNIT
C   NPTS           LENGTH OF COLUMNS OF ARRAY Y
C   MAXPTS         MAXIMUM NUMBER OF ORDINATES TO COMPUTE FOR NEXT CURVE
C   XNZERO         MAXIMUM VALUE OF X FOR WHICH Y IS NON-ZERO
C
C   *VARIABLE IS BOTH INPUT/OUTPUT
C
C ALGORITHM:
C   (NUMERICALLY STABLE FOR P<0.5)
C   COMPLEMENT OF THAT IN ROUTINE DECONF
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, OCTOBER 1979
C=====

```

ENERGY Routine

This routine supervises calculations of monthly energy-related values that form the basis of the production-cost reports: system-wide energy demanded, unserved energy, and the energy generated by each block loaded. The system's generation reliability (LOLP) is computed using single-block loading to minimize errors in the convolution process and to reflect the full availability of hydro units in meeting peak demands.

ENERGY



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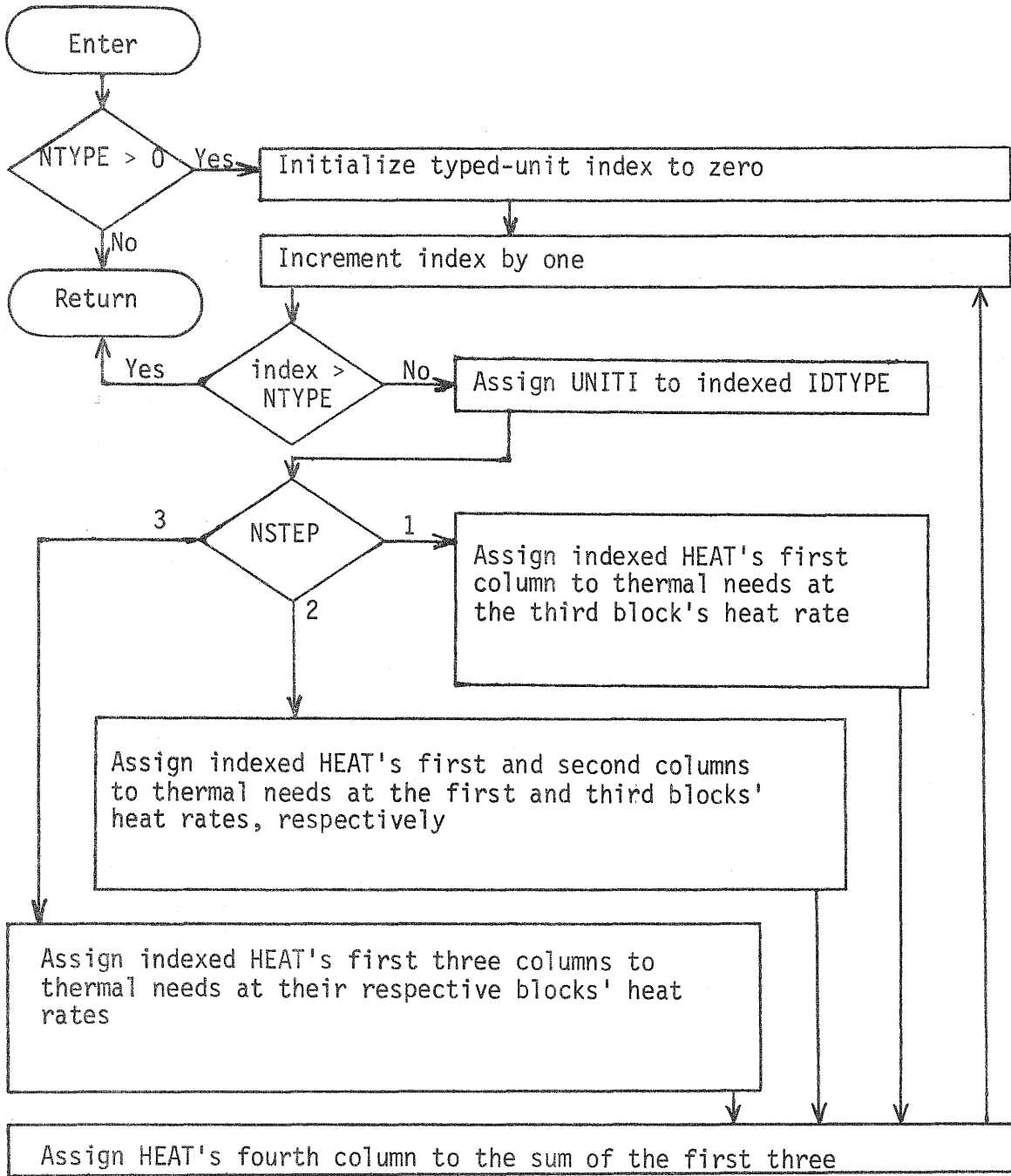
=====
C
C ROUTINE:          **** E N E R G Y ****
C
C PURPOSE:
C   GIVEN A SYSTEM LOAD-PROBABILITY CURVE (ELC), TO PROJECT THE ENERGY
C   GENERATED BY EACH UNIT IN THE SYSTEM, RELIABILITY (LOLP),
C   AND THE AMOUNT OF PURCHASED POWER NEEDED TO MEET SYSTEM DEMANDS.
C
C INPUT VARIABLES:
C   ELC             ORDINATES OF UNMODIFIED LOAD-PROBABILITY CURVE
C   XAXIS1          VALUES FOR LOAD-PROBABILITY CURVE ABSCISSAS
C   ELCPTS          NUMBER OF POINTS IN ELC AND XAXIS1
C   UNIT           LOADING ORDER OF UNITS
C   BLOCK          LOADING ORDER OF BLOCKS
C   MWBLOK         CAPACITY OF BLOCKS LOADED, IN MW
C   EAVAIL         EFFECTIVE AVAILABILITY BY UNIT
C   NBLOCK         NUMBER OF BLOCKS TO LOAD
C   SYSCAP         TOTAL SYSTEM CAPACITY IN MW
C   HOURS          NUMBER OF HOURS IN STUDY PERIOD
C   MONTH          MONTH OF STUDY
C   HYDROS         LOGICAL FOR CONDITION OF HYDROS IN SYSTEM
C   UNTYPE         TYPE OF GENERATION UNIT: 1-STEAM FOSSIL, 2-STEAM NUCLEAR,
C                 3-I.C. ENGINE, 4-GAS TURBINE, 5-JET ENGINE, 6-HYDRO,
C                 7-PUMPED STORAGE
C   UNGEN          THE EXPECTED GENERATION BY EACH HYDRO UNIT
C   IDHYDRO        LOCATION OF THE HYDRO UNIT IN THE ORDER READ
C   NHYDRO         NUMBER OF HYDRO UNITS
C
C OUTPUT VARIABLES:
C   LOLP           LOSS OF LOAD PROBABILITY (0 < LOLP < 1)
C   SYSGEN         TOTAL SYSTEM ENERGY
C   UNSERV         UNSERVED ENERGY
C   ENRGEE         ENERGY BY BLOCK LOADED
C
C VARIABLES INTERNAL TO ENERGY AND THE SUBROUTINES IT CALLS:
C   ELDC           ORDINATES OF CALCULATED LOAD PROBABILITY CURVE
C   XAXIS          THE X AXIS DEMAND VALUES FOR ELDC & ELCSVE
C   ELCSVE         ORDINATES OF THE NEW LOAD PROBABILITY
C                 CURVE COMPUTED IN SUBROUTINE CURVE
C   ELDCPT         NUMBER OF POINTS IN ARRAYS ELDC, XAXIS, AND ELCSVE
C   NZPNTS        NUMBER OF NON-ZERO ORDINATES IN ELCSVE
C
C ROUTINES CALLED:
C   CURVE   LIMITS   INTGR8   GENER8   LOSLOD
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, 2/22/79
C
C LAST REVISED: 10/79
=====

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FINDHT Routine

This routine simply computes the thermal-energy requirements (HEAT) array to correspond with the specified heat-rate for each block and the electrical energy generated by that block. Since thermal energy is reported in millions of British thermal units (MBTU), a conversion factor of .001 is included to cancel the units on the other factors: $(\text{BTU}/\text{KWH}) * (\text{MWH}) = \text{KBTU} * (\text{MBTU}/(1000 * \text{KBTU})) = .001 \text{ MBTU}$. Here M is consistently used to represent million (mega-), in distinction from the confusing convention of using MMBTU for million BTU.

FINDHT




```
C=====
C
C ROUTINE:          **** F I N D H T ****
C
C PURPOSE:
C   TO CALCULATE THE THERMAL ENERGY FOR BLOCKS OF A GIVEN LOADING
C   TYPE AND THE TOTAL THERMAL ENERGY FOR THE UNIT.
C
C INPUT VARIABLES:
C   IDTYPE  INDEX OF UNITS OF SPECIFIED TYPE, IN THE ORDER READ
C   NTYPE   NUMBER OF UNITS LOADED OF SPECIFIED TYPE
C   NSTEP   NUMBER OF LOADING-STEPS USED FOR THIS LOADING TYPE
C   HEATR1  HEAT RATE IN BTU/KWH OF FIRST BLOCK, BY UNIT
C   HEATR2  HEAT RATE IN BTU/KWH OF SECOND BLOCK, BY UNIT
C   HEATR3  HEAT RATE IN BTU/KWH OF THIRD BLOCK, BY UNIT
C   ENRGE2  ENERGY GENERATED BY UNITS, BY COLUMNS: 1-FIRST BLOCK,
C           2-SECOND BLOCK, 3-THIRD BLOCK, 4-TOTAL FOR UNIT
C
C OUTPUT VARIABLES:
C   HEAT    THERMAL ENERGY REQUIREMENTS BY UNITS, BY COLUMNS:
C           1-FIRST BLOCK, 2-SECOND BLOCK, 3-THIRD BLOCK,
C           4-TOTAL FOR UNIT
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====
```

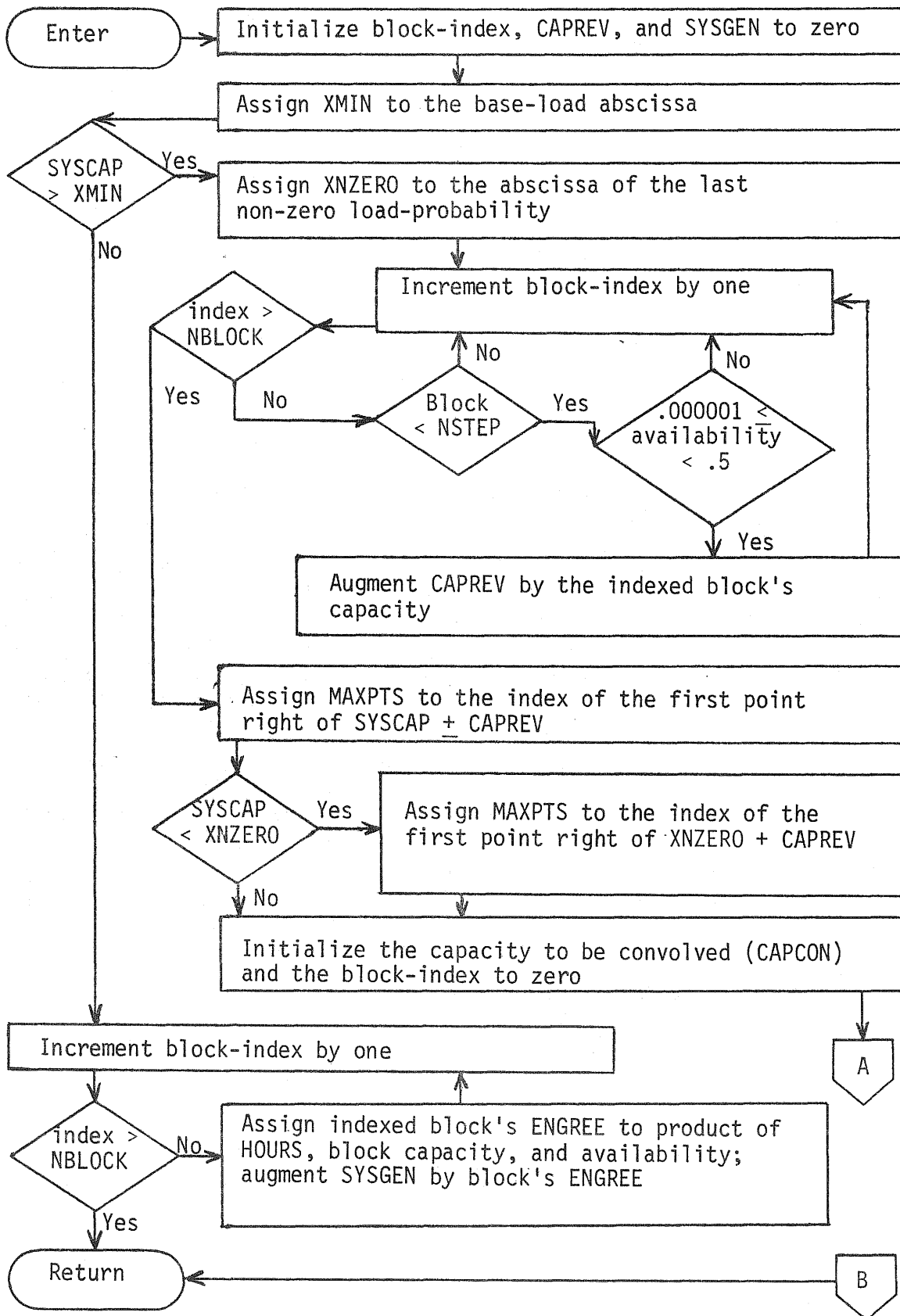
GENER8 Routine

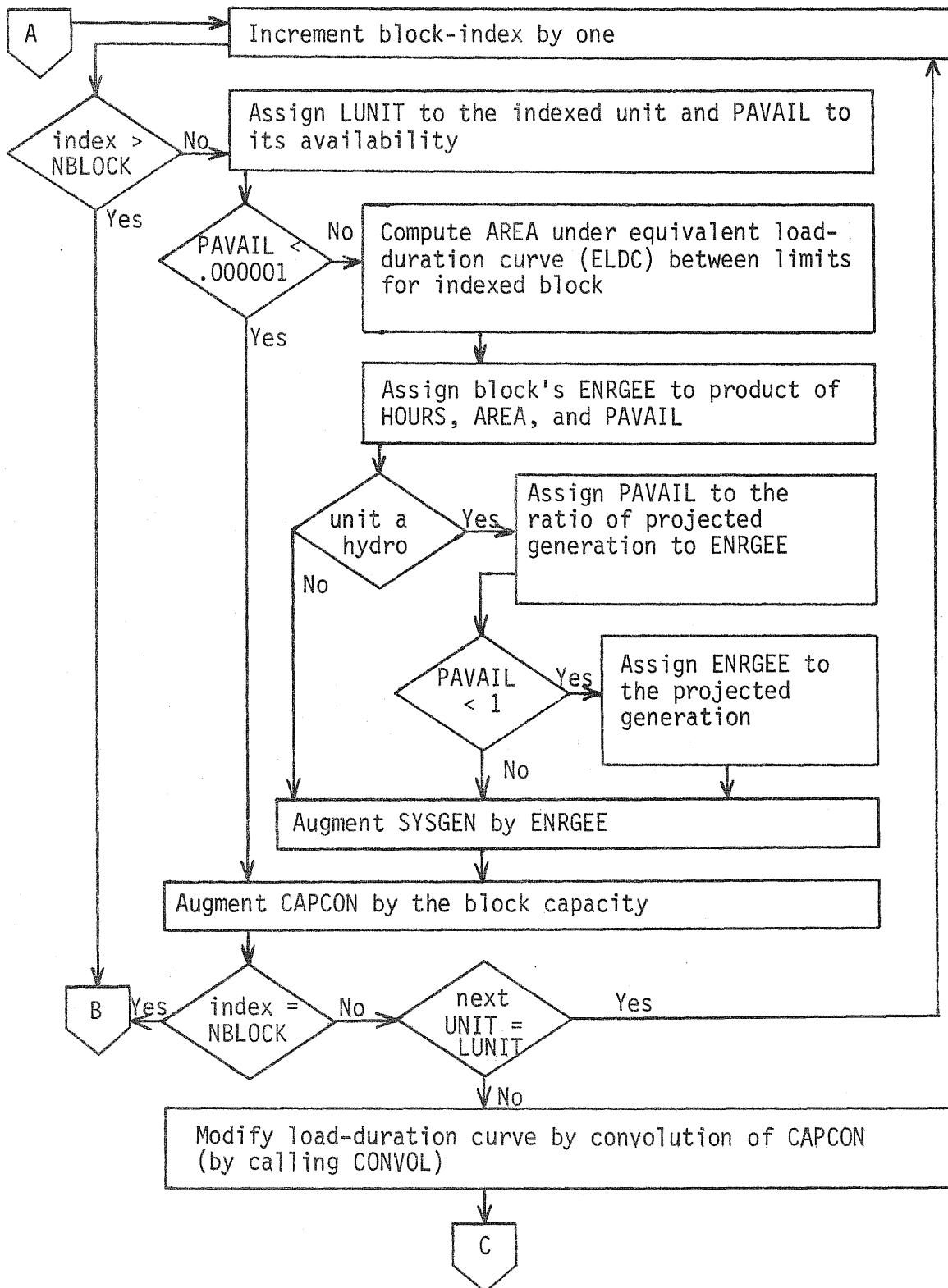
This routine is responsible for the computation of the electrical energy generated by each block in the loading order. The load-duration curve appropriate for the integration of a block's energy is that original load-duration curve modified by the convolution of the outage distribution functions of all independent blocks that had been loaded prior to the current blocks. The requirement of independence means that all prior-loaded blocks which operate or fail as a unit with the current block, must have their outage distribution functions ignored in the computation of the current block's energy. Since the routine stores the cumulative effects of all prior-loaded blocks' outages in the current column of the equivalent load-duration curve (ELDC) array, and since convolution is a commutative (order-independent) operation, deconvolution may be invoked to remove outage effects from prior-loaded blocks of the current unit. Following the energy calculation for a unit's secondary or tertiary block, that block's capacity is aggregated with the sum capacity of the units' prior-loaded blocks for the convolution, regardless of adjacency of blocks. Appropriate steps have been taken to avoid convolution and deconvolution for blocks with unit or zero availability (since, in neither case should the ELDC be affected) and to treat adjacent blocks of a common unit as an aggregate for the purposes of convolution.

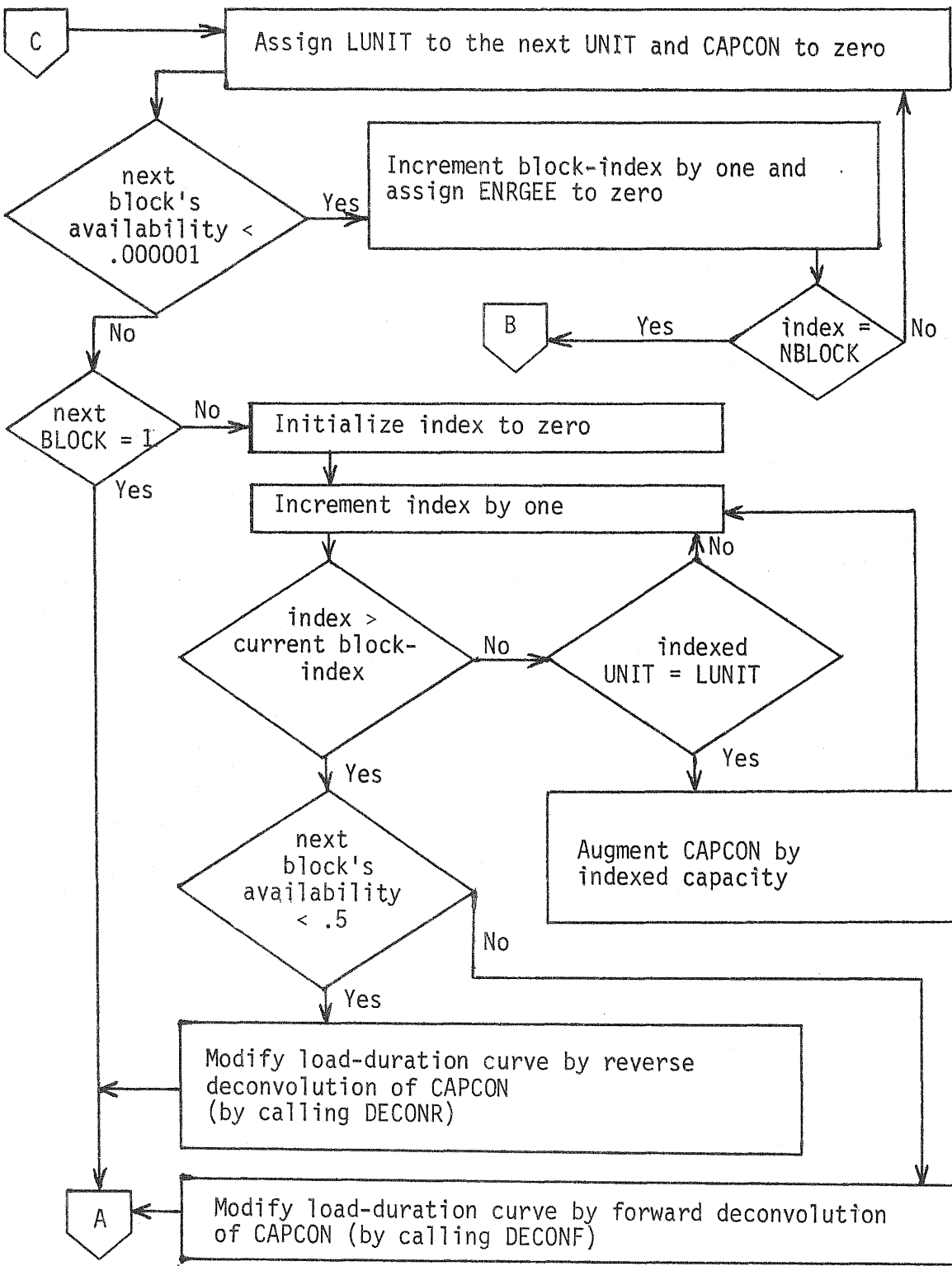
The avoidance of deconvolution for the first block of any unit implies that blocks within a single unit must be loaded in ascending order; neither the second nor third block may have a lambda value lower than the first block's lambda.

The early return due to base-load (XMIN) exceeding system capacity (SYSCAP) is included for use with degenerate cases of input data; it is not expected to be exercised by normal utility system's data. Since the load-duration curve had been normalized to one (time unit), the area under any portion of its base-load section is simplified to the range of integration.

GENER8







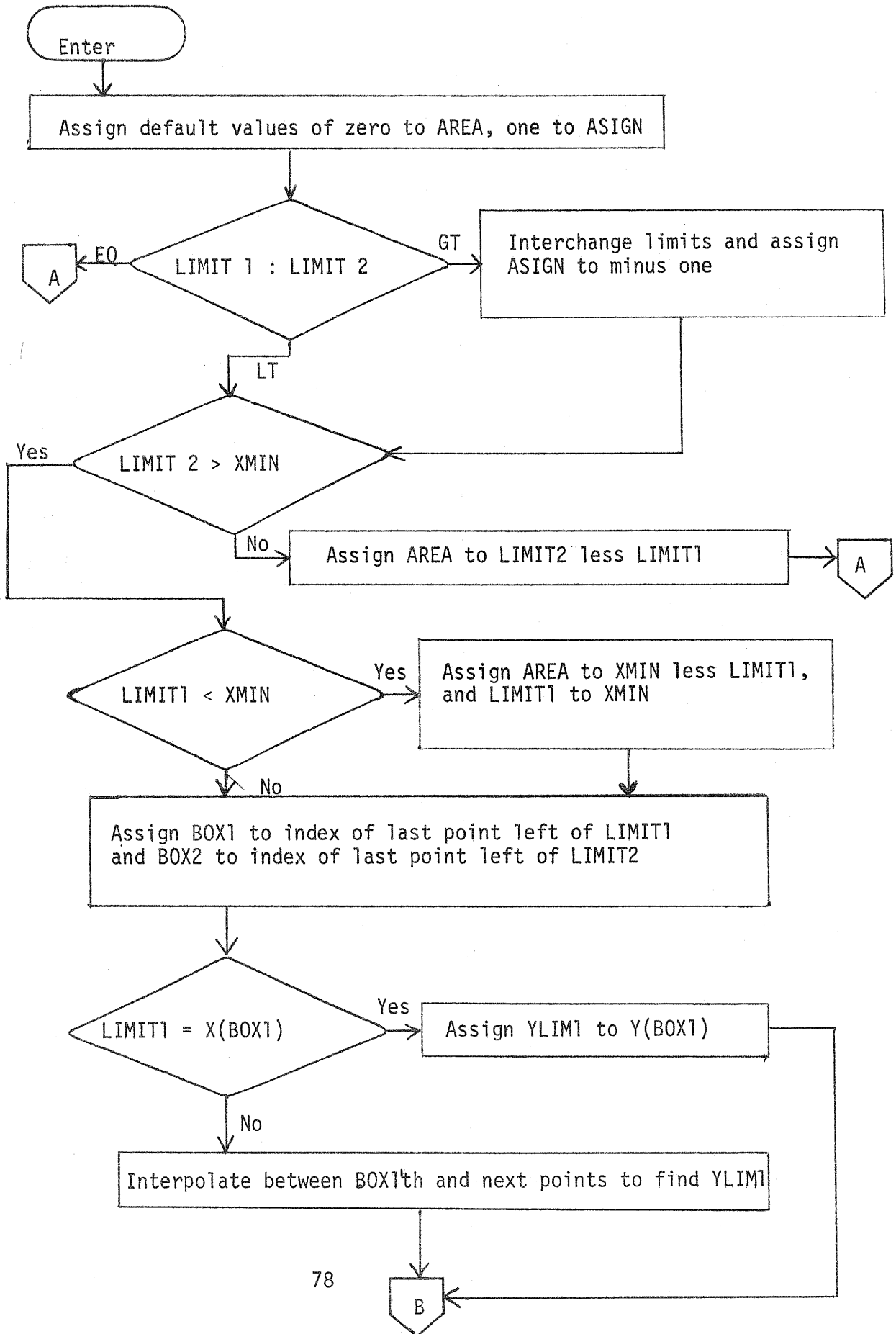
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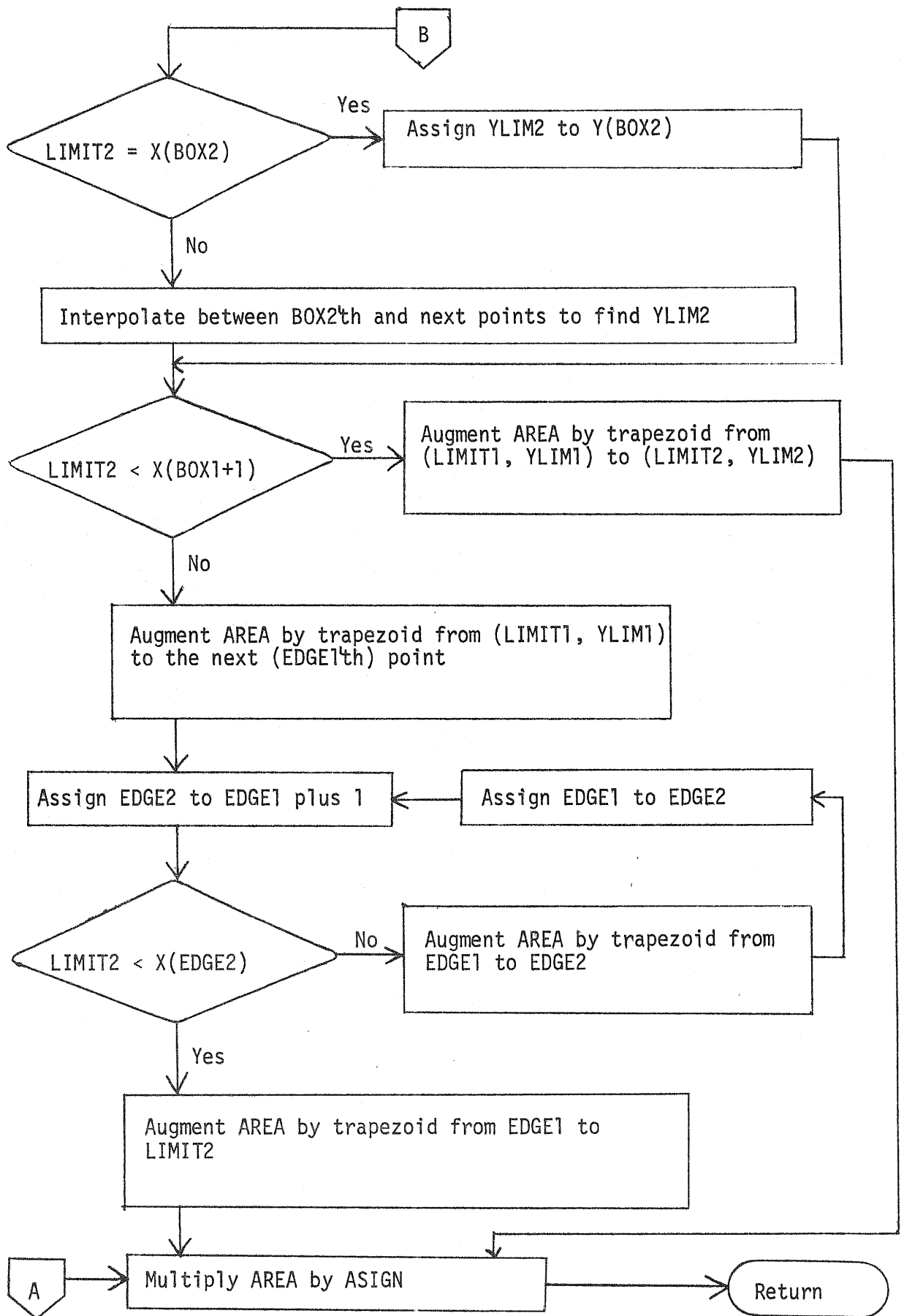
C=====
C
C ROUTINE:          **** G E N E R 8 ****
C
C PURPOSE:
C   TO CALCULATE GENERATION IN MWH FOR EACH BLOCK LOADED
C
C INPUT VARIABLES:
C   ELDC           ORDINATES OF CALCULATED LOAD-PROBABILITY CURVE
C   XAXIS          ORDINATES OF LOAD-PROBABILITY CURVE
C   DELTA          STEP-SIZE FOR ARRAY XAXIS
C   EAVAIL         EFFECTIVE AVAILABILITY BY UNIT
C   MONTH         MONTH OF STUDY
C   UNIT          LOADING ORDER OF UNITS
C   MWBLOK        CAPACITY OF BLOCKS LOADED, IN MW
C   BLOCK         LOADING ORDER OF BLOCKS
C   NBLOCK        NUMBER OF BLOCKS TO LOAD
C   LIMITA        LEFT-HAND INTEGRATION LIMITS BY BLOCK
C   LIMITB        RIGHT-HAND INTEGRATION LIMITS BY BLOCK
C   HOURS         NUMBER OF HOURS IN MONTH
C   ELDCPT        NUMBER OF POINTS IN ARRAYS ELDC AND XAXIS
C   NZPNTS        NUMBER OF NON-ZERO ORDINATES IN ELDC'S COLUMNS
C   UNLOAD        LOADING TYPE OF UNIT:  1-BASE, 2-CYCLING, 3-PEAKING,
C                 4-HYDRO
C   NSTEP         NUMBER OF LOADING STEPS FOR THE FOUR TYPES OF UNITS
C
C OUTPUT VARIABLES:
C   ENRGEE        GENERATION OF EACH BLOCK, IN MWH
C   SYSGEN        TOTAL SYSTEM GENERATION, IN MWH
C
C ROUTINES CALLED:
C   INTGR8        CONVOL   DECONF   DECONR
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, MAY 1979
C
C LAST REVISED:  10/79
C=====

```

INTGR8 Routine

This routine performs trapezoidal integration of the area under the curve $Y(X)$, where $X(I)$ and $Y(I,J)$ are both arrays of coordinates; the second subscript on Y allows reference to more than one curve by the calling statement. Since the ordinates for abscissas from zero through $XMIN$ are assumed to be unity, the area of integrals over portions of that range is simply the difference of the integration limits. Beyond $XMIN$, the piecewise-linear representation of the curve justifies the sufficiency of the trapezoidal approach. Each trapezoid is no wider than the increment between values of X ; for integration limits non-coincident with the x -grid, linear interpolation is used to compute the corresponding ordinates.





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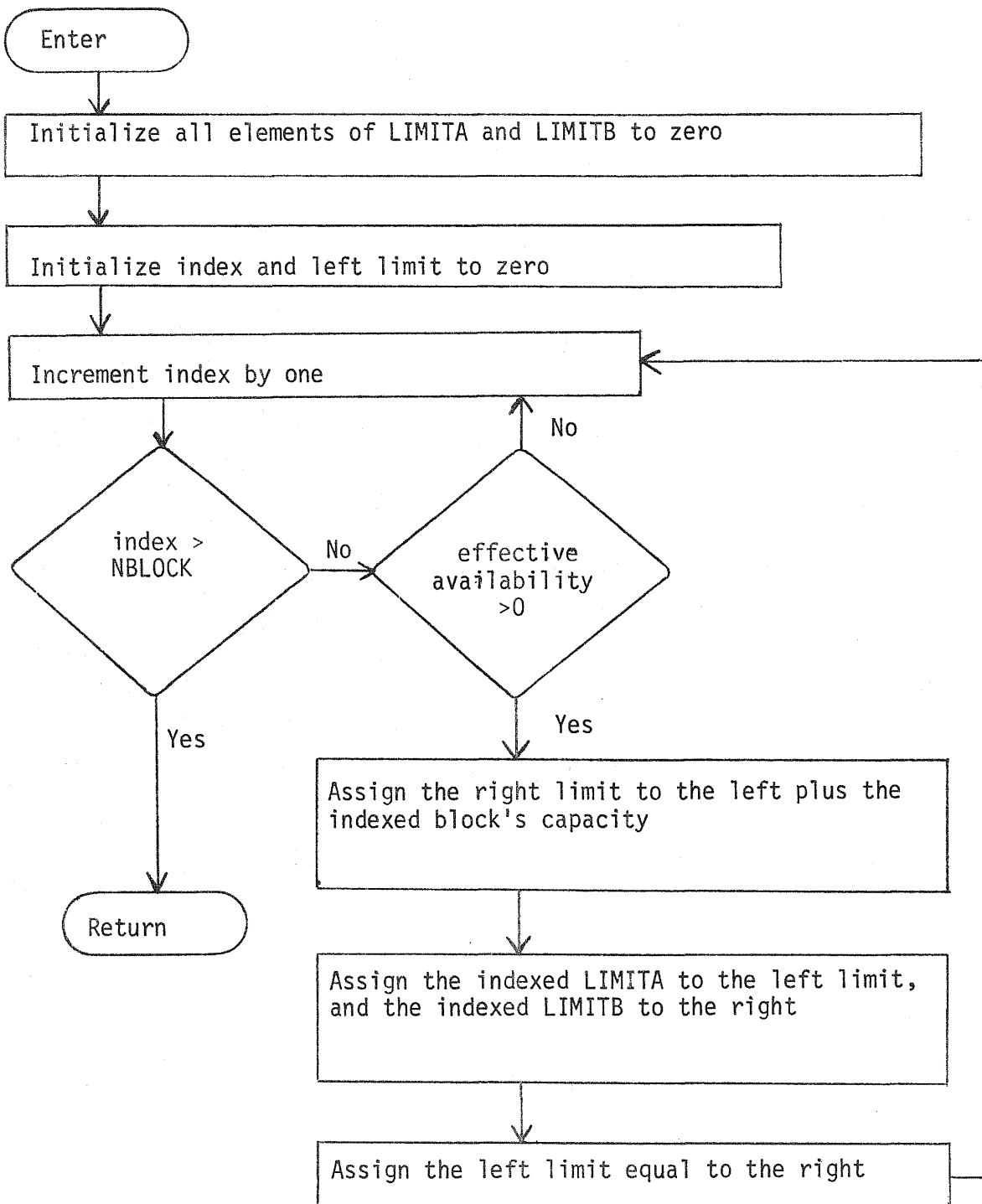
C=====
C
C ROUTINE:          **** I N T G R 8 ****
C
C PURPOSE:
C   TO FIND THE AREA UNDER THE CURVE Y(X) FROM LIMITA TO LIMITB
C
C INPUT VARIABLES:
C   Y               ORDINATES OF THE LOAD-PROBABILITY CURVE TO BE INTEGRATED
C   CURRNT          IF 1, USE THE CURVE IN Y(*,1)
C                  IF 2, USE THE CURVE IN Y(*,2)
C   NPTS           NUMBER OF VALUES IN ONE COLUMN OF Y
C   X              ABSCISSAS OF THE LOAD-PROBABILITY CURVE
C   XMIN           MAXIMUM VALUE OF X FOR WHICH Y=1
C   DELTA          STEP-SIZE FOR THE X-AXIS
C   LIMITA         ABSCISSA WHERE INTEGRATION BEGINS
C   LIMITB        ABSCISSA WHERE INTEGRATION ENDS
C
C OUTPUT VARIABLES:
C   AREA          AREA UNDER Y FROM LIMITA TO LIMITB
C
C NOTES:
C   ROUTINE WILL HANDLE THE FOLLOWING CONDITIONS DIFFERENTLY
C
C       LIMIT1 < LIMIT2
C       LIMIT1 = LIMIT2
C       LIMIT1 > LIMIT2
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====

```

LIMITS Routine

This routine steps through the blocks of units in the loading order, assigning left and right load-axis end-points for later use as the range of integration for each block. The end-points are defined as the extremes of system demand over which the block would be partially loaded.

LIMITS



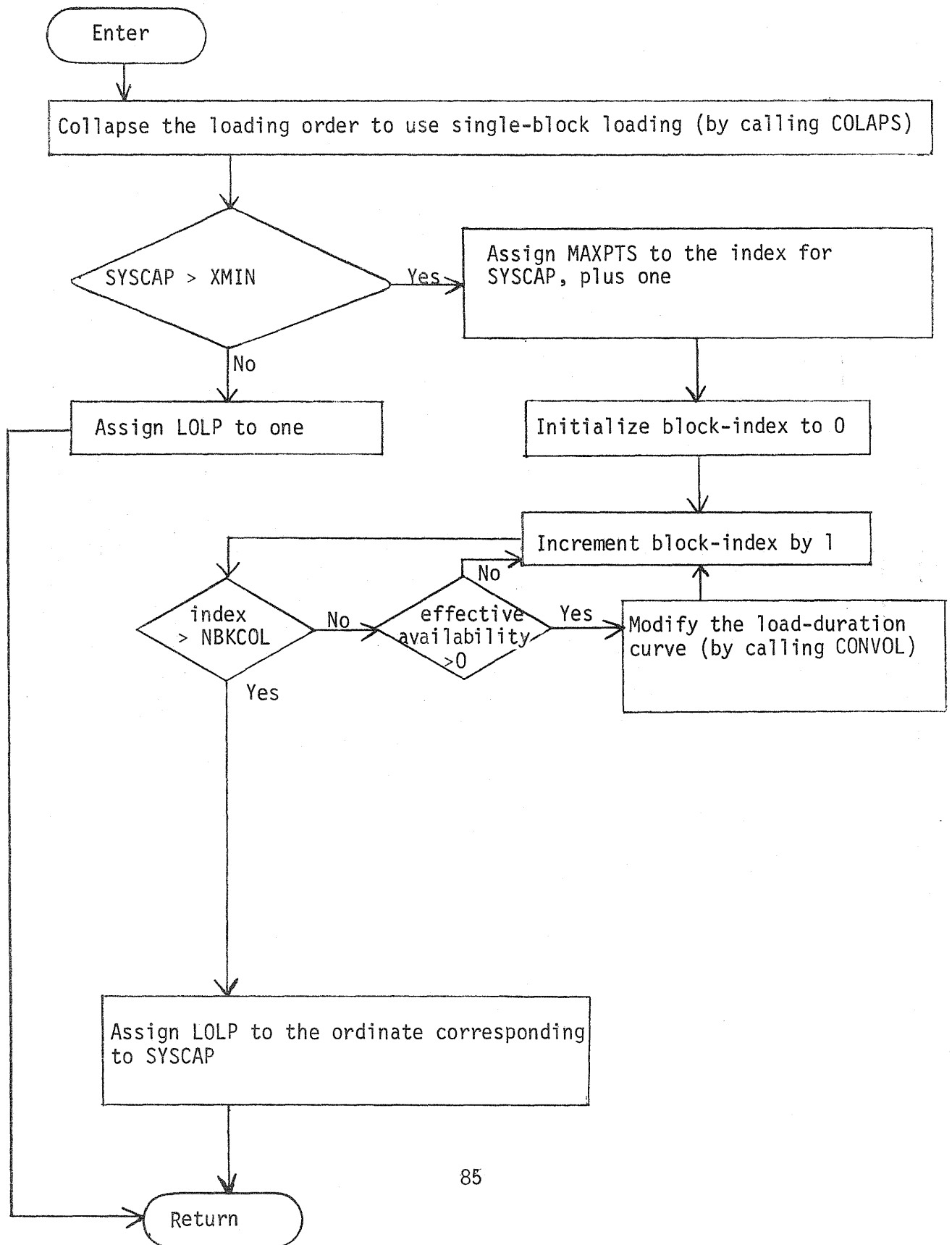
```
C=====
C
C ROUTINE:          **** L I M I T S ****
C
C PURPOSE:
C   TO FIND AND STORE THE LIMITS OF INTEGRATION FOR
C   EACH LOADING BLOCK OF EACH UNIT
C
C INPUT VARIABLES:
C   MWBLOK          CAPACITY OF BLOCKS LOADED, IN MW
C   NBLOCK          NUMBER OF BLOCKS TO LOAD
C   UNIT            LOADING ORDER OF UNITS
C   BLOCK           LOADING ORDER OF BLOCKS
C   EAVAIL          EFFECTIVE AVAILABILITY BY UNIT
C   MONTH           MONTH OF STUDY
C   SYSCAP          TOTAL SYSTEM CAPACITY IN MW
C
C OUTPUT VARIABLES:
C   LIMITA          LEFT-HAND INTEGRATION LIMIT
C   LIMITB          RIGHT-HAND INTEGRATION LIMIT
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, MAY 1979
C
C LAST REVISED:   10/79
C=====
```

LOSL0D Routine

This routine computes the system reliability (or loss-of-load probability, LOLP) as that ordinate on the system's equivalent load-duration curve (ELDC) corresponding to an abscissa equal to system capacity. Although the system's ELDC had been developed in routine GENER8, the treatment of hydro units as having limited availability and the multi-block loading used with deconvolution of lower-order units resulted in distortions of the curve's shape. To avoid such distortions, the system's ELDC is regenerated from the original curve (ELCSVE), incorporating each unit (up to three blocks operating or failing together) by a single convolution (call to CONVOL). This is accomplished by collapsing the loading-order to that implied by single-block loading, then cycling through the number of aggregate blocks (NBKCOL), modifying the ELDC at each pass.

The early return with LOLP assigned to one is included for use with degenerate cases of input data; it is not expected to be exercised by normal utility systems' data.

LOSLOD



```

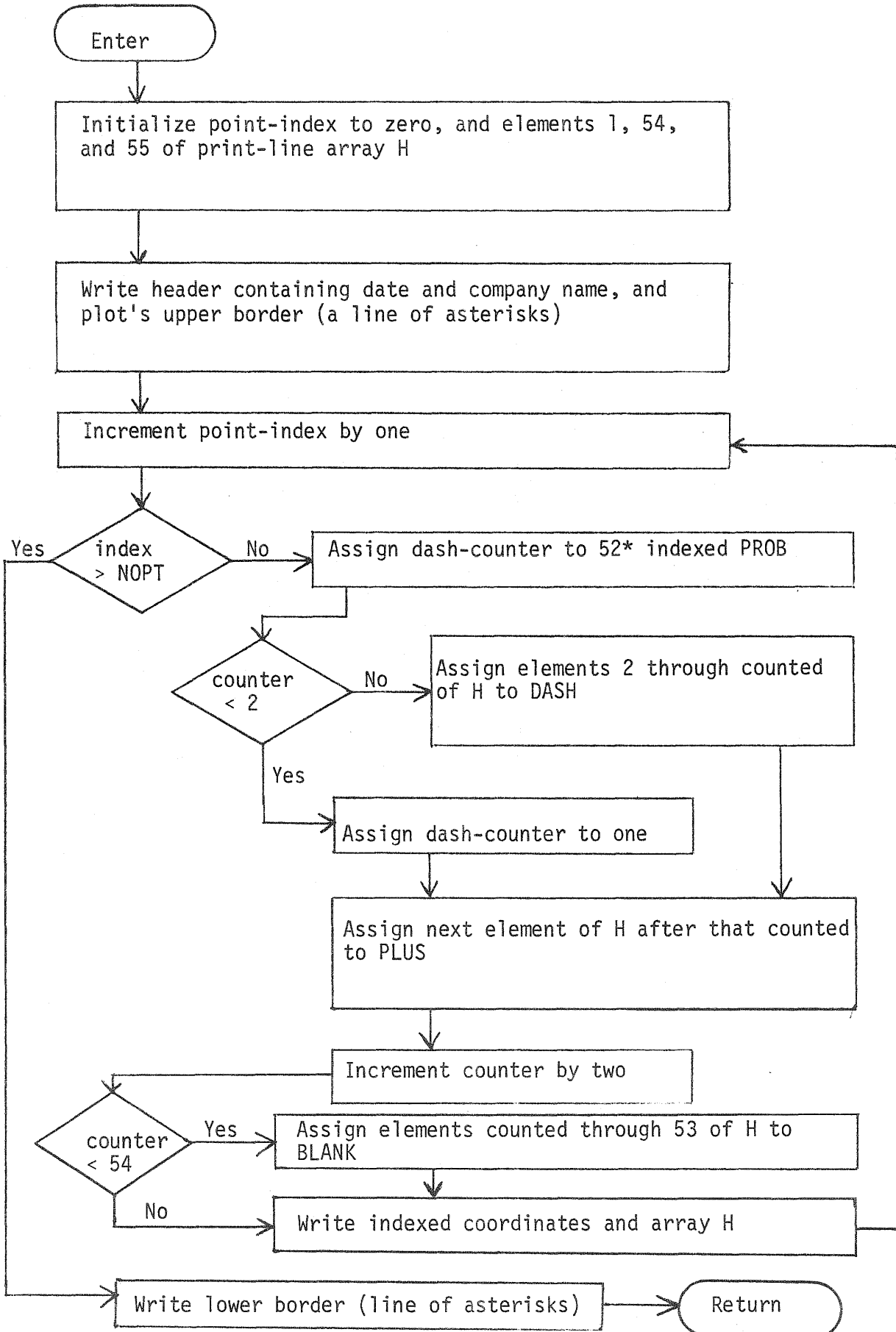
=====
C
C ROUTINE:          **** L O S L O D ****
C
C PURPOSE:
C   TO CALCULATE THE LOSS-OF-LOAD PROBABILITY FOR THE GENERATING SYSTEM
C
C INPUT VARIABLES:
C   ELDC           ORDINATES OF CALCULATED LOAD-PROBABILITY CURVE
C   DELTA          STEP-SIZE FOR THE X-AXIS
C   XAXIS          VALUES FOR LOAD-PROBABILITY CURVE ABSCISSAS
C   ELDCPT         NUMBER OF POINTS IN ARRAYS ELDC AND XAXIS
C   NZPNTS        NUMBER OF NON-ZERO ORDINATES IN ELDC
C   UNIT          LOADING ORDER OF UNITS
C   BLOCK          LOADING ORDER OF BLOCKS
C   MWBLOK        CAPACITY OF BLOCKS LOADED, IN MW
C   EAVAIL        EFFECTIVE AVAILABILITY BY UNIT
C   NBLOCK        NUMBER OF BLOCKS TO LOAD
C   SYSCAP        TOTAL SYSTEM CAPACITY IN MW
C   MONTH         MONTH OF STUDY
C   CURRNT        1 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,1)
C                 2 IF CURRENT COLUMN OF ORDINATES IS IN Y(*,2)
C   NEXT          1 IF NEXT COLUMN OF ORDINATES IS IN Y(*,1)
C                 2 IF NEXT COLUMN OF ORDINATES IS IN Y(*,2)
C
C OUTPUT VARIABLES:
C   LOLP          LOSS OF LOAD PROBABILITY (0 < LOLP < 1)
C
C INTERNAL VARIABLES:
C   UNCOL         LOADING ORDER ARRAY COLLAPSED BY SINGLE-BLOCK UNITS
C   NBKCOL        NUMBER OF BLOCKS IN THE COLLAPSED ORDER
C   BOX           ARRAY POSITION WHERE SYSTEM CAPACITY FALLS
C   K             INDEX USED FOR BLOCK-LOOPING
C   MAXPTS        MAXIMUM NUMBER OF ORDINATES TO BE CALCULATED
C   PAVAIL        UNIT AVAILABILITY
C   XNZERO        MAXIMUM ABSCISSA FOR WHICH Y IS NOT ZERO
C
C ROUTINES CALLED:
C   COLAPS       CONVOL
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, MAY 1979
C
C LAST REVISED: 10/79
=====

```


LPLOT Routine

This routine generates a crude plot of the NOPT coordinates on the unmodified load-probability curve as passed by routine RDPROB. Each coordinate-pair is printed on the same line as a sequence of one asterisk (STAR) and hyphens (DASH) representing the magnitude of the ordinate (PROB). The hyphens are terminated by a plus-sign (PLUS) in the position (J) corresponding to the smallest integer exceeding 52 times the ordinate. Thus a plus-sign preceded by an asterisk and no hyphens would be printed for an ordinate of zero; for an ordinate of 0.499, twenty-four hyphens would precede the plus-sign; for 0.500, twenty-five hyphens. If the left-hand column of asterisks is considered the x-axis (corresponding to zero probability for a continuous curve), the subjective effect of the plus-sign assignment is to overstate the ordinates by up to one increment. To read the plot accurately, one must recall the assignment algorithm, which effectively locates the ordinate only as lying somewhere on the range of one increment preceding the plus-sign. If great significance will be placed on the plotted points, one may remove the subjective bias by subtracting 0.5 in the dash-counter assignment statement. If the resultant dash-counter (IN) is less than one, the flow should branch directly to the plus-sign assignment. This would, more conventionally, represent zero ordinates by a plus-sign in the first possible position, overwriting the asterisk.

LPLOT

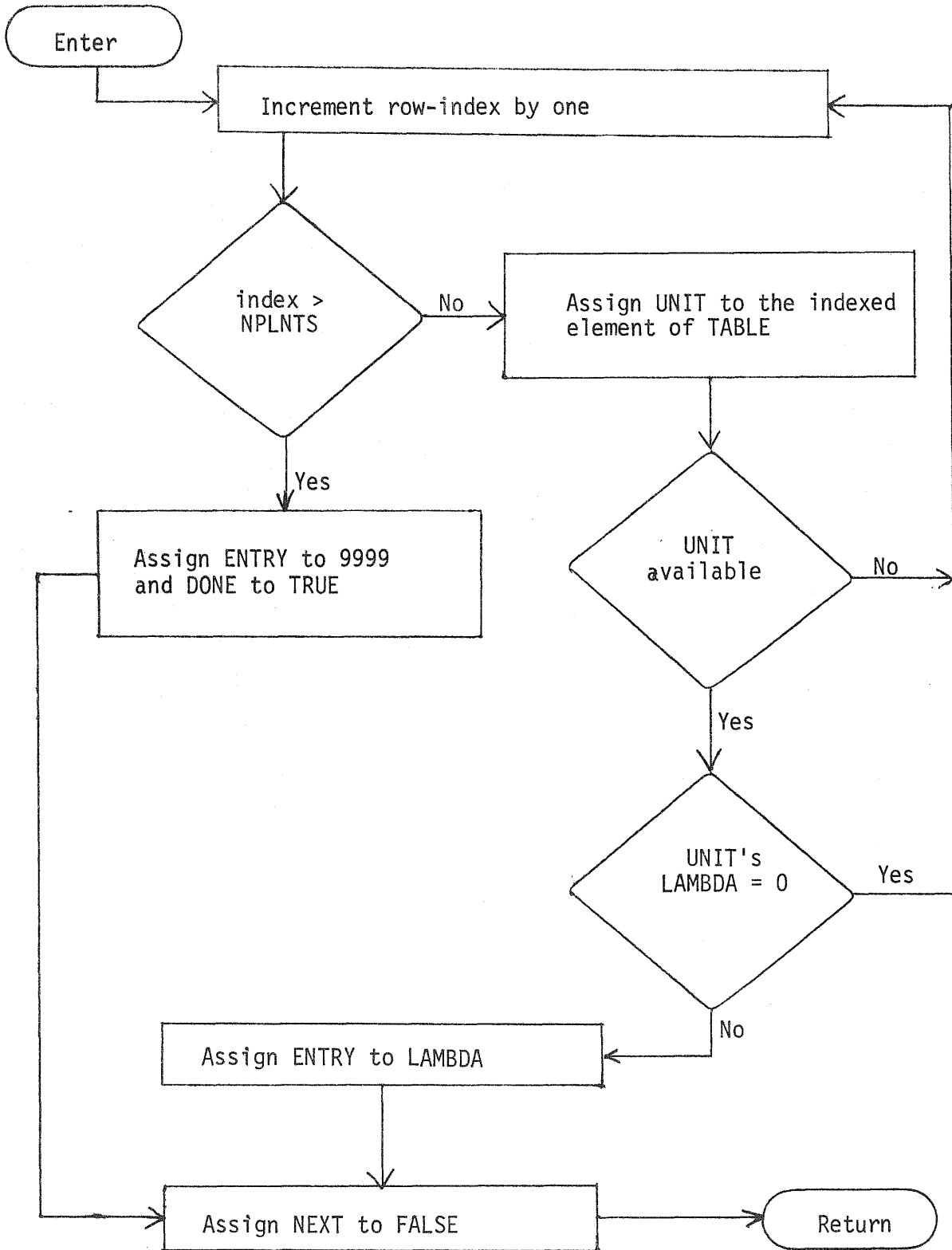


```
C=====
C
C ROUTINE:          **** L P P L O T ****
C
C PURPOSE:
C   TO PLOT THE LOAD-PROBABILITY CURVE USING NOPT POINTS
C
C INPUT VARIABLES:
C   LODVAL          X-AXIS LOAD VALUES
C   PROB            Y-AXIS PROBABILITY VALUES
C   NOPT            NUMBER OF (NON-ZERO) POINTS TO BE PLOTTED
C   MONTH           MONTH OF STUDY (1-12)
C   IYEAR           YEAR OF STUDY
C   COMPNA          COMPANY NAME
C   FILE            LOGICAL UNIT ON WHICH POINTS ARE TO BE PLOTTED
C
C NOTES:
C   ADAPTED FROM AN EARLIER VERSION FOR THE PUBLIC UTILITIES COMMISSION
C   OF OHIO
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:   10/79
C=====
```

NXTBLK Routine

This routine simply scans forward in the array TABLE until a unit is found which is available during the current month and has non-zero priority (LAMDA). When the COL column of TABLE is exhausted, the value of ENTRY is returned as 9999 to allow it to function in the numerical comparisons of CREORD without the possibility of being the smallest among the three considered.

NXTBLK



```

C=====
C
C ROUTINE:          **** N X T B L K ****
C
C PURPOSE:
C   TO FIND THE NEXT AVAILABLE BLOCK WHICH IS TO BE LOADED.
C   THE CONDITIONS FOR BEING LOADED ARE THAT THE CORRESPONDING
C   LAMBDA VALUE MUST NOT EQUAL 0 AND THAT THE BLOCK MUST BE
C   AVAILABLE DURING THIS SECTION OF THE STUDY.
C
C INPUT VARIABLES:
C   AVAIL           .TRUE. IF UNIT IS AVAILABLE
C                   .FALSE. IF UNIT IS NOT AVAILABLE
C   NUNITS          LENGTH OF AVAIL, TABLE & LAMBDA
C   TABLE          INDEX TABLE TO BE SEARCHED
C   LAMBDA          BLOCKS' LOADING-ORDER INDICES
C   POINTR          ROW IN TABLE WHERE THE SEARCH BEGINS
C   COL             COLUMN OF TABLE TO USE
C   MONTH           MONTH OF STUDY PERIOD
C
C OUTPUT VARIABLES:
C   DONE            .TRUE. IF NO MORE BLOCKS TO LOOK FOR IN TABLE
C                   .FALSE. IF MORE BLOCKS STILL UNLOADED
C   NEXT            .FALSE. TO INDICATE THAT THIS ROUTINE WAS CALLED
C   POINTR          UPDATED ROW-LOCATION OF THE CURRENT BLOCK
C   ENTRY           VALUE OF THE LAMBDA FOR THE UNIT
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE, FEBRUARY 1979
C
C LAST REVISED:  10/79
C=====

```

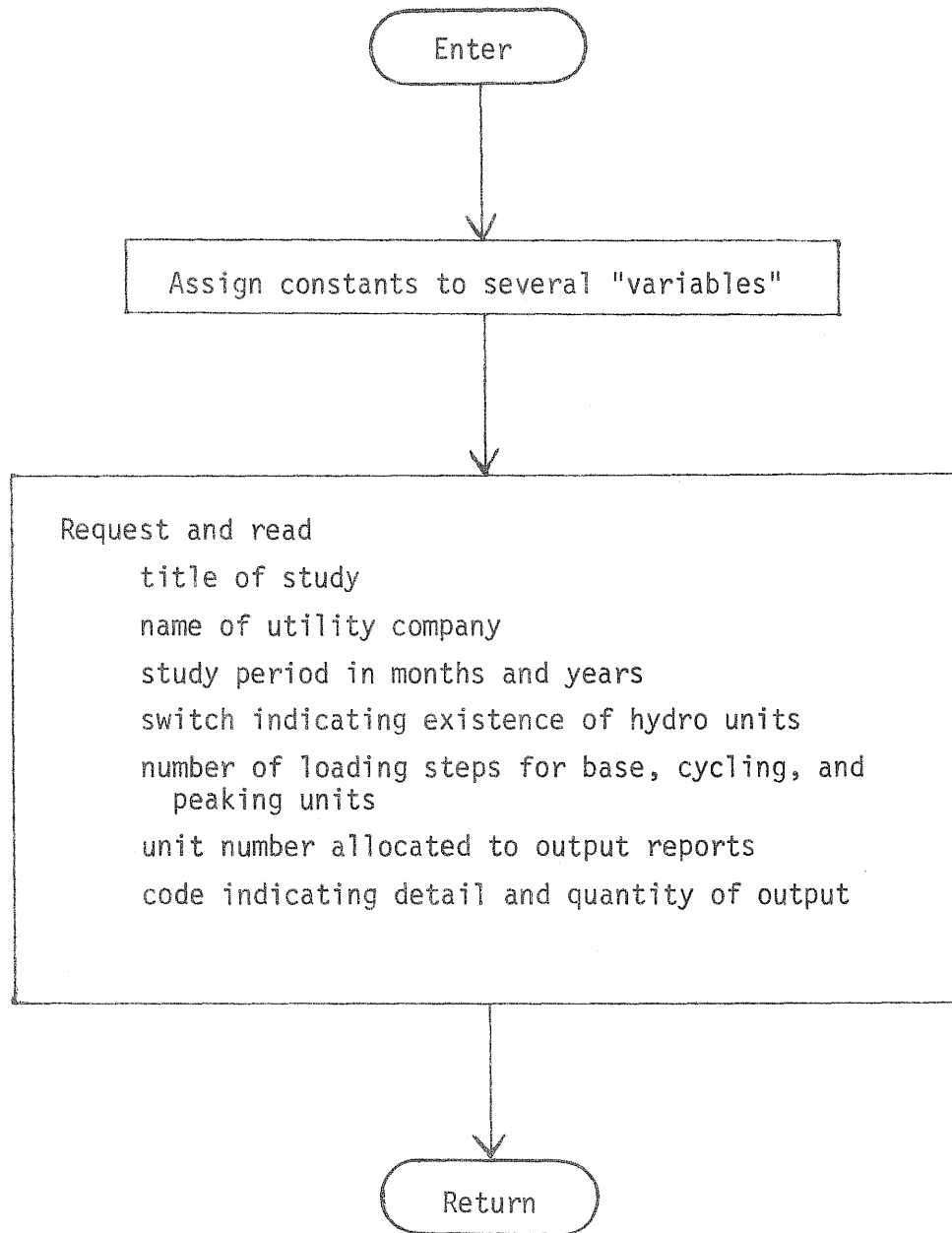
RDPARM Routine

This routine currently uses a machine-dependent free-form READ statement (interpreting blanks and commas as field delimiters) for several variables. To eliminate ambiguity in some of the field-widths expected, and to allow operation at other installations, recommended formats and corresponding numeric examples are given for these variables:

MONTH1	I2	01
YEAR1	I4	1977
MONTH2	I2	06
YEAR2	I4	1978
NBSTEP, NCSTEP, NPSTEP	3I2	030303
SUNIT	I2	15
OPTION	I1	2

Note that the current program array dimensions limit the number of loading steps (NBSTEP, NCSTEP, NPSTEP) to three.

RDPARM




```

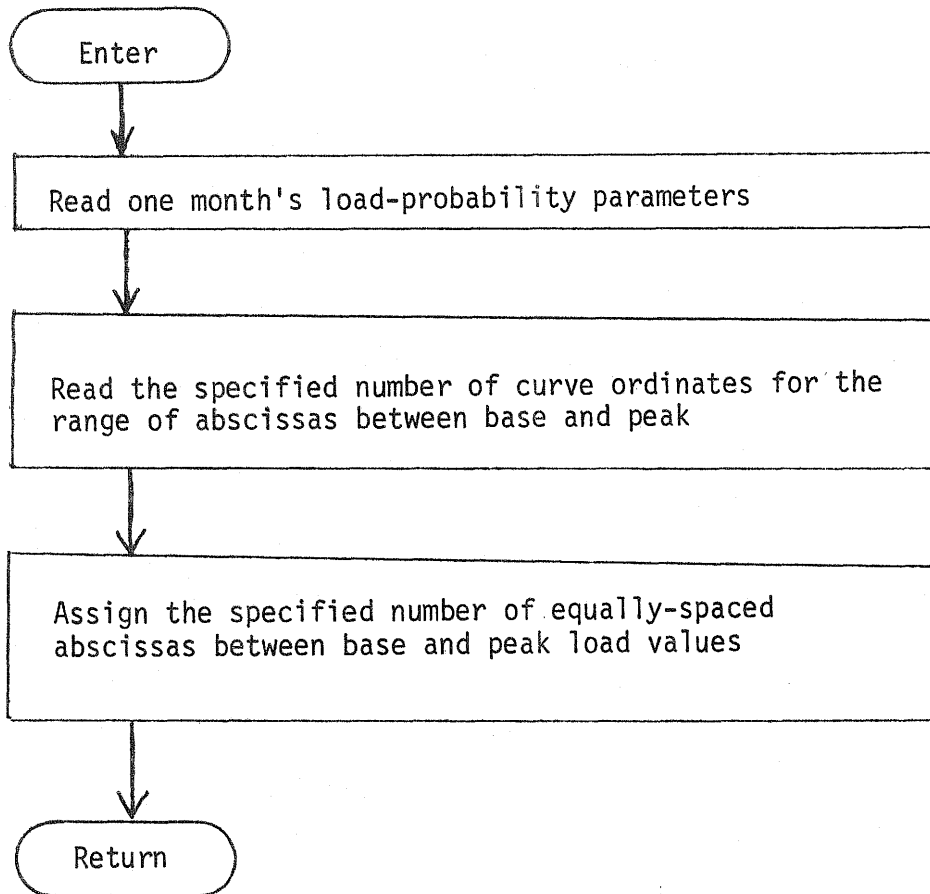
C=====
C
C ROUTINE:          **** R D P A R M ****
C
C PURPOSE:
C   TO READ IN THE PROGRAM PARAMETERS DESCRIBED IN THE OUTPUT
C   SECTION BELOW
C
C INPUT VARIABLES:
C   NONE
C
C OUTPUT VARIABLES:
C   HYDROS          .FALSE. IF NO HYDRO UNITS
C                   .TRUE. IF HYDRO UNIT INFORMATION IS TO BE READ
C   HYUNIT          LOGICAL UNIT FROM WHICH TO READ HYDRO INFO
C   PFUNIT          LOGICAL UNIT FROM WHICH TO READ FOSSIL INFO
C   PBUNIT          LOGICAL UNIT FROM WHICH TO READ LOAD-PROBABILITY CURVE
C   MUNIT           LOGICAL UNIT TO WHICH TO WRITE MONTHLY REPORT
C   QUNIT           LOGICAL UNIT TO WHICH TO WRITE QUARTERLY REPORT
C   AUNIT           LOGICAL UNIT TO WHICH TO WRITE ANNUAL REPORT
C   SUNIT           LOGICAL UNIT TO WHICH TO WRITE FUEL-USAGE SUMMARY
C   MONTH1         FIRST MONTH OF STUDY
C   MONTH2         LAST MONTH OF STUDY
C   YEAR1           FIRST YEAR OF STUDY
C   YEAR2           LAST YEAR OF STUDY
C   NBSTEP         NUMBER OF BASE UNIT LOADING STEPS
C   NCSTEP         NUMBER OF CYCLE UNIT LOADING STEPS
C   NPSTEP         NUMBER OF PEAKER UNIT LOADING STEPS
C   COMPNA         COMPANY NAME
C
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====

```

RDPROB Routine

The NOPT ordinates on the monthly load-probability curve read by this routine must correspond to NOPT (implicit) load values equally spaced between the base and peak values, inclusive. In addition to the coordinates for the probability curve, the routine returns values, as read, for the number of hours covered and the energy generation in the current month.

RDPROB



```

C=====
C
C ROUTINE:          **** R D P R O B ****
C
C PURPOSE:
C   TO READ THE LOAD PROBABILITY DATA SUPPLIED BY THE COMPANY AND TO
C   CALCULATE THE LOAD VALUES FOR EACH INPUT VALUE.
C
C INPUT VARIABLES:
C   PBUNIT   LOGICAL UNIT FROM WHICH TO READ THE LOAD-PROBABILITY DATA
C   HRSIP    HOURS IN EACH PERIOD COVERED
C   GENMO    ENERGY GENERATION IN EACH PERIOD
C
C OUTPUT VARIABLES:
C   LODVAL   X-AXIS LOAD VALUES
C   PROB     Y-AXIS PROB VALUES
C   NOPT     NUMBER OF DATA POINTS
C   BASE     BASE LOAD FOR EACH PERIOD
C   PEAK     PEAK LOAD FOR EACH PERIOD
C   DELTA    LOAD VALUE INCREMENT
C   IFLAG    0 IF CURVE WAS READ FROM PBUNIT
C             1 IF CURVE WAS NOT ON UNIT PBUNIT
C
C NOTES:
C   THE PROGRAM WILL END ABNORMALLY IF AN END-OF-FILE IS
C   ENCOUNTERED PREMATURELY.
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====

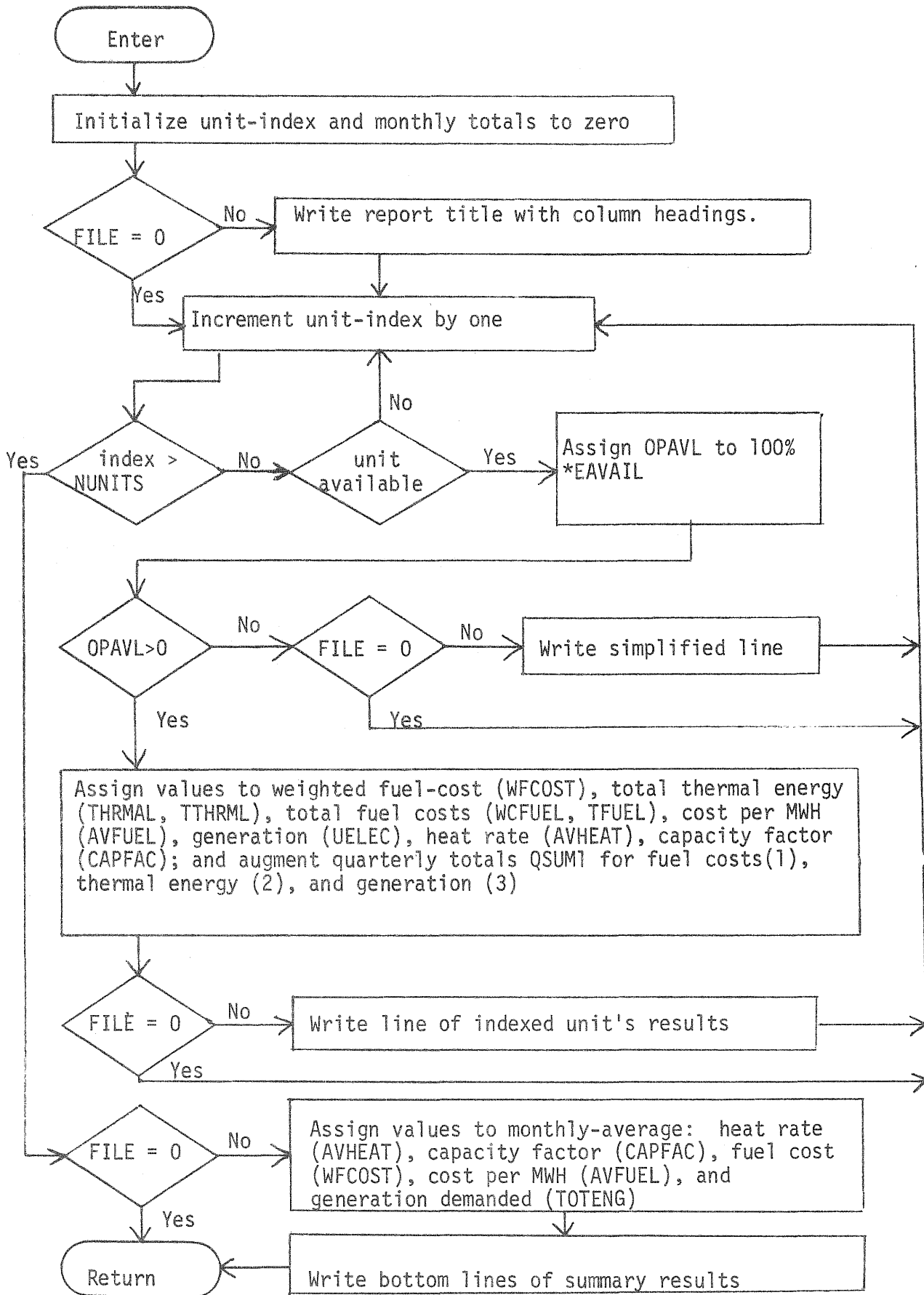
```

REPRT1 Routine

This routine computes unit operating characteristics during the specified month. If the output unit (FILE) is not zero, the results are printed. In either case, quarterly sums (QSUM1 columns) are augmented for possible use in other reports.

The scale factors used in the assignments deserve explanation. In the table following, M is consistently used to represent million.

<u>units of contributing factors</u>		<u>numeric factor</u>		<u>units carried</u>	<u>variable assigned</u>
(MBTU) * (ϕ /MBTU)	=	.00001	*	(K\$)	TFUEL
(K\$)/(MWH)	=	1000	*	(\$/MWH)	AVFUEL
(MBTU)/(MWH)	=	1000	*	(BTU/KWH)	AVHEAT
none	=	100	*	(%)	OPAVL
(MWH)/((MW)*(H))	=	100	*	(%)	CAPFAC



```

=====
C
C ROUTINE:          **** R E P R T 1 ****
C
C PURPOSE:
C   TO WRITE A MONTHLY REPORT OF THE EXPECTED UNIT OPERATING
C   CHARACTERISTICS; ALSO, TO ROLL MONTHLY VALUES FOR EACH
C   UNIT INTO ARRAY QSUM1, WHICH WILL BE USED TO
C   PRINT AND CALCULATE VALUES IN REPR3.
C
C INPUT VARIABLES:
C   PBTUCT          COST OF PRIMARY FUEL IN CENTS/MEGA-BTU
C   ABTUCT          COST OF ALTERNATE FUEL IN CENTS/MEGA-BTU
C   PGENFC          FRACTION OF GENERATION USING PRIMARY FUEL
C   ENRGE2          ENERGY GENERATED BY EACH UNIT OVER THE MONTH
C   AVAIL           .TRUE. IF UNIT WAS AVAILABLE DURING STUDY
C                   .FALSE. IF UNIT WAS NOT AVAILABLE DURING STUDY
C   BLKCAP          CUMULATIVE BLOCK CAPACITIES FOR EACH UNIT, IN MW
C   HRSIP           NUMBER OF HOURS IN STUDY PERIOD
C   YEAR            YEAR OF STUDY (FOUR-DIGIT)
C   MONTH           MONTH OF STUDY
C   NUNITS          NUMBER OF UNITS LOADED
C   UNAME           NAMES OF GENERATING UNITS
C   COMPNA          COMPANY NAME
C   FILE            LOGICAL UNIT TO WHICH REPORT IS TO BE WRITTEN
C   EAVAIL          EFFECTIVE AVAILABILITY
C   UNIT            LOADING ORDER OF UNITS
C   TITLE           STUDY DESCRIPTION
C
C OUTPUT VARIABLES:
C   QSUM1           QUARTERLY TOTALS BY UNITS, BY COLUMNS:  1-FUEL COSTS,
C                   2-THERMAL ENERGY, 3-ELECTRIC GENERATION
C   TTHRML          TOTAL THERMAL ENERGY FOR THIS MONTH
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
=====

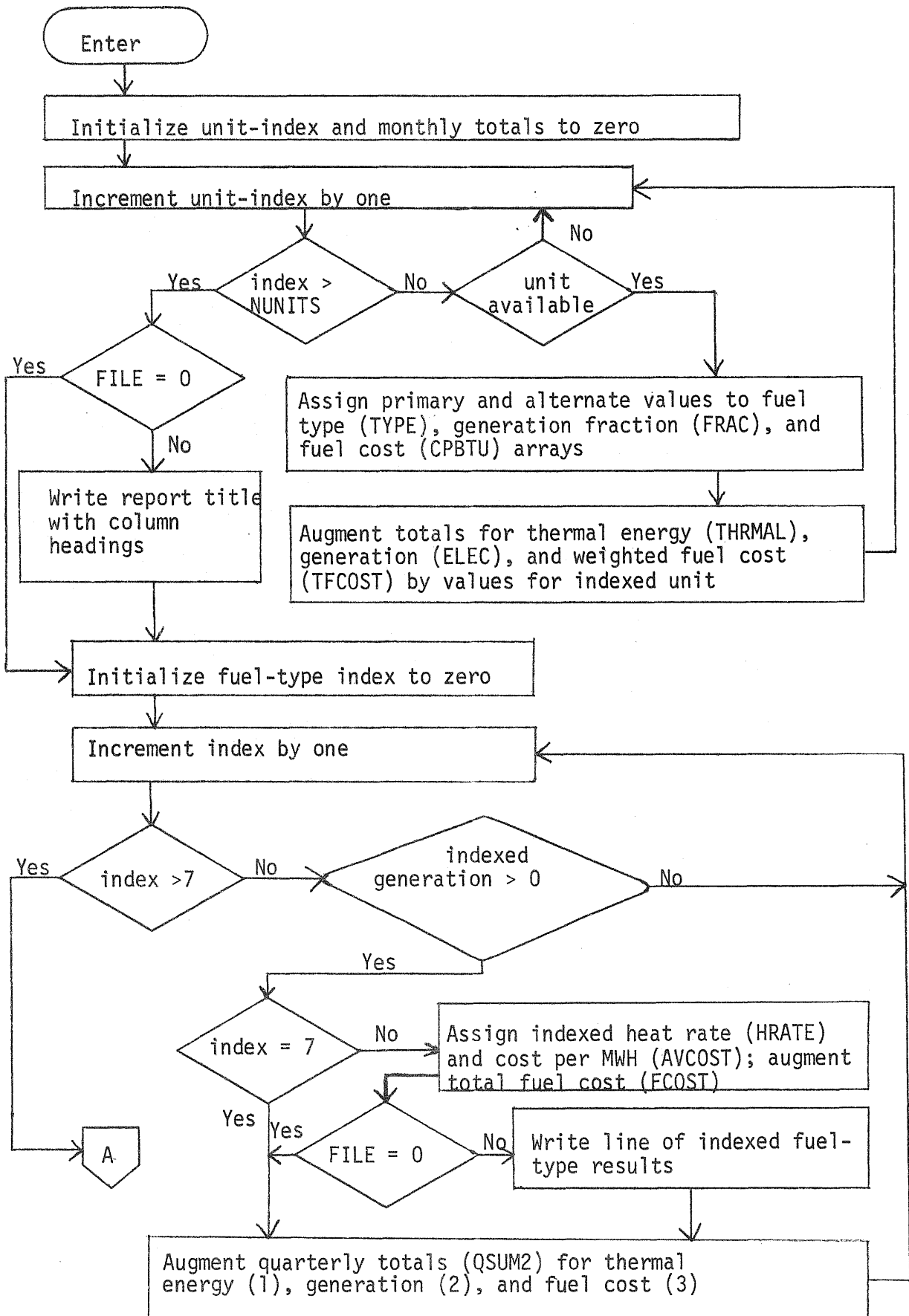
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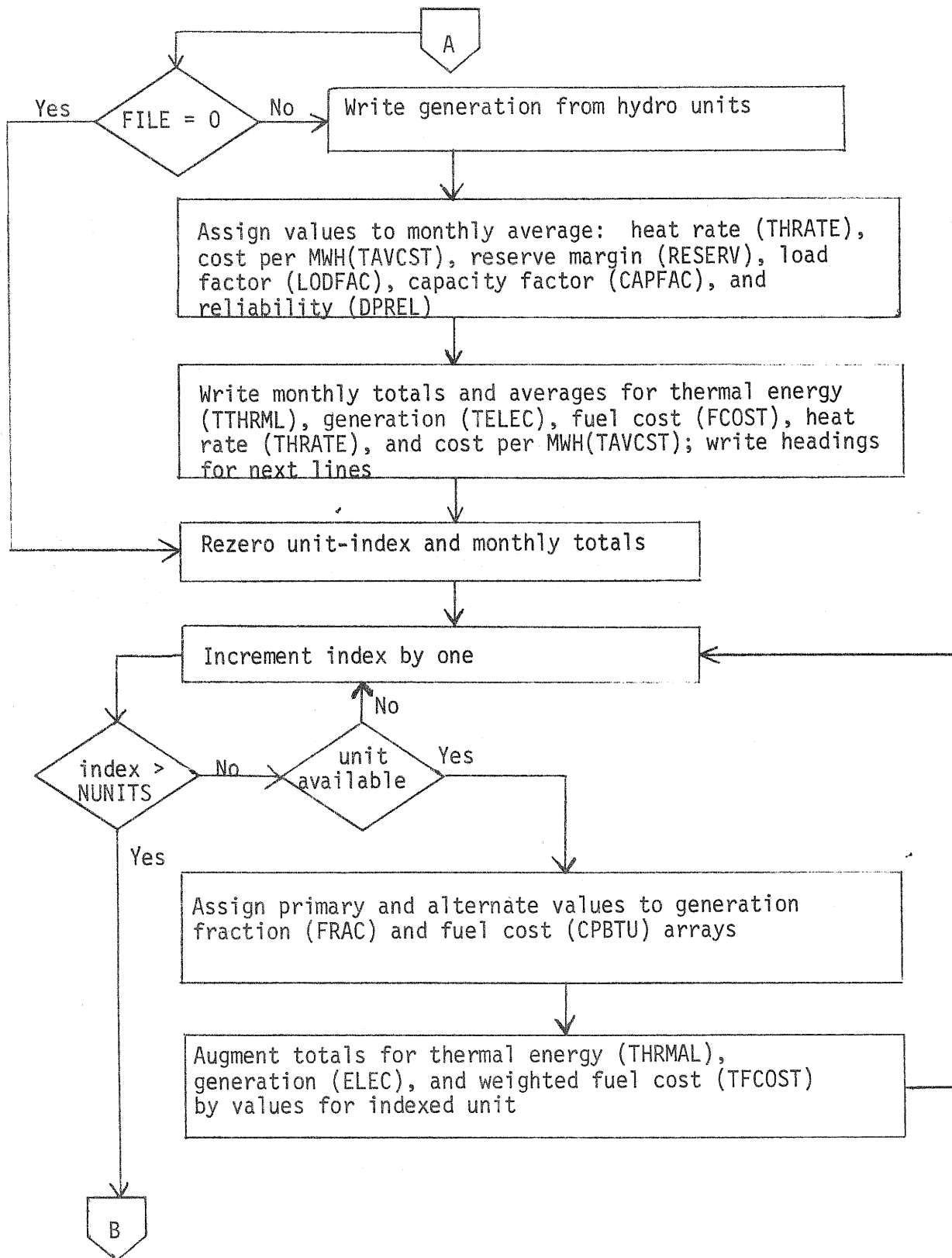
REPRT2 Routine

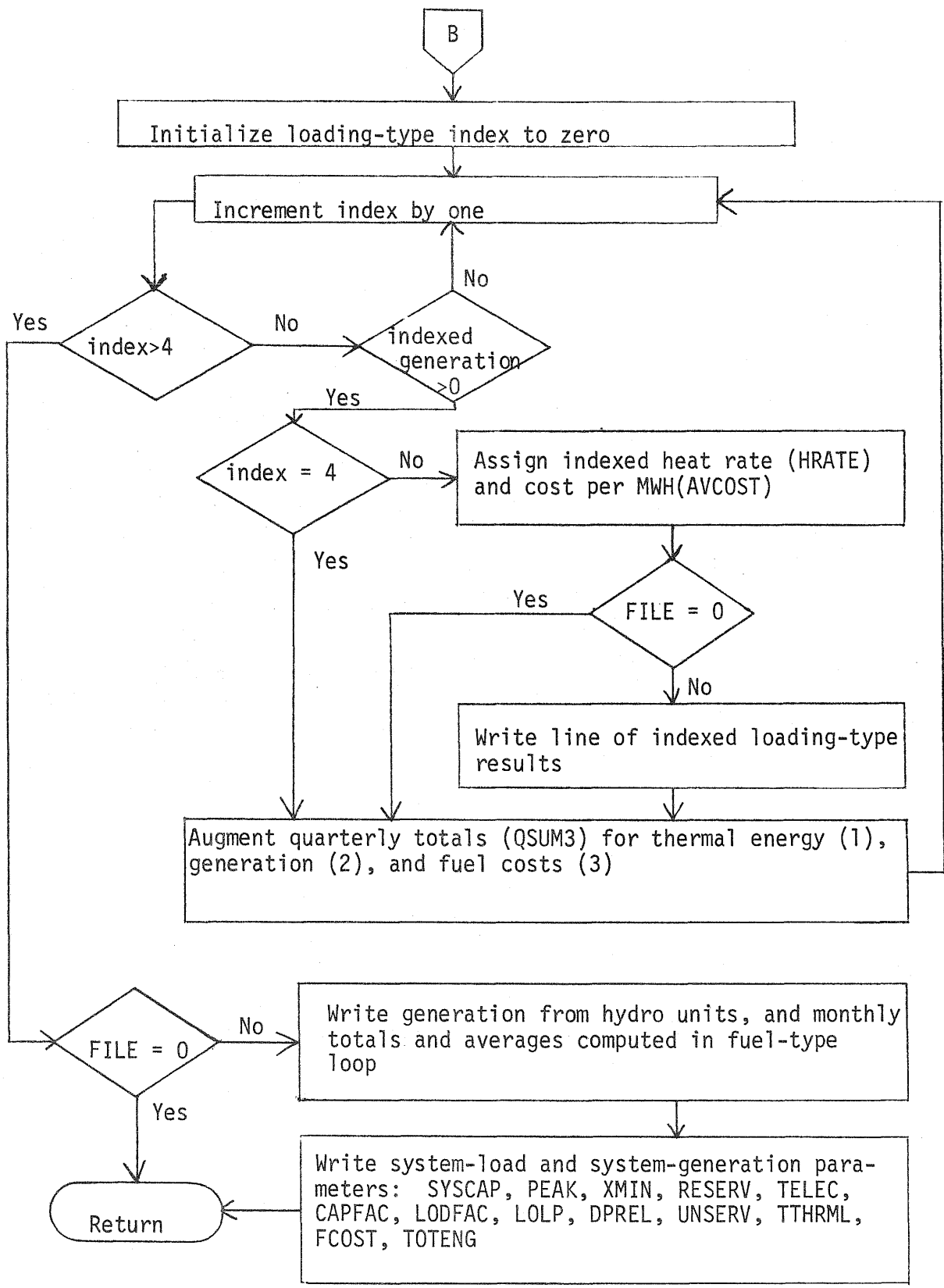
This routine computes the specified month's fuel-usage characteristics from two aspects of the generation system, segmenting it first by the seven fuel types and secondly by the four types of loading. If the output unit (FILE) is not zero, the results are printed. In either case, quarterly sums (arrays QSUM2 and QSUM3) are augmented for possible use in other reports. In conclusion, a line of parameters characterizing the system load is printed: capacity, base and peak loads, load and capacity factors, reserve margin, generated and unserved energy values, and generation reliability. To avoid apparent discrepancies due to single-precision arithmetic, the fuel-usage parameters averaged across fuel types are used as surrogates for those averaged across loading types.

The scale factors used in the assignments deserve explanation. In the table following, M is consistently used to represent million.

<u>units of contributing factors</u>	<u>numeric factor</u>	<u>units carried</u>	<u>variable assigned</u>
(¢/MBTU) * (MBTU)	= .00001	* (K\$)	TFCOST
(K\$)/(MWH)	= 1000	* (\$/MWH)	AVCOST
(MBTU)/(MWH)	= 1000	* (BTU/KWH)	HRATE
(MWH)/((MW)*(H))	= 100	* (%)	LODFAC
(MWH)/((MW)*(H))	= 100	* (%)	CAPFAC







```

=====
C
C ROUTINE:          **** R E P R T 2 ****
C
C PURPOSE:
C   TO WRITE A REPORT THAT SUMMARIZES THE SYSTEM PARAMETERS
C   BY FUEL TYPE AND UNIT LOADING TYPE; ALSO, TO ROLL QUARTERLY
C   TOTALS BY FUEL TYPE AND LOADING TYPE INTO QSUM2 AND QSUM3
C   RESPECTIVELY.
C
C INPUT VARIABLES:
C   SYSCAP          SYSTEM CAPACITY IN MW, BY MONTH
C   PEAK            SYSTEM PEAK LOADS IN MW, BY MONTH
C   LOLP            LOSS-OF-LOAD PROBABILITY, BY MONTH
C   HRSIF           HOURS IN A STUDY MONTH
C   UNSERV          UNSERVED ENERGY IN MWH, BY MONTH
C   PGENFC          FRACTION OF ENERGY GENERATED BY PRIMARY FUEL, BY MONTH
C   PBTUCT          COST OF PRIMARY FUEL, IN CENTS/MEGA-BTU
C   ABTUCT          COST OF ALTERNATE FUEL, IN CENTS/MEGA-BTU
C   PRIEUL          PRIMARY FUEL TYPE FOR UNIT
C   ALTFUL          ALTERNATE FUEL TYPE FOR UNIT
C   MONTH          MONTH OF STUDY
C   FILE           LOGICAL UNIT TO WHICH REPORT IS TO BE WRITTEN
C   ENRGE2         ENERGY GENERATED BY UNITS, BY COLUMNS: 1-FIRST BLOCK,
C                 2-SECOND BLOCK, 3-THIRD BLOCK, 4-TOTAL FOR UNIT
C   HEAT           THERMAL ENERGY REQUIREMENTS BY UNITS, BY COLUMNS:
C                 1-FIRST BLOCK, 2-SECOND BLOCK, 3-THIRD BLOCK,
C                 4-TOTAL FOR UNIT
C   NUNITS         NUMBER OF UNITS IN STUDY
C   AVAIL          .TRUE. IF UNIT WAS AVAILABLE
C                 .FALSE. IF UNIT WAS NOT AVAILABLE
C   COMPNA         NAME OF COMPANY
C   YEAR           YEAR OF STUDY
C   TTHRML         TOTAL THERMAL ENERGY FOR THIS MONTH
C   UNTYPE         LOADING TYPE OF UNIT
C   XMIN           BASE LOAD IN MW
C
C OUTPUT VARIABLES:
C   MSUM2          MONTHLY ELECTRIC AND COST TOTALS BY FUEL TYPE
C   QSUM2          QUARTERLY THERMAL, ELECTRIC, AND COST TOTALS BY
C                 FUEL TYPE
C   QSUM3          QUARTERLY THERMAL, ELECTRIC, AND COST TOTALS BY
C                 LOADING TYPE
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
=====

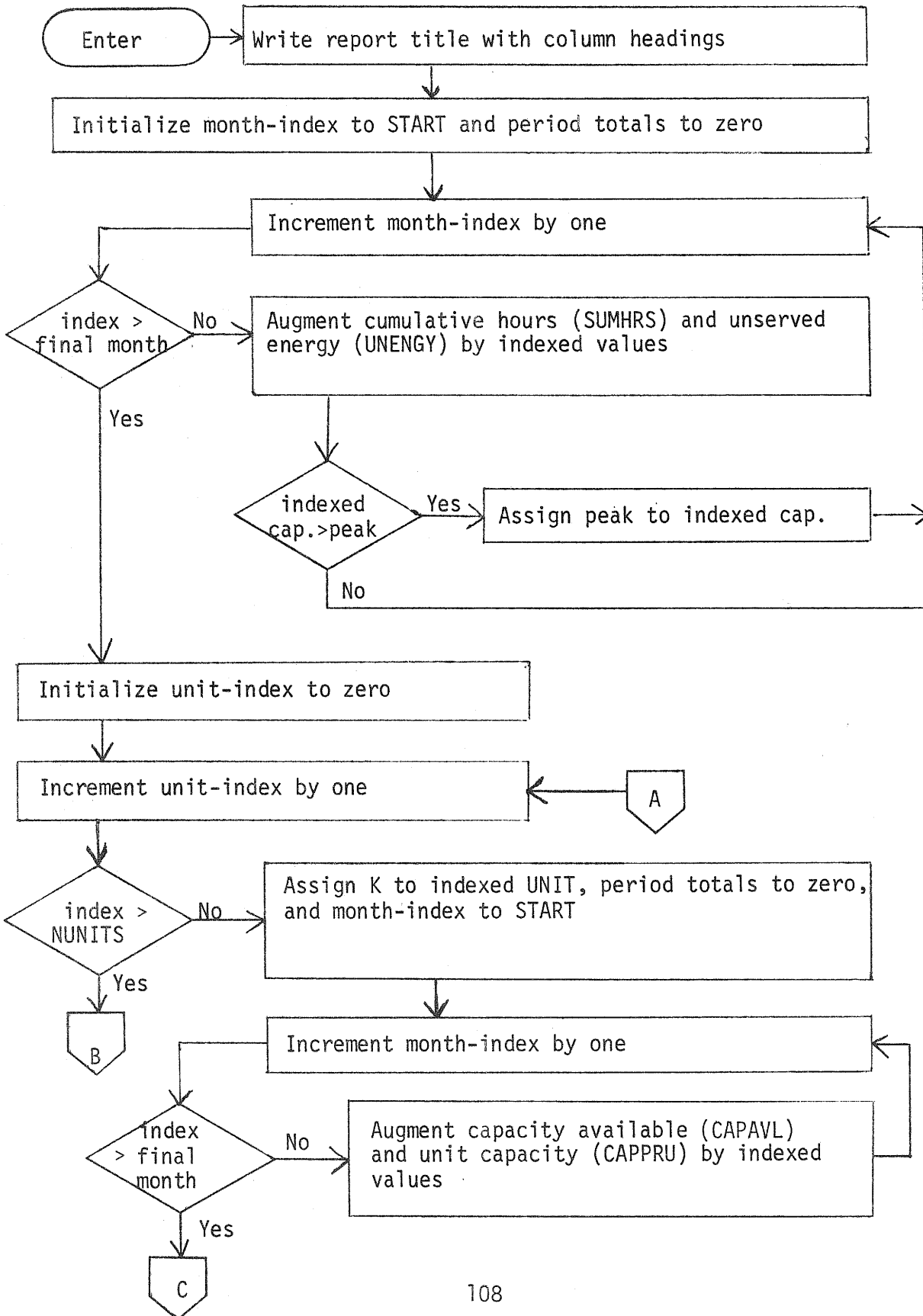
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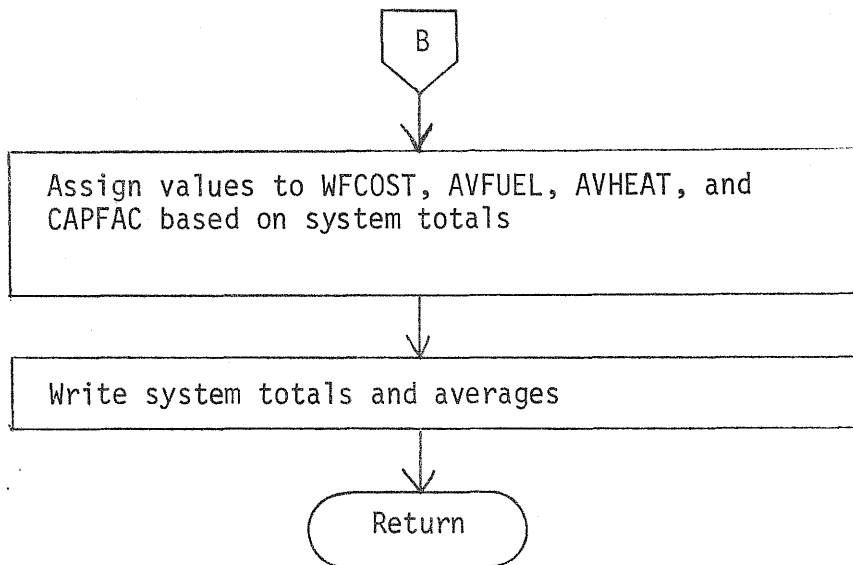
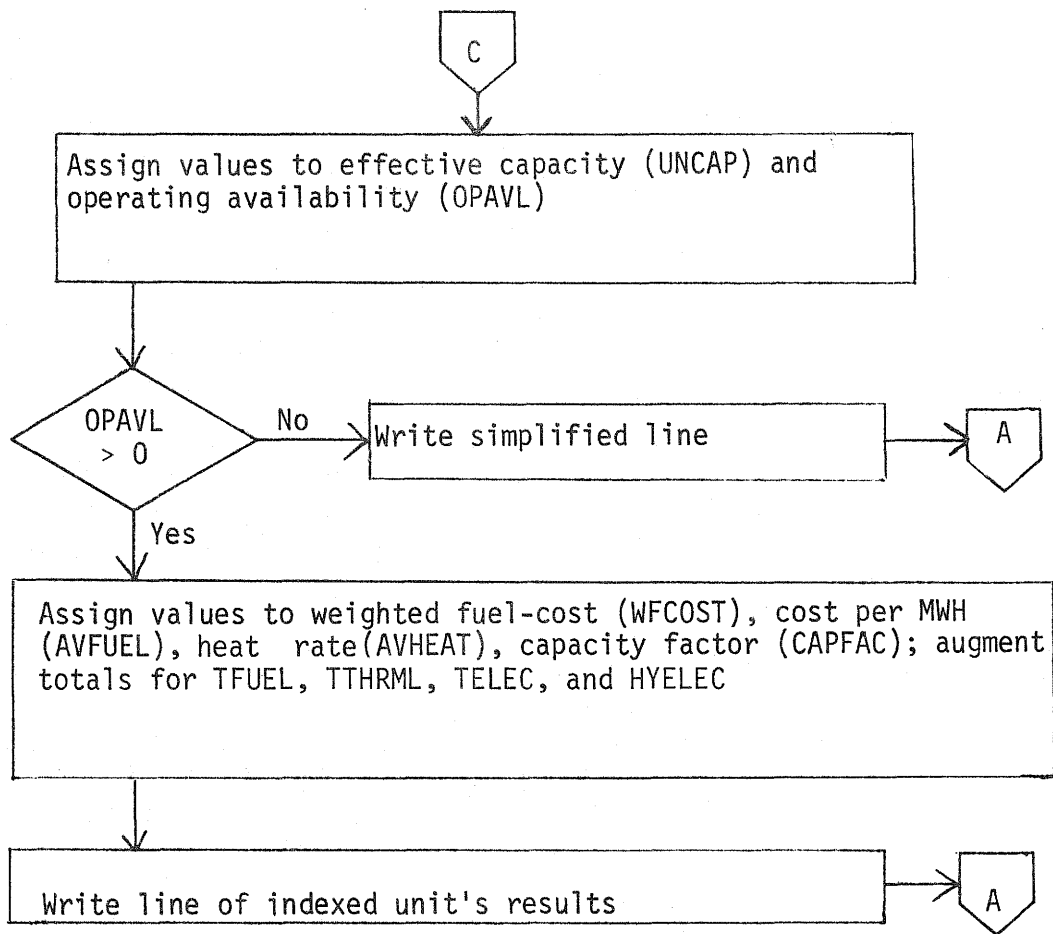
REPRT3 Routine

This routine computes unit operating characteristics over the specified period (from START to MONTH), usually a year or quarter thereof. Previously-computed data passed via array SUM1 (from routine REPRT1 if QSUM1, from MAIN program if ASUM1) are used with other unit-indexed arrays (EAVAIL and COWNMW).

The scale factors used in the assignments deserve explanation. In the table following, M is consistently used to represent million.

<u>units of contributing factors</u>		<u>numeric factor</u>		<u>units carried</u>	<u>variable assigned</u>
(K\$)/(MBTU)	=	100,000	*	(¢/MBTU)	WFCOST
(K\$)/(MWH)	=	1000	*	(\$/MWH)	AVFUEL
(MBTU)/(MWH)	=	1000	*	(BTU/KWH)	AVHEAT
(MWH)/(MWH)	=	100	*	(%)	CAPFAC





```

C=====
C
C ROUTINE:          **** R E P R T 3 ****
C
C PURPOSE:
C   TO WRITE A REPORT OF THE EXPECTED UNIT OPERATING CHARACTERISTICS
C   ON A QUARTERLY AND AN ANNUAL BASIS
C
C INPUT VARIABLES:
C   SUM1           BY COLUMNS:  TOTAL FUEL COST, ELECTRIC AND THERMAL
C                   ENERGY GENERATION
C   WFCOST         WEIGHTED-AVERAGE FUEL COST, IN CENTS/MEGA-BTU
C   AVFUEL         AVERAGE FUEL COST, IN DOLLARS/MWH
C   AVHEAT         AVERAGE HEAT RATE
C   CAPFAC         CAPACITY FACTOR
C   START          STARTING MONTH OF REPORT PERIOD
C   BLKCAP         CUMULATIVE BLOCK CAPACITIES FOR EACH UNIT, IN MW
C   HRSIP          HOURS IN STUDY PERIOD
C   YEAR           YEAR OF STUDY
C   MONTH          MONTH OF STUDY
C   NUNITS         NUMBER OF UNITS IN STUDY
C   UNAME          NAMES OF GENERATING UNITS
C   COMPNA        COMPANY NAME
C   FILE           LOGICAL UNIT TO WHICH REPORT IS TO BE WRITTEN
C   EAVAIL         EFFECTIVE AVAILABILITY
C   UNIT           LOADING ORDER OF UNITS
C   PRIFUL        PRIMARY FUEL TYPE
C   UNLOAD         LOADING TYPE OF UNIT
C   TITLE          STUDY DESCRIPTION
C   SYSTEMW       SYSTEM CAPACITY IN MW
C   UNSERV        UNSERVED ENERGY IN MWH
C
C OUTPUT VARIABLES:
C   TELEC          CUMULATIVE GENERATION IN MWH
C   TTHRML        CUMULATIVE THERMAL ENERGY IN MEGA-BTU
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====

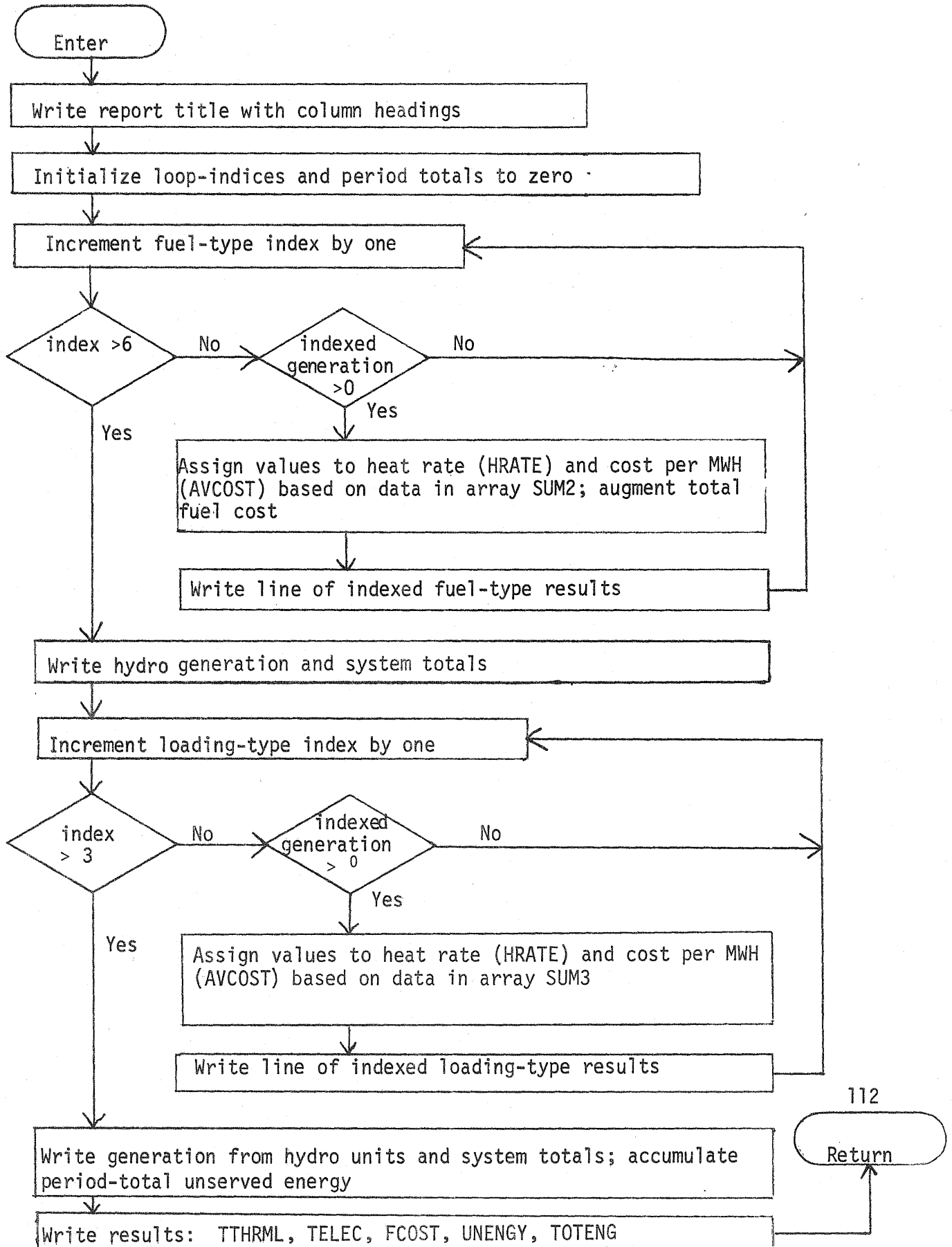
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REPRT4 Routine

This routine computes the fuel-usage characteristics over the specified period (from START to MONTH) from two aspects of the generation system, segmenting it first by the seven fuel types and secondly by the four types of loading. Previously-computed data passed via arrays SUM2 and SUM3 (from routine REPRT2 if a quarterly period, from MAIN program if annual) are used.

The scale factors used in the assignments deserve explanation. In the table following, M is consistently used to represent million.

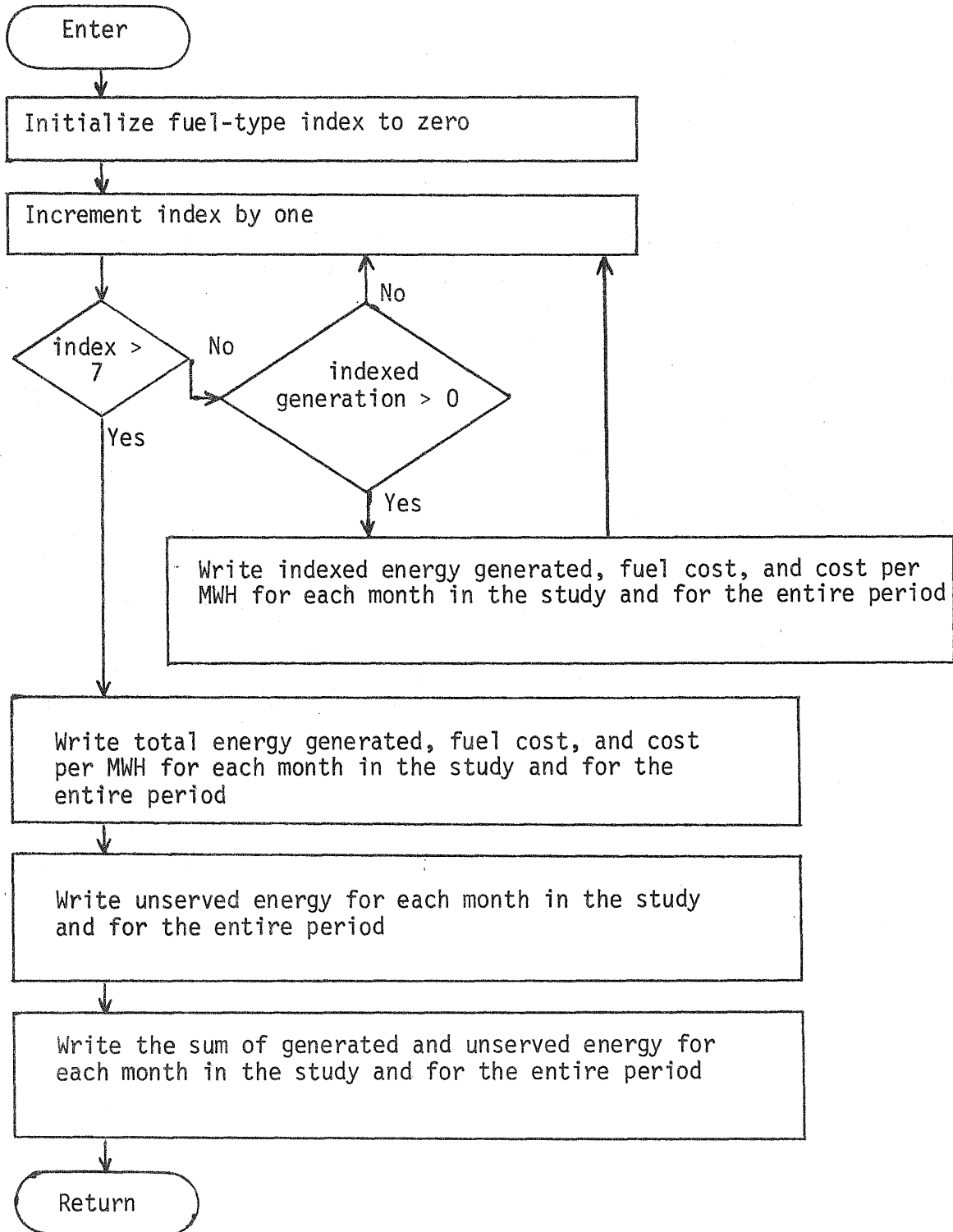
<u>units of contributing factors</u>		<u>numeric factor</u>		<u>units carried</u>	<u>variable assigned</u>
(MBTU)/(MWH)	=	1000	*	(BTU/KWH)	HRATE
(K\$)/(MWH)	=	1000	*	(\$/MWH)	AVCOST



```
C=====
C
C ROUTINE:          **** R E P R T 4 ****
C
C PURPOSE:
C   TO WRITE A REPORT SUMMARIZING GENERATION AND FUEL USAGE BY FUEL
C   TYPE AND LOADING TYPE ON A QUARTERLY AND ANNUAL BASIS.
C
C INPUT VARIABLES:
C   UNSERV          UNSERVED ENERGY BY MONTH
C   START           FIRST MONTH OF STUDY PERIOD
C   MONTH          FINAL MONTH OF STUDY PERIOD
C   FILE           LOGICAL UNIT TO WHICH REPORT IS TO BE WRITTEN
C   SUM2           THERMAL, ELECTRIC, AND COST TOTALS BY FUEL TYPE
C   SUM3           THERMAL, ELECTRIC, AND COST TOTALS BY LOADING TYPE
C   COMPNA        COMPANY NAME
C   YEAR           YEAR OF STUDY
C   TELEC          TOTAL GENERATION IN MWH
C   TTHRML        TOTAL THERMAL ENERGY IN MEGA-BTU
C
C OUTPUT VARIABLES:
C   FCOST          TOTAL FUEL COST IN THOUSANDS OF DOLLARS
C   TAVCST        TOTAL AVERAGE FUEL COST IN DOLLARS/MWH
C   UNENGY        TOTAL UNSERVED ENERGY, IN MWH
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====
```

REPRT5 Routine

This routine simply and concisely restates the fuel-usage as computed in other report routines for each month covered by the study period, and for the entire period. Supporting data on generated and unserved energy are printed. The numeric factor of 1000 is included in the average-cost calculation to convert from (K\$)/(MWH) to (\$/MWH) units.

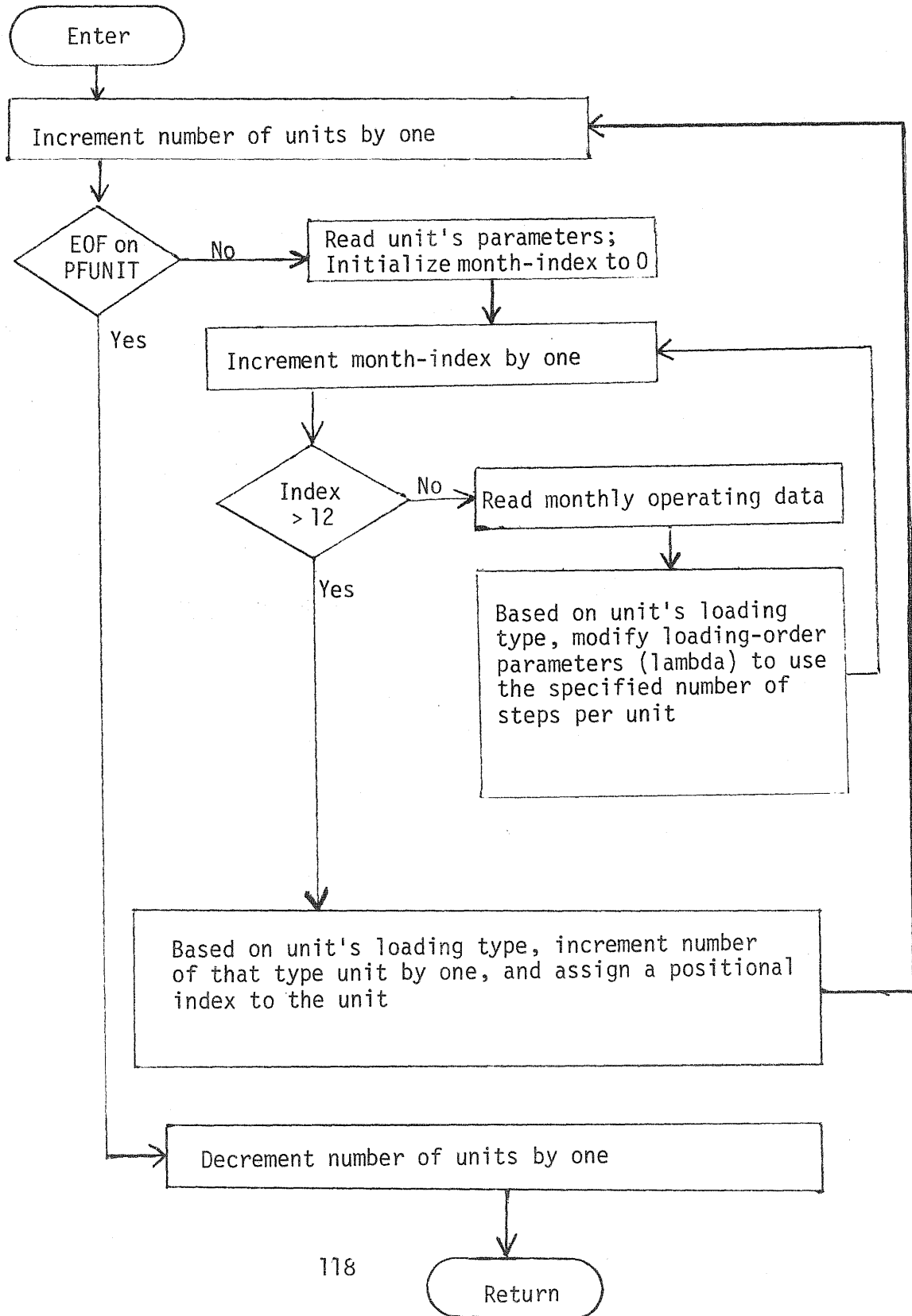


```
C=====
C
C ROUTINE:          *** R E P R T 5 ***
C
C PURPOSE:
C   TO WRITE A REPORT SUMMARIZING MONTHLY FUEL USAGE.
C
C INPUT VARIABLES:
C   UNSERV          UNSERVED ENERGY BY MONTH, IN MWH
C   UNENGY          TOTAL UNSERVED ENERGY, IN MWH
C   MONTH1         FIRST MONTH OF STUDY PERIOD
C   MONTH          FINAL MONTH OF STUDY PERIOD
C   FILE           LOGICAL UNIT TO WHICH REPORT IS TO BE WRITTEN
C   MSUM2          MONTHLY ELECTRIC AND COST TOTALS BY FUEL TYPE
C   ASUM2          ANNUAL THERMAL, ELECTRIC, AND COST TOTALS BY FUEL TYPE
C   COMPNA         COMPANY NAME
C   YEAR           YEAR OF STUDY
C   TELEC          TOTAL GENERATION IN MWH
C   FCOST          TOTAL FUEL COST IN THOUSANDS OF DOLLARS
C   TAVCST         RATIO OF TOTAL FUEL COST TO TOTAL GENERATION, IN $/MWH
C
C AUTHOR:
C   NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED:  10/79
C=====
```

UNIFOS Routine

This routine reads data values for nuclear and fossil-fueled generating units primarily (outer-loop) by unit and secondarily (inner-loop) by month within the study year. Each such unit's loading type is here restricted to 1, 2, or 3 to indicate base, cycling, or peaking, respectively; type 4 (hydro) is disallowed. Thus the loading type determines the branching which assigns the number of loading steps per unit (NSTEP) and the branching for counting and indexing each unit.

The three lambda arrays (LAMDA1, LAMDA2, LAMDA3) as read indicate the dispatch priorities, a block having a lower-value lambda being loaded prior to one with a higher value. In general, all three arrays will be specified by the input data, yet the analyst may want to make a run using only one or two loading steps per unit. This option having been specified independently across loading types by parameters NBSTEP, NCSTEP, and NPSTEP (one of which is assigned to local variable NSTEP), the lambda arrays are used unaltered if NSTEP is three. For NSTEP equal to two, the priority for the full-load block (in LAMDA3) is assigned to that specified for the next lower-order block (in LAMDA2), and LAMDA2 is assigned to zero, so that each unit is priority-loaded in two steps. For NSTEP equal to one, the priority for the full-load block is assigned to that specified for the lowest block (in LAMDA1), and both LAMDA2 and LAMDA1 are assigned to zero, so that each unit is fully-loaded according to the lowest-order priorities.




```

C=====
C
C ROUTINE:          **** U N I F O S ****
C
C PURPOSE:
C   TO READ THE NUCLEAR- AND FOSSIL-FUELED UNITS' DATA FROM LOGICAL
C   UNIT PFUNIT.  THE OPERATION CHARACTERISTICS ARE READ AND STORED FOR
C   EACH MONTH OF THE STUDY.  ALSO THE UNIT CAPACITY AVAILABLE TO THE
C   COMPANY IS CALCULATED.
C
C INPUT VARIABLES:
C   PFUNIT   LOGICAL UNIT FROM WHICH UNIT INFORMATION IS READ
C   IYEAR    FOUR-DIGIT STUDY-YEAR
C   NBSTEP   NUMBER OF LOADING STEPS FOR BASE UNITS
C   BCSTEP   NUMBER OF LOADING STEPS FOR CYCLING UNITS
C   NPSTEP   NUMBER OF LOADING STEPS FOR PEAKING UNITS
C
C OUTPUT VARIABLES:
C   AUPAVL   ANNUAL UNIT PRODUCTION AVAILABILITY
C   CAPCST   CAPITAL COST OF UNIT IN DOLLARS PER INSTALLED KW
C   VSCCNO   UNIT NUMBER ASSIGNED BY VSCC
C   UNAME    UNIT NAME
C   FRAOWN   FRACTION OF UNIT OWNED BY COMPANY
C   UNTYPE   THE CLASSIFICATION OF THE UNIT:
C              1-STEAM FOSSIL, 2-STEAM NUCLEAR,
C              3-I.C. ENGINE, 4-GAS TURBINE,
C              5-JET ENGINE, 6-HYDRO,
C              7-PUMPED STORAGE
C   UNLOAD   UNIT LOADING TYPE: 1-BASE, 2-CYCLING, 3-PEAKING, 4-HYDRO
C   PRIFUL   PRIMARY FUEL USED BY EACH UNIT:
C              1-COAL           5-NATURAL GAS
C              2-NUCLEAR        6-GASOLINE
C              3-LIGHT OIL      7-WATER
C              4-HEAVY OIL      0-NONE
C   ALTFUL   ALTERNATE FUEL USED BY EACH UNIT, AS IN PRIFUL
C   IGFUEL   IGNITION FUEL USED BY EACH UNIT, AS IN PRIFUL
C   ONLIMO   THE MONTH THAT THE UNIT WENT INTO COMMERCIAL SERVICE
C   ONLIYR   THE YEAR THE UNIT WENT INTO SERVICE
C   OFLIMO   THE LAST MONTH THE UNIT IS EXPECTED TO REMAIN IN SERVICE
C   OFLIYR   THE LAST YEAR THE UNIT IS EXPECTED TO REMAIN IN SERVICE
C   UNETCP   UNLIMITED NET CAPACITY OF UNIT
C   LNETCP   LIMITED NET CAPACITY OF UNIT
C   HEATR1   HEAT RATE FOR FIRST BLOCK, IN BTU/KWH
C   HEATR2   HEAT RATE FOR SECOND BLOCK, IN BTU/KWH
C   HEATR3   HEAT RATE FOR THIRD BLOCK, IN BTU/KWH
C   EAVAIL   EFFECTIVE AVAILABILITY
C   BLKCAP   CUMULATIVE BLOCK CAPACITIES FOR EACH UNIT, IN MW
C   PBTUCT   PRIMARY FUEL COST IN CENTS/MEGA-BTU
C   ABTUCT   COST OF ALTERNATE FUEL IN CENTS PER MEGA-BTU
C   LAMDA1   LOADING PRIORITY FOR THE UNIT'S FIRST BLOCK
C   LAMDA2   LOADING PRIORITY FOR THE UNIT'S SECOND BLOCK
C   LAMDA3   LOADING PRIORITY FOR THE UNIT'S THIRD BLOCK
C   PGENFC   FRACTION OF GENERATION USING PRIMARY FUEL
C   IDBASE   LOCATION OF EACH BASE UNIT IN THE ORDER OF READING
C   IDCYCL   LOCATION OF EACH CYCLING UNIT IN THE ORDER OF READING
C   IDPEAK   LOCATION OF PEAKING UNITS IN THE ORDER OF READING
C   NBASE    THE NUMBER OF BASE UNITS
C   NCYCL    THE NUMBER OF CYCLING UNITS
C   NPEAK    THE NUMBER OF PEAKING UNITS
C   NUNITS   THE TOTAL NUMBER OF UNITS

```

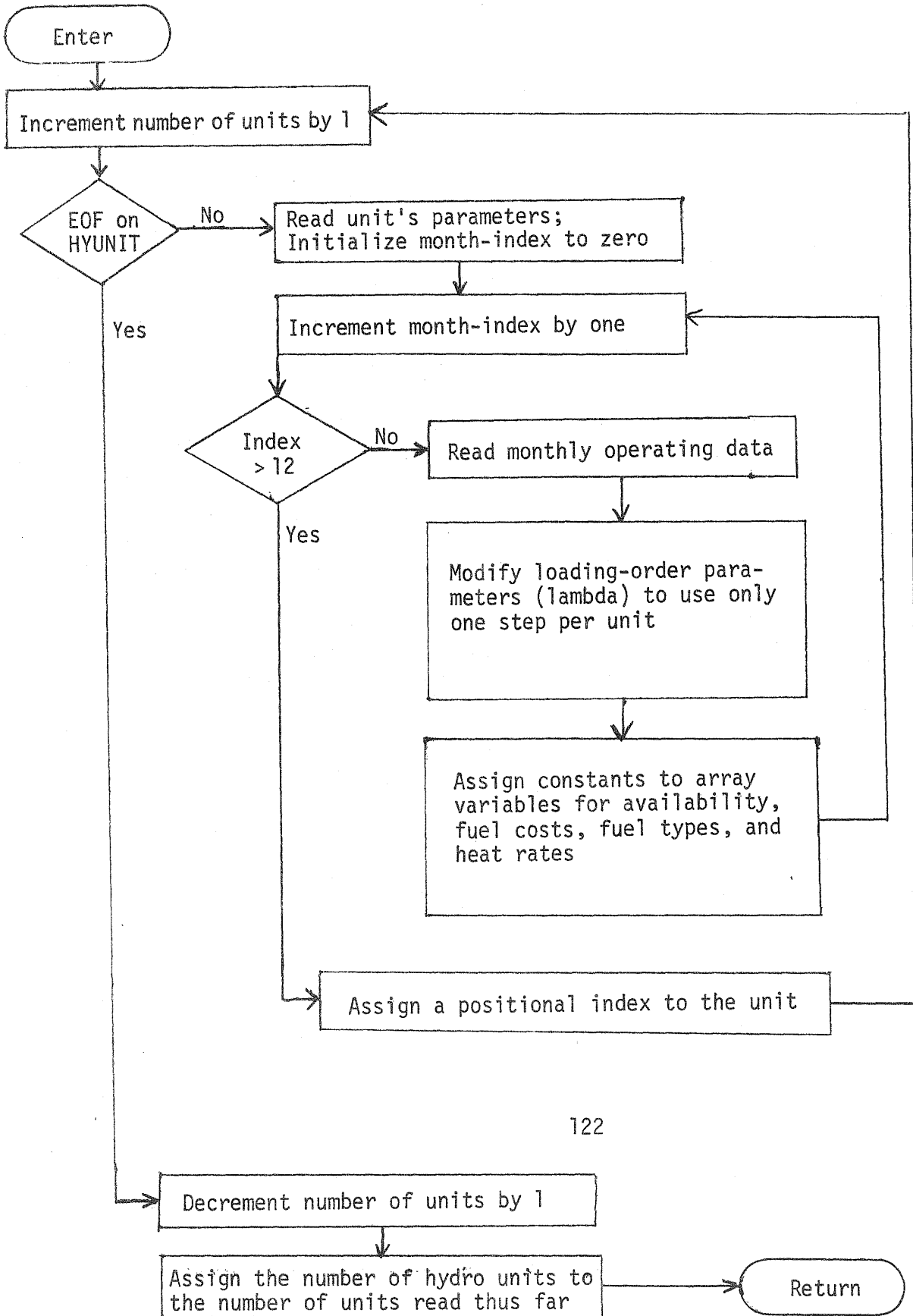
C
C NOTES:
C PROGRAM WILL END ABNORMALLY SHOULD AN UNEXPECTED EOF
C OCCUR OR IF THE YEAR ON FILE DOES NOT MATCH THAT ANTICIPATED.
C
C AUTHOR:
C NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED: 10/79
C
C=====

UNIHVD Routine

This routine reads and assigns data values for hydro generating units primarily (outer-loop) by unit and secondarily (inner-loop) by month within the study year. Hydro units are assigned availabilities of one (100%). Since no fuel is consumed, the heat rates and fuel costs are assigned to zero.

The three lambda arrays (LAMDA1, LAMDA2, LAMDA3) as read indicate the dispatch priorities, a block having a lower-value lambda being loaded prior to one with a higher value. In general, all three arrays will be specified by the input data, yet the program requires using only one loading step per hydro unit. This having been specified by parameter NHSTEP, the lambda arrays are altered: the priority for the full-load block is assigned to that specified for the lowest block (in LAMDA1), and both LAMDA2 and LAMDA1 are assigned to zero, so that each unit is fully-loaded according to the lowest-order priorities.

UNIHVD



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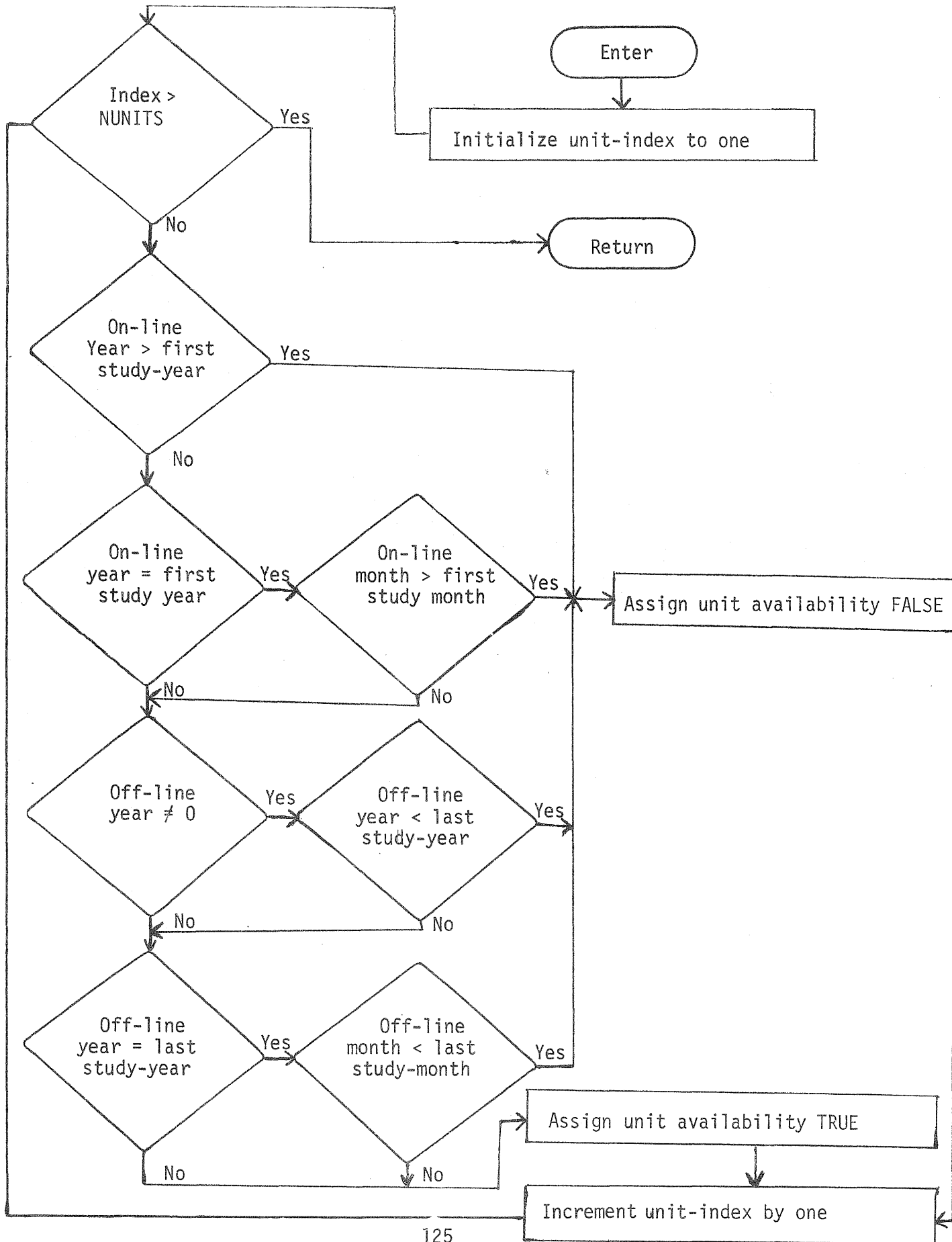
C=====
C
C ROUTINE:          **** U N I H Y D ****
C
C PURPOSE: TO READ THE HYDRO UNIT DATA FROM UNIT HYUNIT AND STORE
C THEM BY UNIT AND MONTH
C
C INPUT VARIABLES:
C HYUNIT LOGICAL UNIT FROM WHICH HYDRO INFORMATION IS READ
C IYEAR  FOUR-DIGIT STUDY-YEAR
C NHSTEP NUMBER OF LOADING STEPS FOR HYDRO UNITS
C
C OUTPUT VARIABLES:
C VSCCNO UNIT ID NUMBER
C UNAME  NAME OF UNIT
C FRAOWN FRACTION OWNED BY COMPANY
C UNTYPE TYPE OF GENERATION UNIT: 1-STEAM FOSSIL, 2-STEAM NUCLEAR,
C 3-I.C. ENGINE, 4-GAS TURBINE, 5-JET ENGINE, 6-HYDRO,
C 7-PUMPED STORAGE
C UNLOAD LOADING TYPE OF UNIT: 1-BASE, 2-CYCLE, 3-PEAK, 4-HYDRO
C HYTYPE TYPE OF HYDRO UNIT: 1-RUN OF RIVER, 2-STORAGE, 3-PUMPED
C STORAGE
C PRIFUL PRIMARY FUEL FOR UNIT: 1-COAL, 2-NUCLEAR, 3-LIGHT OIL,
C 4-HEAVY OIL, 5-NATURAL GAS, 6-GASOLINE, 7-WATER, 0-NONE
C ONLIMO ON-LINE MONTH FOR UNIT
C ONLIYR ON-LINE YEAR FOR UNIT
C OFLIMO OFF-LINE MONTH FOR UNIT
C OFLIYR OFF-LINE YEAR FOR UNIT
C AUPAVL ANNUAL UNIT PRODUCTION AVAILABILITY
C CAPCST CAPACITY COST
C UNETCP UNLIMITED NET CAPACITY OF UNIT
C LNETCP LIMITED NET CAPACITY OF UNIT
C LAMDA1 LOADING PRIORITY FOR THE UNIT'S FIRST BLOCK
C LAMDA2 LOADING PRIORITY FOR THE UNIT'S SECOND BLOCK
C LAMDA3 LOADING PRIORITY FOR THE UNIT'S THIRD BLOCK
C NUNITS CURRENT NUMBER OF UNITS IN SYSTEM
C NHYDRO NUMBER OF HYDRO UNITS IN SYSTEM
C IDHYDR LOCATION OF EACH UNIT IN THE ORDER OF READING
C ALTFUL ALTERNATE FUEL CODE, AS IN PRIFUL
C IGFUEL IGNITION FUEL CODE, AS IN PRIFUL
C UNGEN PROJECTED GENERATION OF EACH UNIT, IN MWHR
C BLKCAP CUMULATIVE BLOCK CAPACITIES FOR EACH UNIT, IN MW
C EAVAIL EFFECTIVE AVAILABILITY
C HEATR1 HEAT RATE FOR FIRST BLOCK, IN BTU/KWH
C HEATR2 HEAT RATE FOR SECOND BLOCK, IN BTU/KWH
C HEATR3 HEAT RATE FOR THIRD BLOCK, IN BTU/KWH
C PBTUCT COST OF PRIMARY FUEL IN CENTS/MEGA-BTU
C ABTUCT COST OF ALTERNATE FUEL IN CENTS/MEGA-BTU
C PGENFC FRACTION OF GENERATION USING PRIMARY FUEL
C
C AUTHOR:
C NATIONAL REGULATORY RESEARCH INSTITUTE
C
C LAST REVISED: 10/79
C
C=====

```

UNITON Routine

To meet the availability criteria, this routine requires that a plant (unit) have its date of on-line transfer no later than the first month of the first study-year, and its date of off-line transfer no earlier than the last month of the last study-year. As called, however, the routine has the first and last study-years identical, as are the first and last study-months. In practice, then, the criteria degenerate to simply having the current (study) month and year date no earlier than the date of on-line transfer and no later than the date of off-line transfer. Logic requires that the month of off-line transfer be specified as the last full month during which the unit is expected to be in service.

UNITON



C *****
C ROUTINE: *** U N I T O N ***
C

C PURPOSE:
C TO FILL AN ARRAY (AVAIL) WITH LOGICAL (TRUE/FALSE)
C VALUES INDICATING WHETHER A PARTICULAR UNIT IS ONLINE
C FOR THE MONTH OF STUDY.
C

C INPUT VARIABLES:
C MOLOW BEGINNING MONTH OF STUDY
C YRLOW BEGINNING YEAR OF STUDY (LAST 2 DIGITS)
C MONHIGH ENDING MONTH OF STUDY
C YRHIGH ENDING YEAR OF STUDY (LAST 2 DIGITS...I.E. 1976 => 76)
C NUMITS NUMBER OF UNITS TO CHECK
C ONLIMO MONTH THE UNIT WENT INTO SERVICE
C ONLIYR YEAR THE UNIT WENT INTO SERVICE
C OFLIMO LAST MONTH THE UNIT IS EXPECTED IN SERVICE
C OFLIYR LAST YEAR THE UNIT IS EXPECTED IN SERVICE
C

C OUTPUT VARIABLES:
C AVAIL .TRUE. IF UNIT IS AVAILABLE
C .FALSE. IF UNIT IS NOT AVAILABLE
C

C AUTHDR:
C NATIONAL REGULATORY RESEARCH INSTITUTE
C

C LAST REVISED: 10/79
C

C *****

DISPATCH MODULE ROUTINES

The DISPATCH module contains a MAIN routine and 9 subroutines. Figure 23 shows the name of each subroutine and the calling sequence.

This section contains a description of each subroutine and a flow chart for each one.

MAIN Routine

The MAIN routine of the DISPATCH module carries out more than the normal control function. Except for a few subroutines the function of DISPATCH is performed in the MAIN routine.

The concept of the DISPATCH module is to calculate a loading order based on some first order constraints. These constraints are

1. The first loading blocks of the available units are loaded by increasing cost until a minimum load value is reached. This allows in a simplistic way to simulate the backing-off of units during night time.
2. Maintaining an on-line reserve margin.

The values that these constraints use are entered by the user. The imaginative use of these values will lead to some interesting dispatching orders.

The MAIN routine performs the following functions:

1. read user information;
2. read plant data;
3. if hydro units are in the system it determines the type of units;
4. if hydro units are in the system the appropriate fuel costs are calculated;
 - run of river zero costs
 - pumped storage loss factor times average pumping cost
 - river storage relative cost provided by user
 - contract cost on data file

5. determine the cost of each fossil and nuclear loading block;
6. order the first, second and third loading step by cost within each group;
7. load the first blocks of the units until the minimum load condition is met;
8. order all the unloaded steps by cost;
9. check and correct for improper sequencing of a unit's loading blocks;
10. load the unload blocks subject to the reserve constraint;
11. assign relative dispatching values to each loading step. These values are in increments of five, thus providing ease of shifting the loading order based on other constraints.
12. write the new plant files.

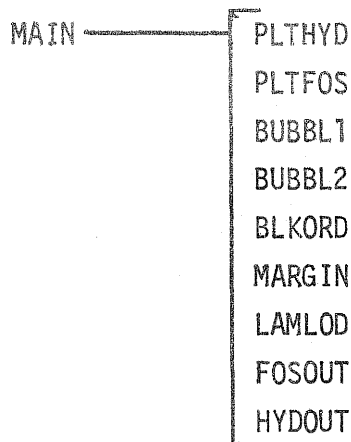
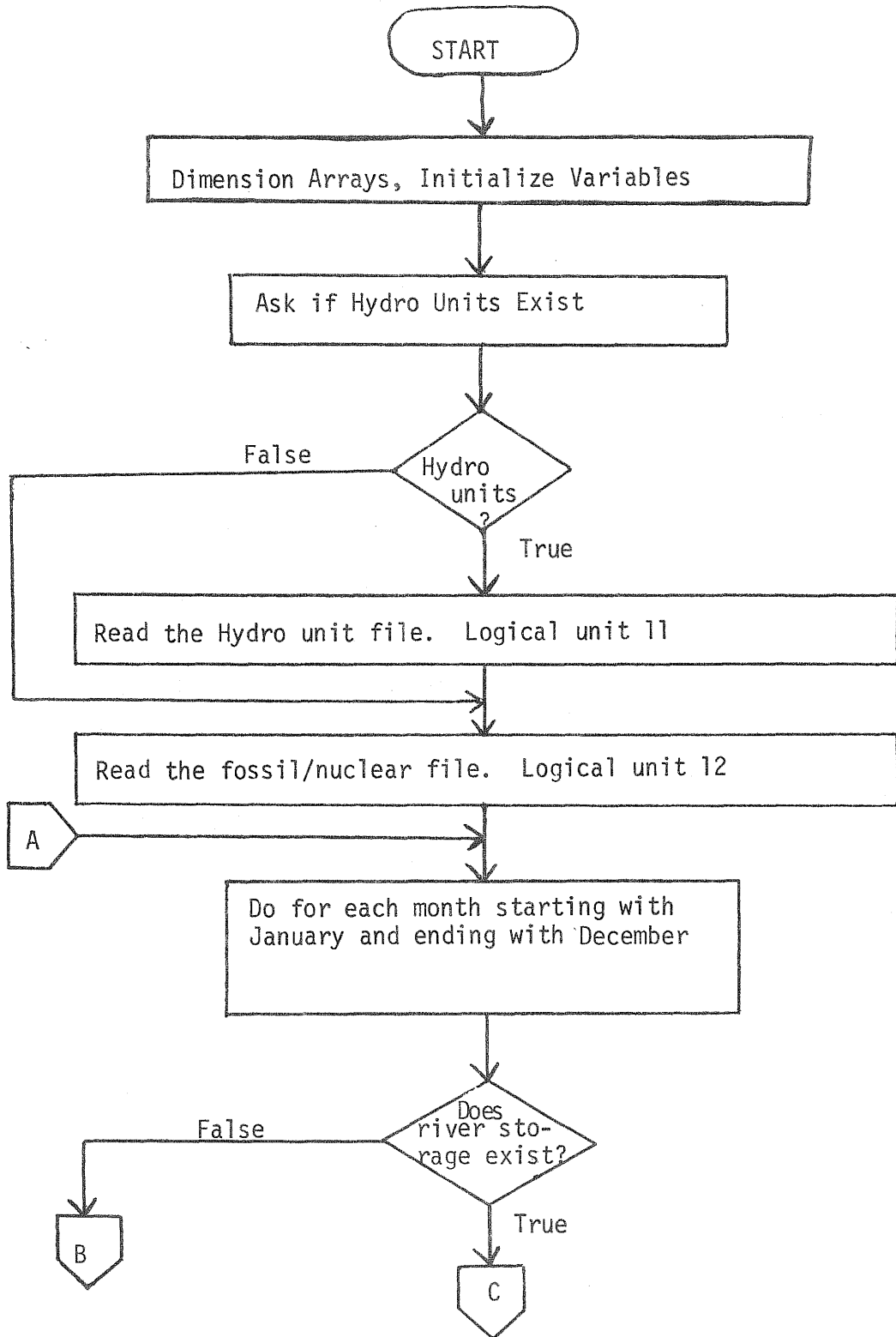
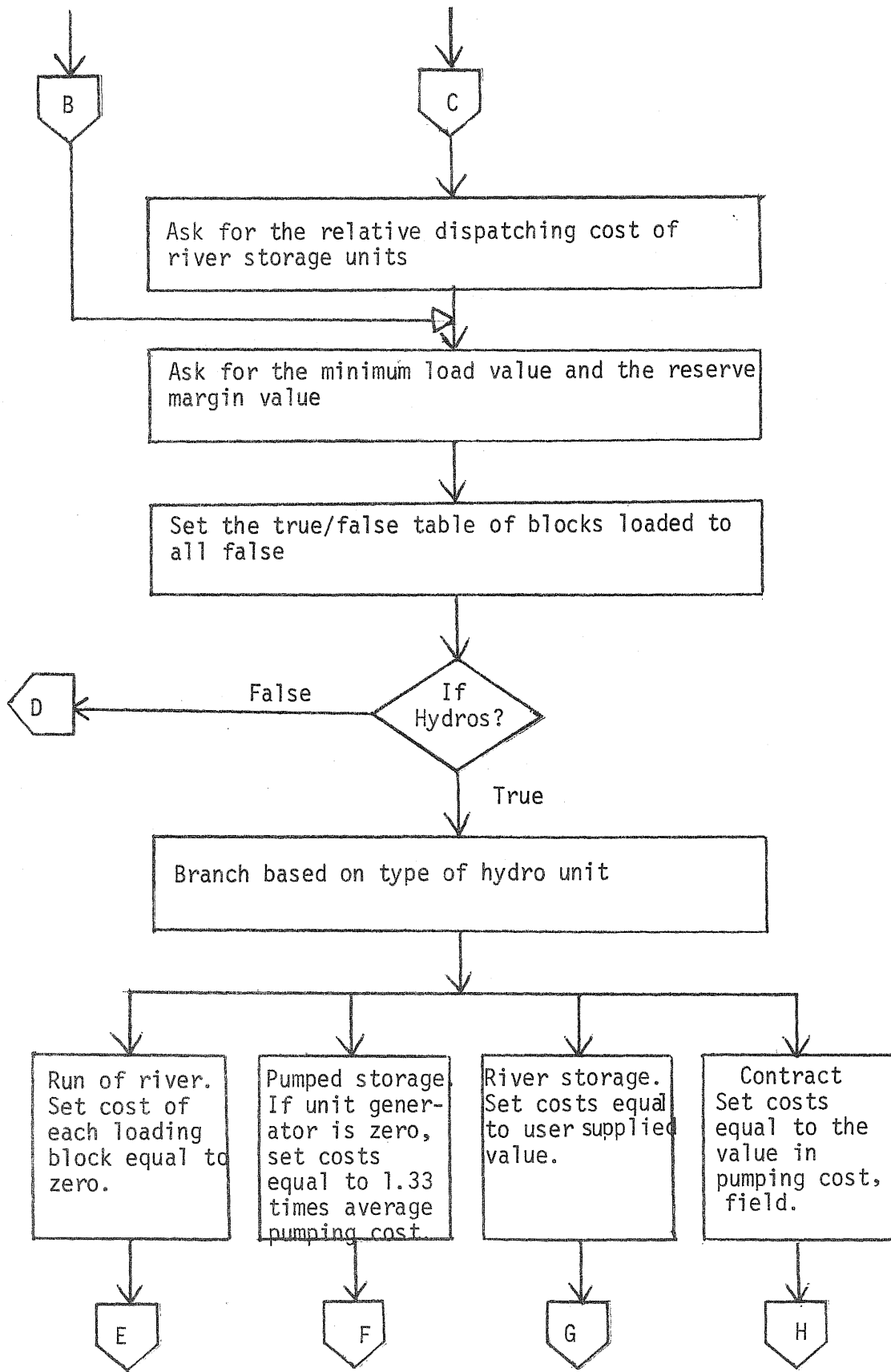
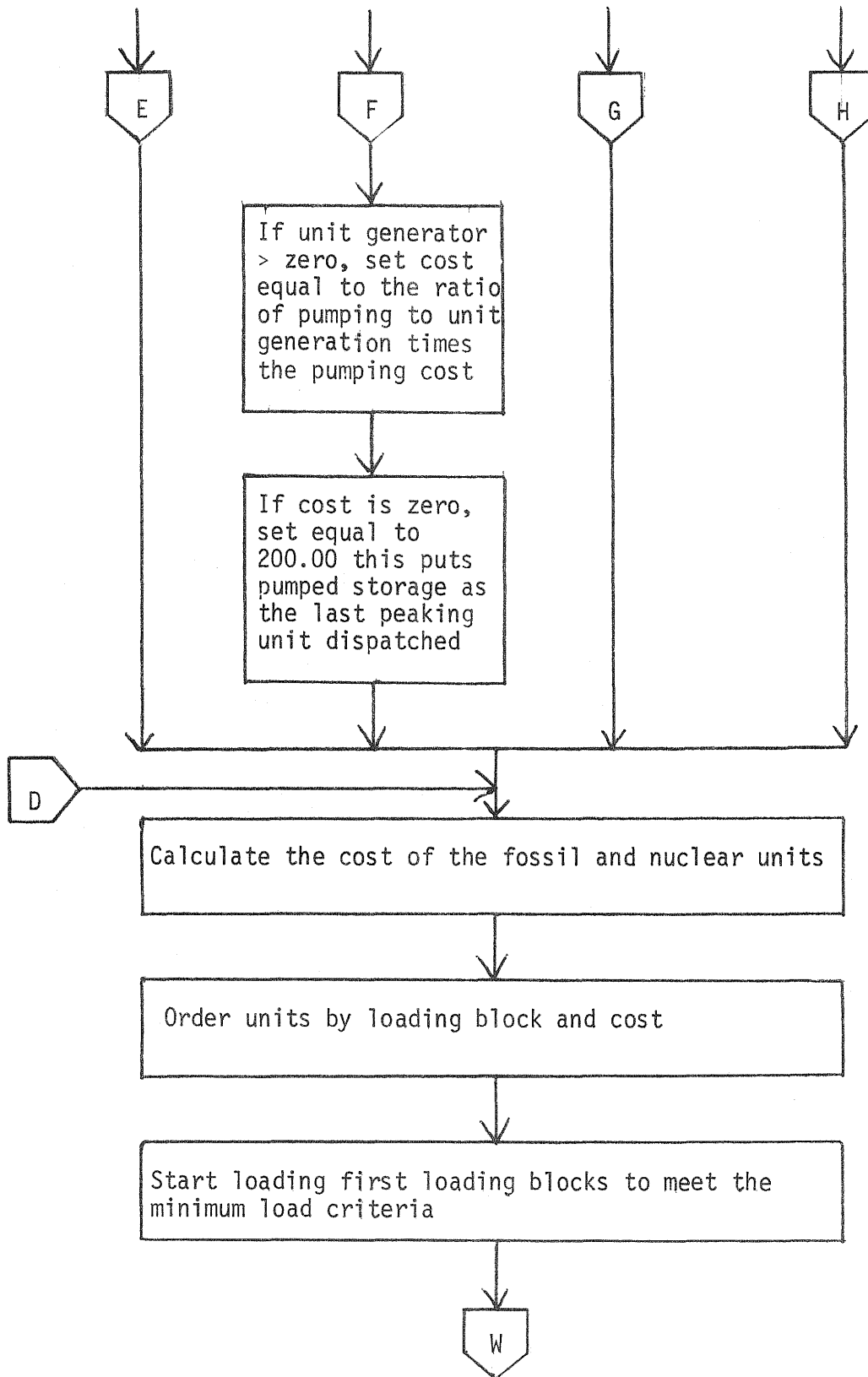


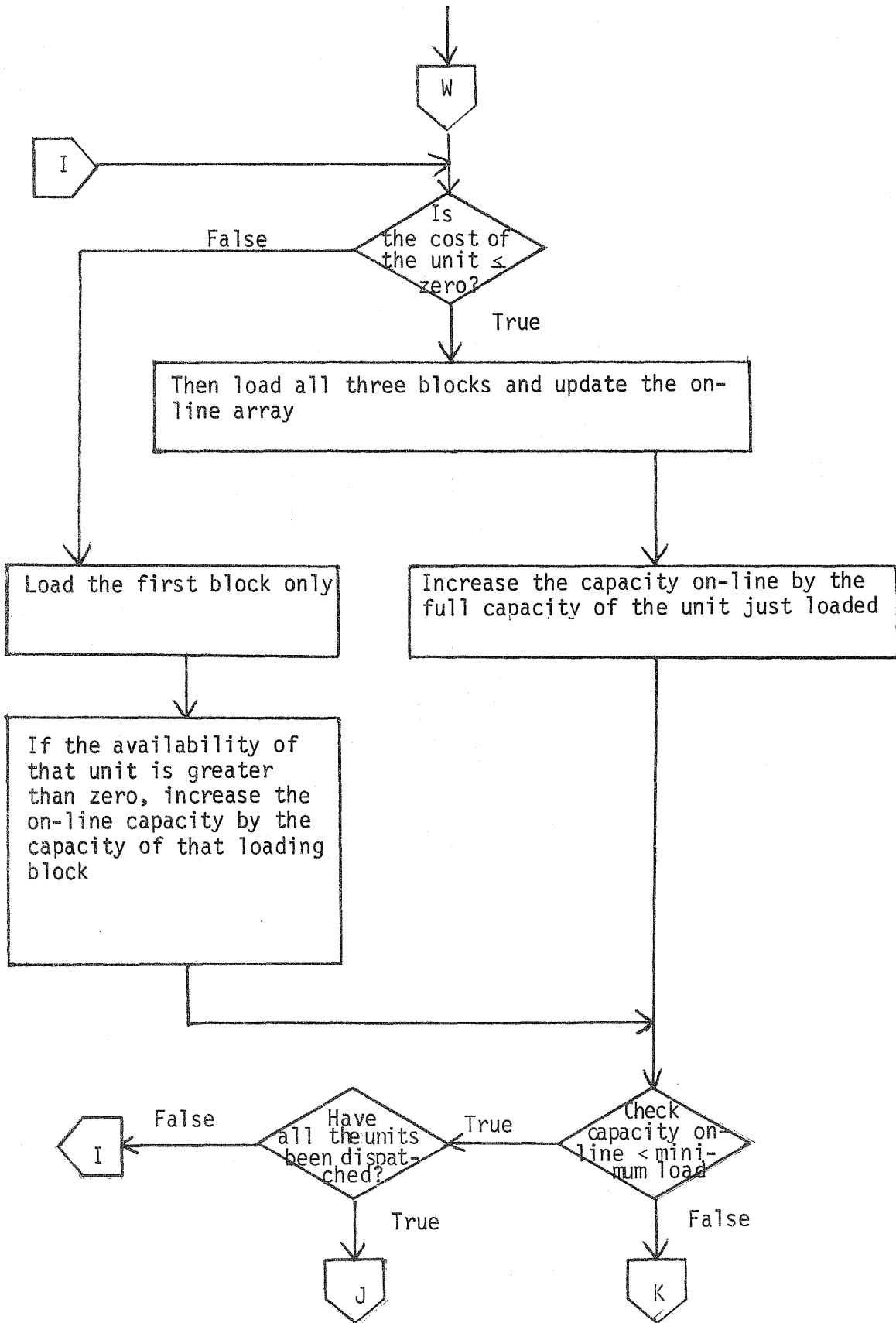
Figure 23 DISPATCH Module Subroutines in the Sequence Called

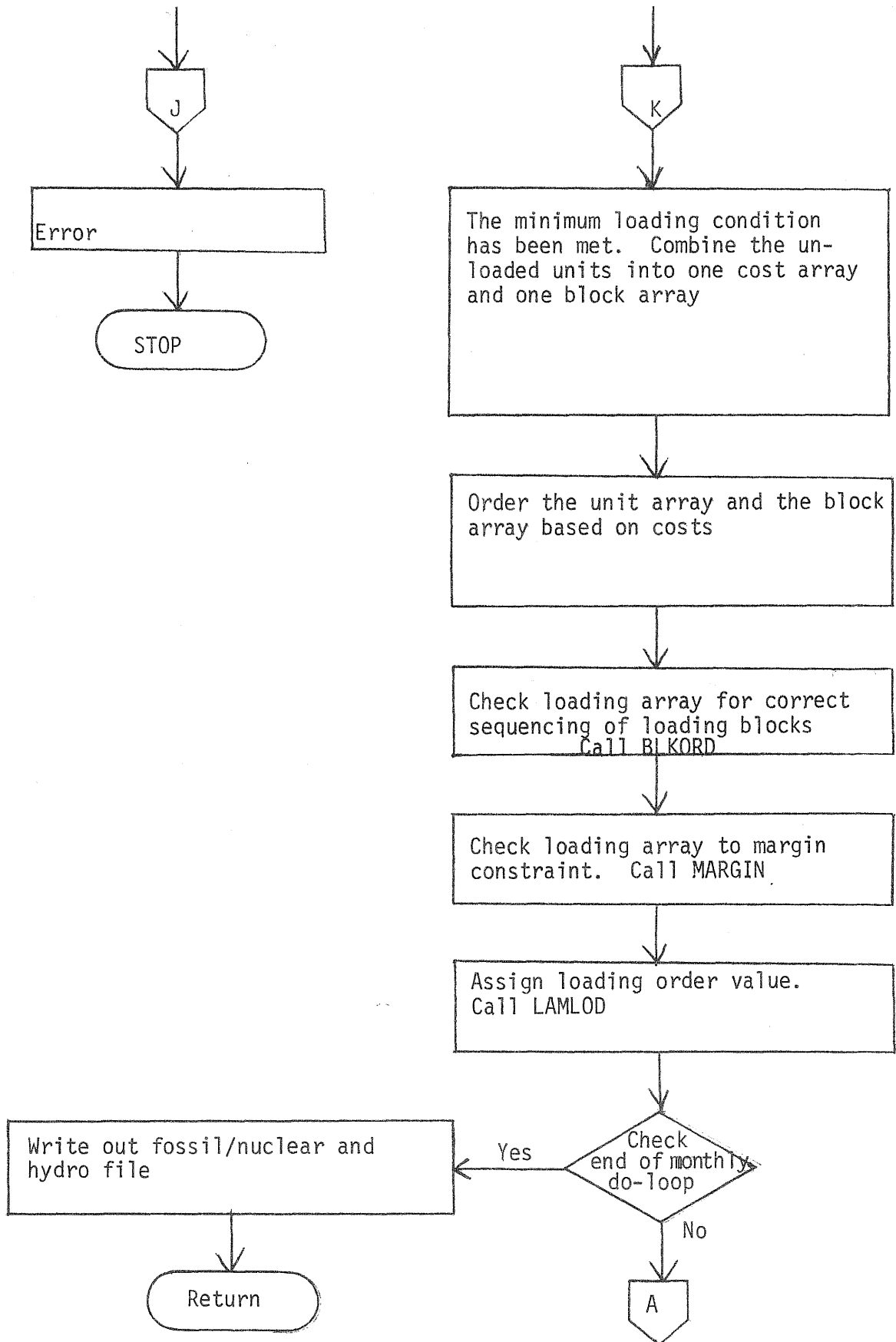
MAIN ROUTINE





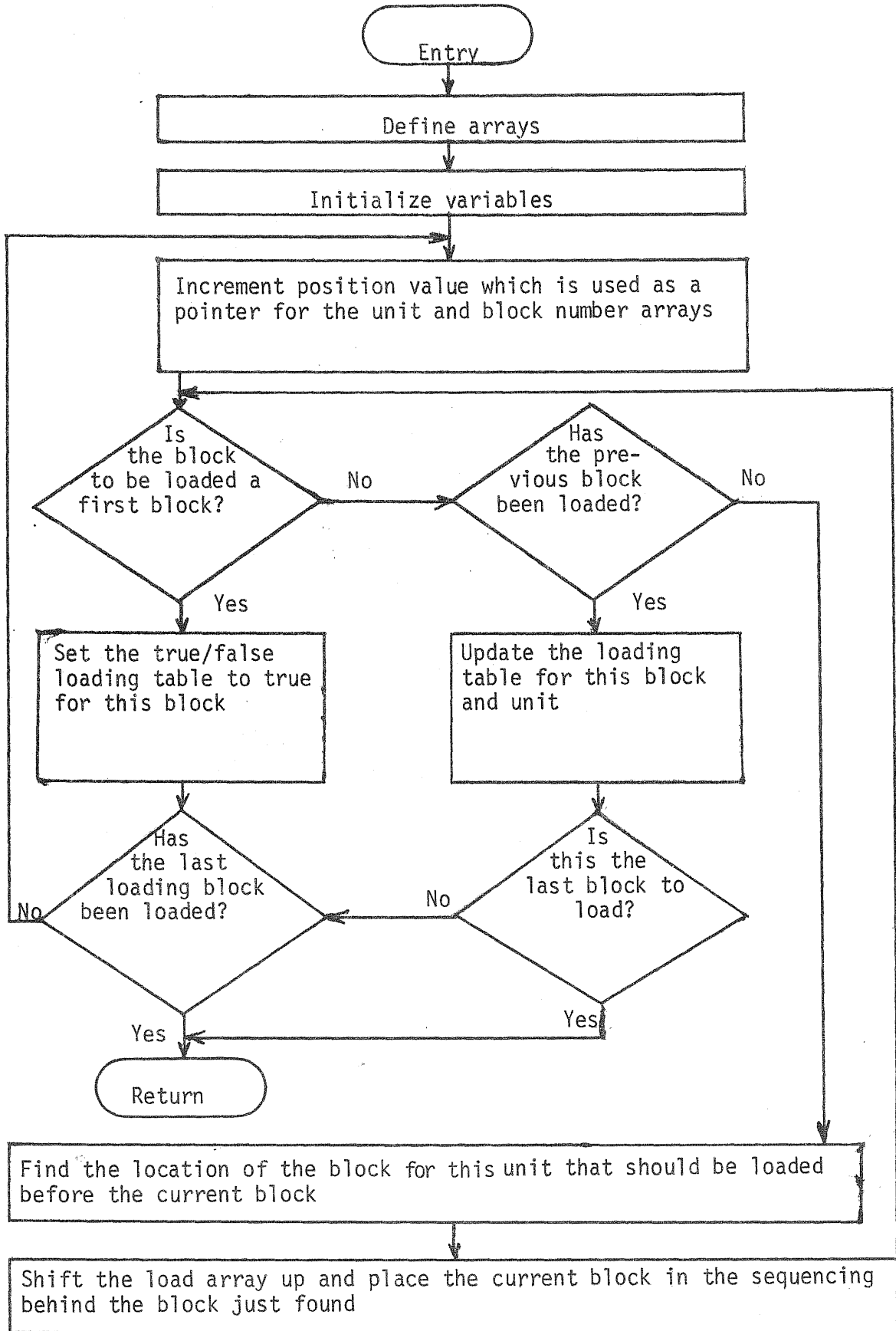






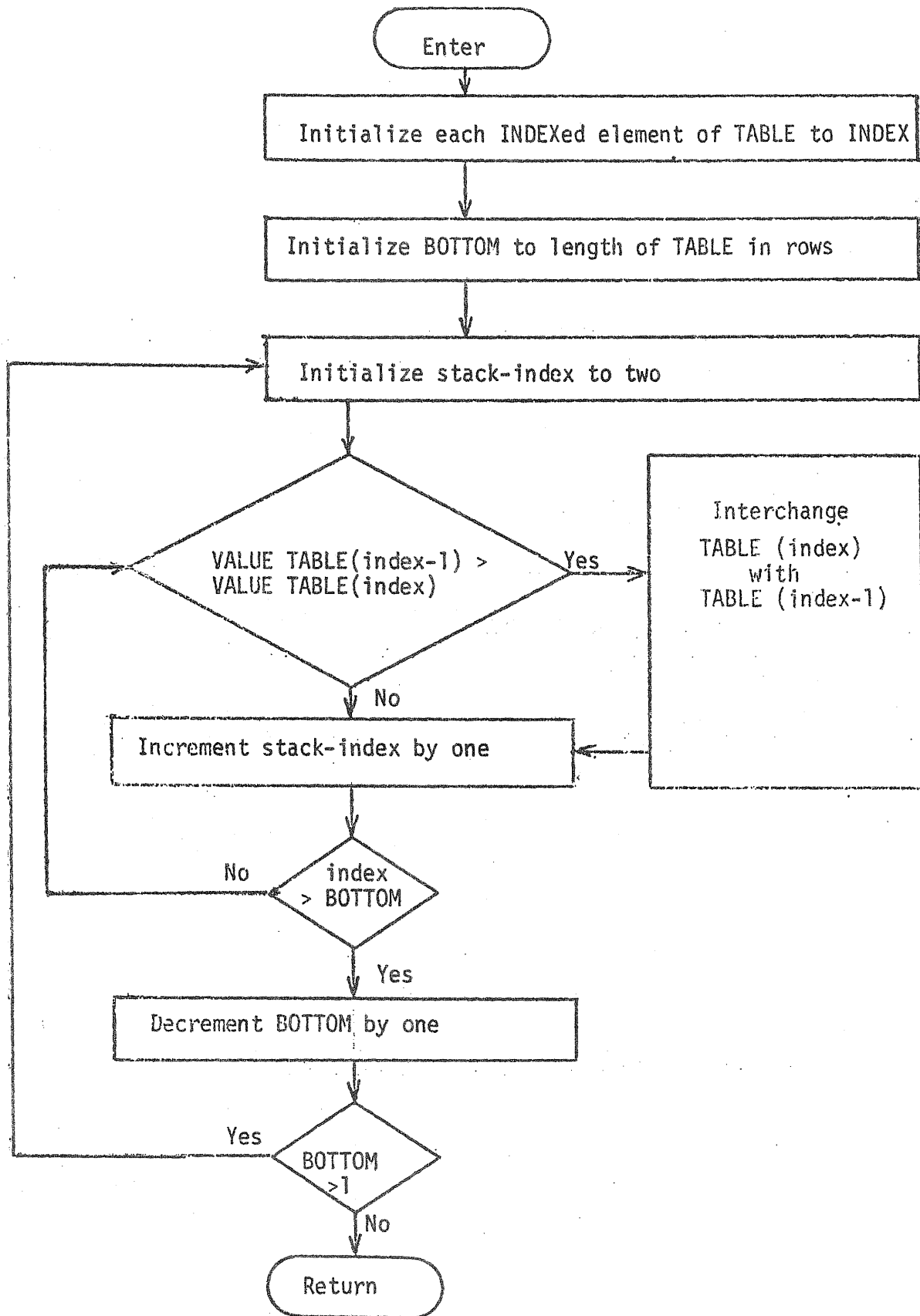
BLKORD Routine

The function of this routine is to make sure that the units are loaded in their proper physical order. That is, block one is loaded before block two and three, etc.



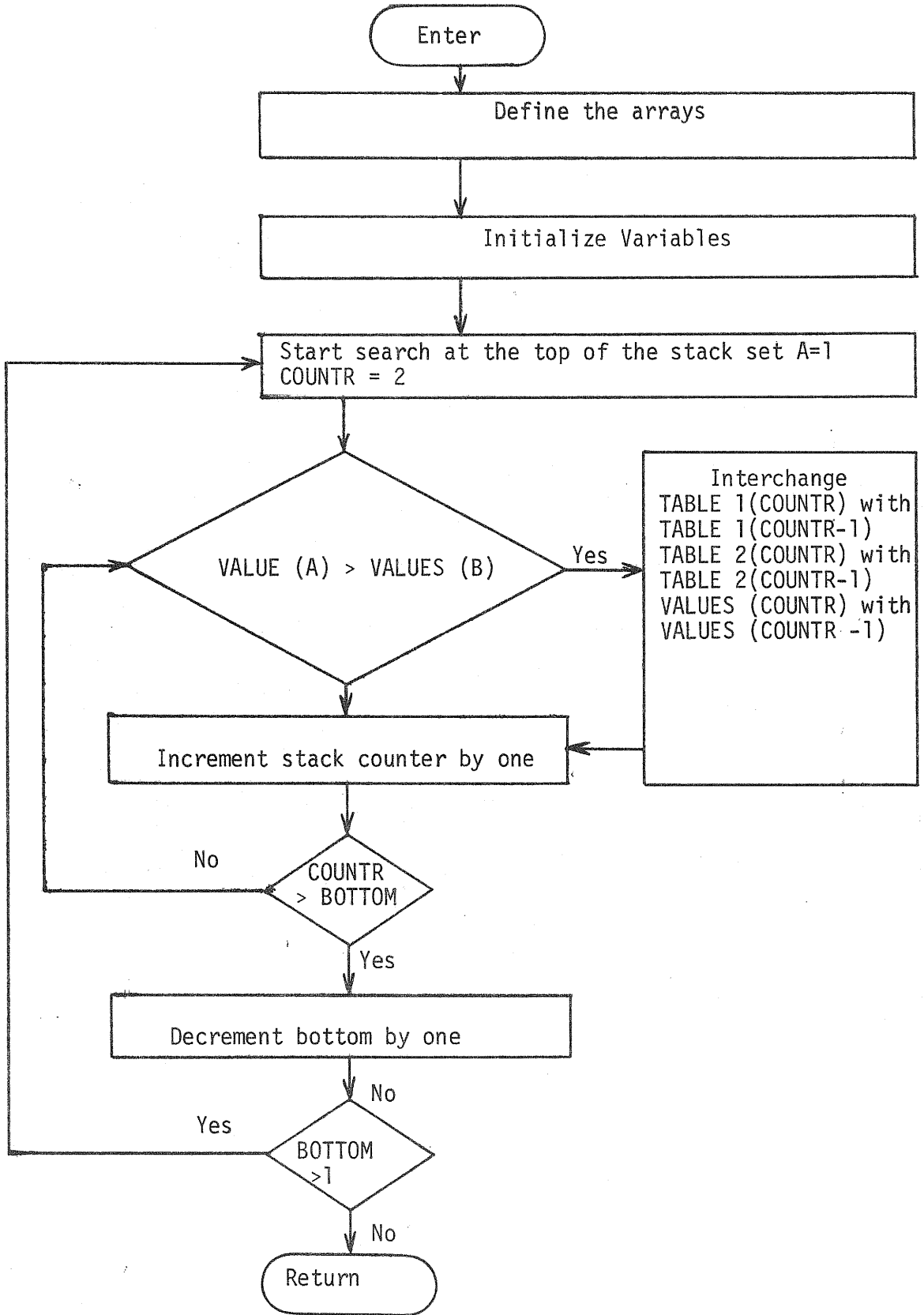
BUBBL1 Routine

This routine orders the array TABLE by the values in the array VALUES. It is designed to order the loading blocks by increasing cost.



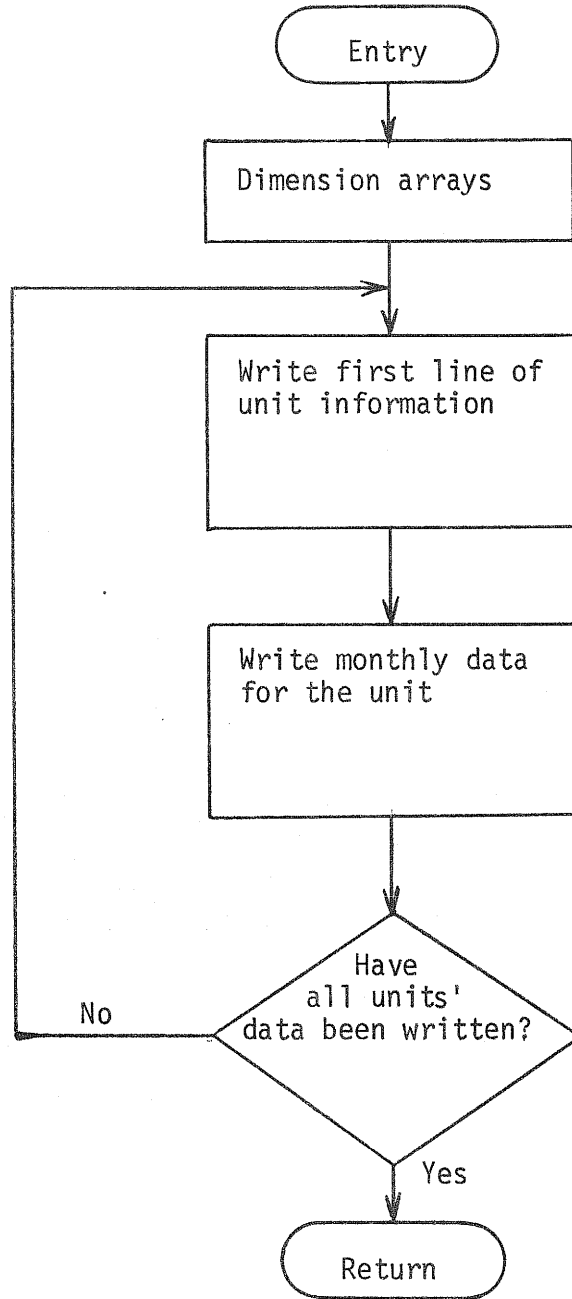
BUBBL2 Routine

This routine orders the two arrays TABLE1 and TABLE2 by the values in array VALUES.



FOSOUT Routine

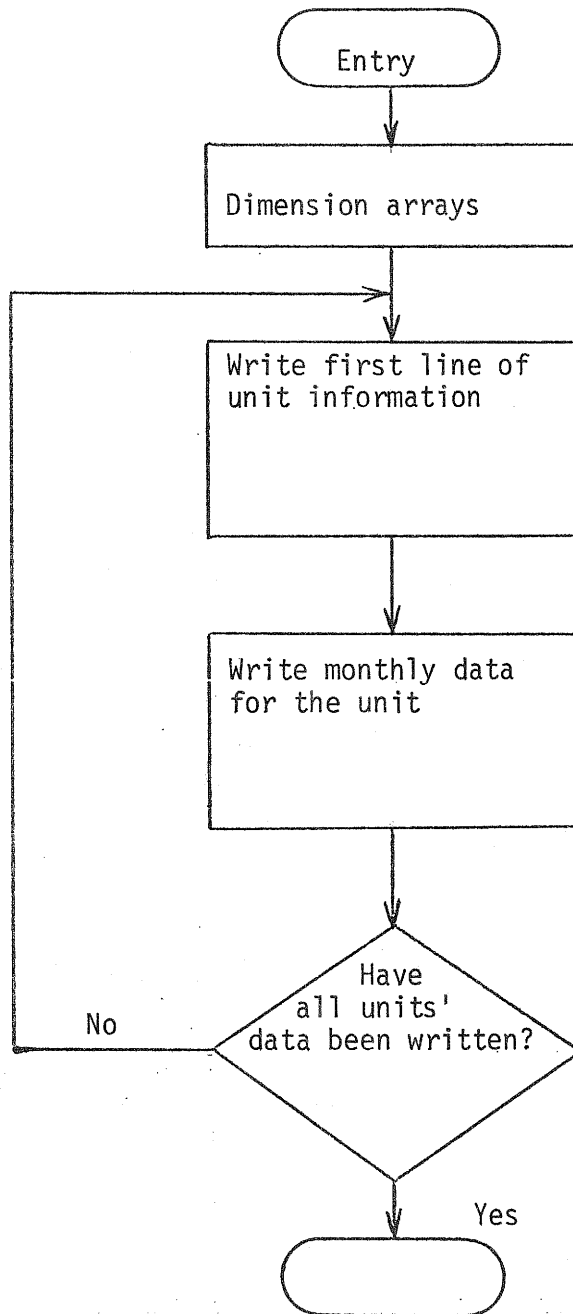
This subroutine is used to write the fossil/nuclear file to logical unit 20.



HYDOUT Routine

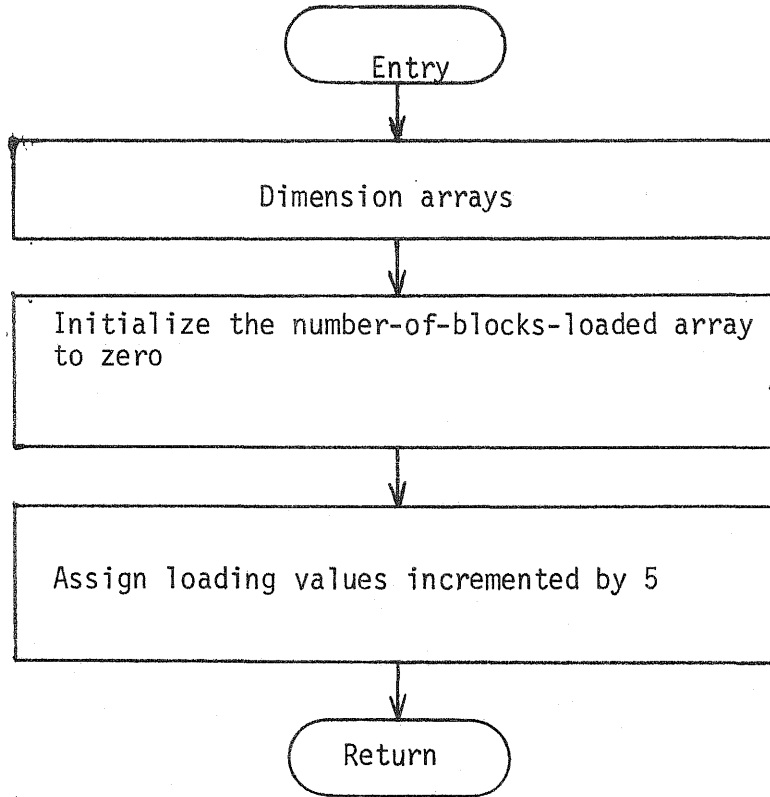
This routine writes the hydro file, if there is one, to logical unit 21.

HYDOUT



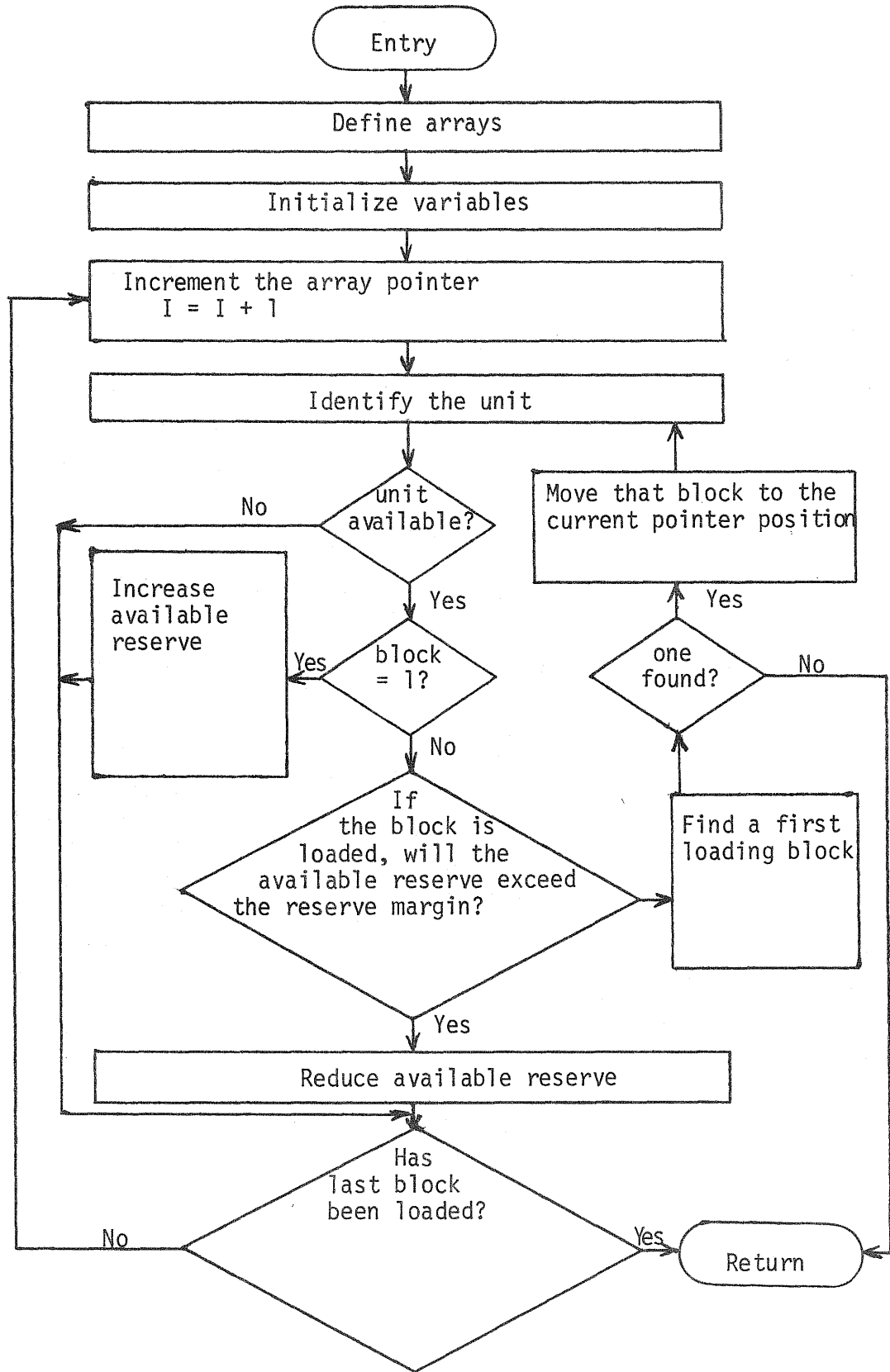
LAMLOD

This routine assigns the loading order values to the generating units using increments of five.



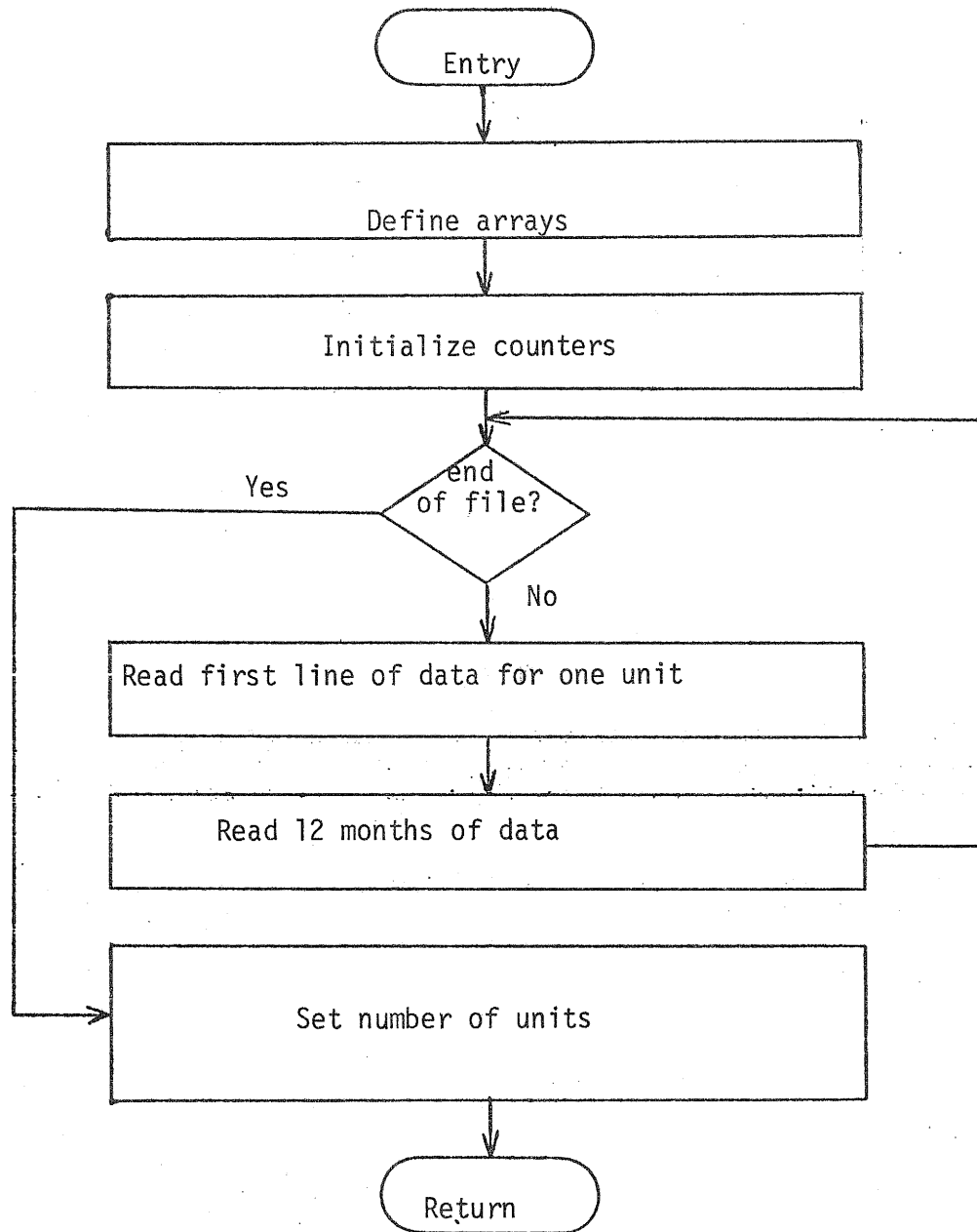
MARGIN Routine

The MARGIN routine loads capacity subject to keeping the available reserve above the user-defined reserve margin. When a loading step is put on line that would cause the available reserve to drop below the reserve margin, the program looks for the next first loading block of a unit and loads it. This causes the available reserve to be increased. If all first loading blocks have been loaded, control is returned to the MAIN routine since the reserve margin constraint can not be satisfied.



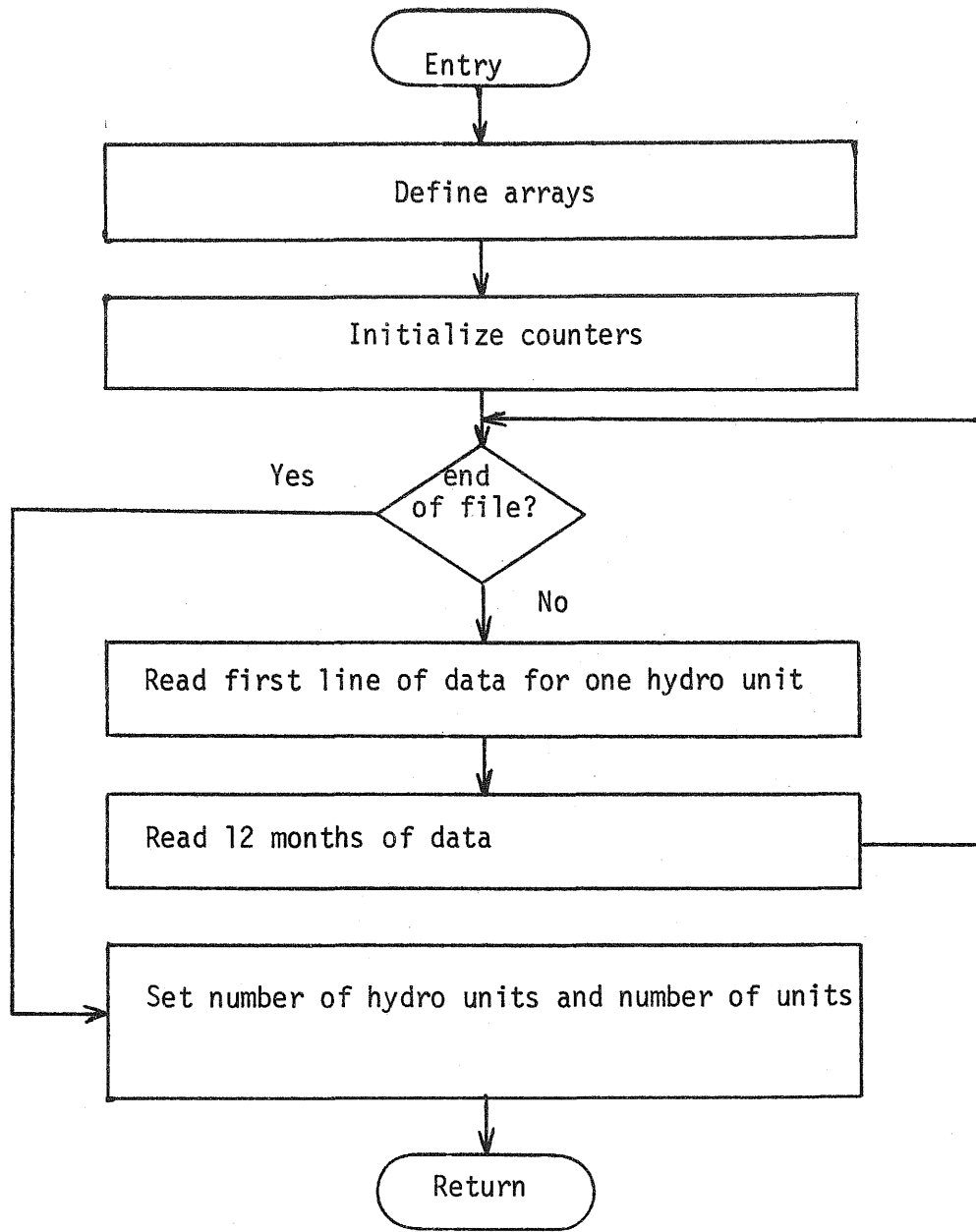
PLTFOS Routine

This routine reads the fossil/nuclear plant file from logical unit 12.



PLTHYD Routine

This routine reads the hydro file from logical unit 11.



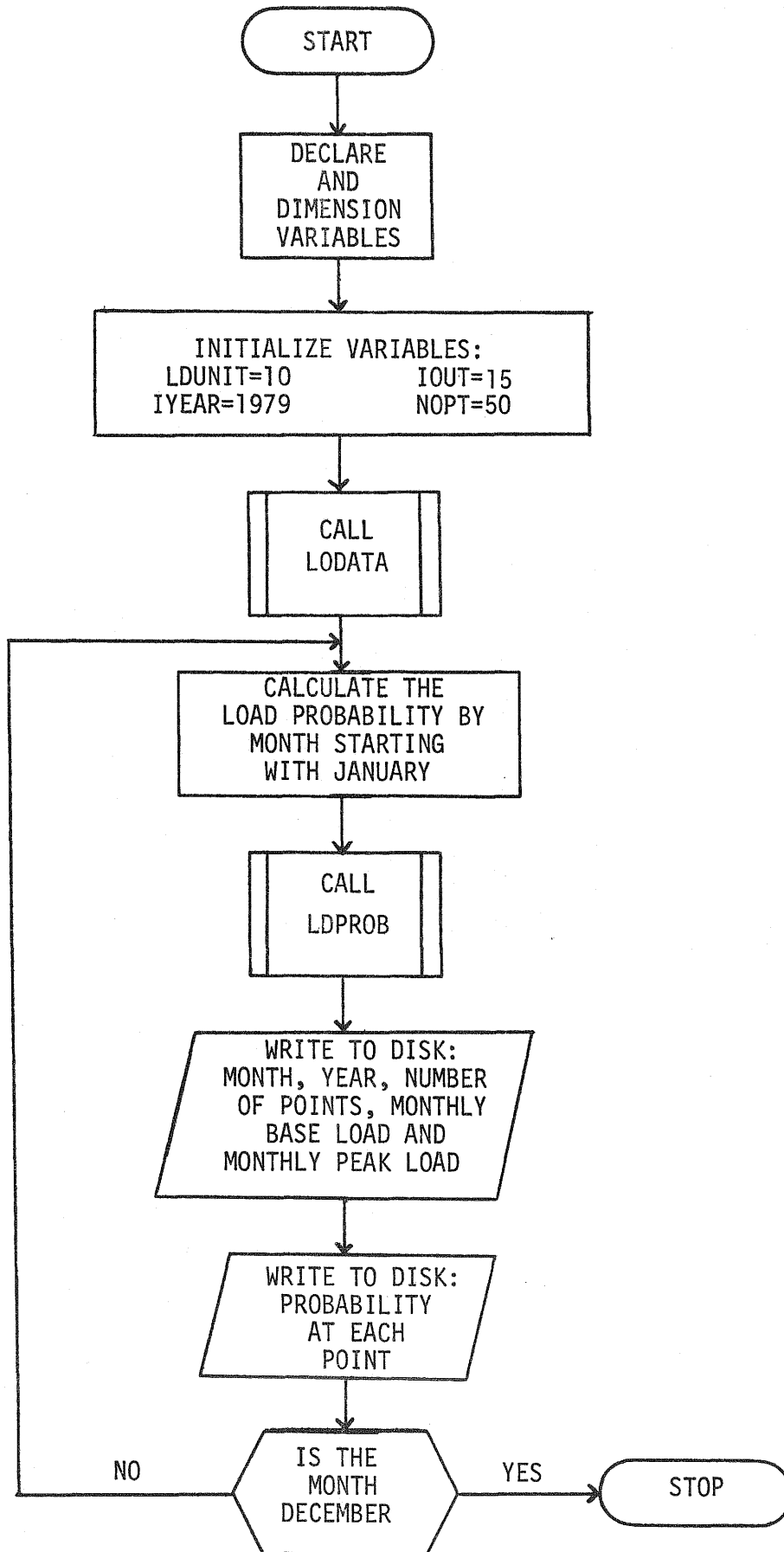
LOAD PROBABILITY MODULE ROUTINES

MAIN Routine

The MAIN portion of this module is to act as a control routine. It calls the two subroutines, LODATA and LOPROB, and writes the calculated load probability curve to the appropriate file.

The input logical file number is 10 for the hourly load data. The output file is number 15. These numbers can be changed by changing the values of variables LDUNIT and IOUT in the MAIN routine.

The number of points on the load probability curve is 50. This is a sufficient number of points for the PCS module. Up to 200 points can be calculated, but this number of points would greatly increase the calculation time of the PCS module but not necessarily increase the accuracy of the calculation.

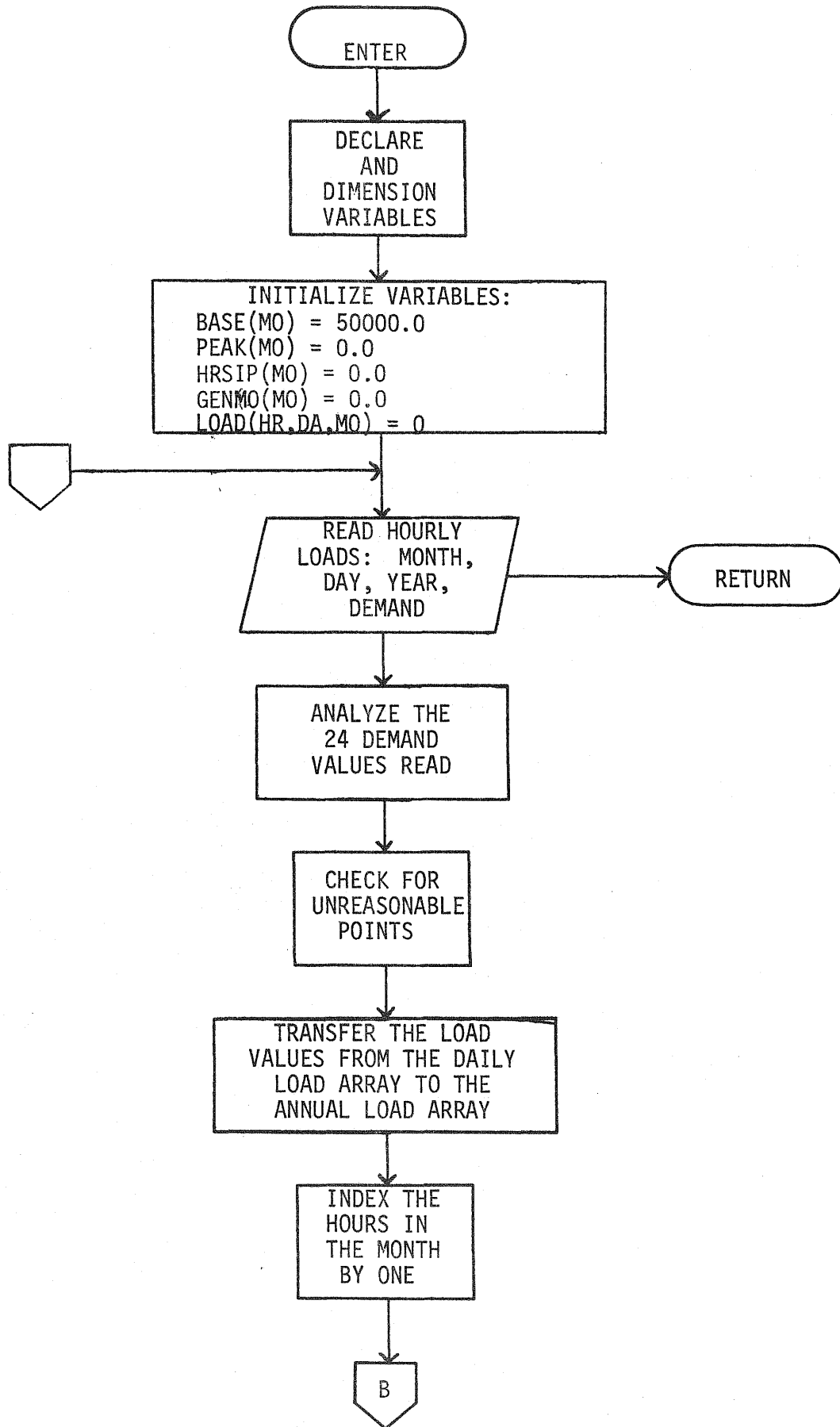


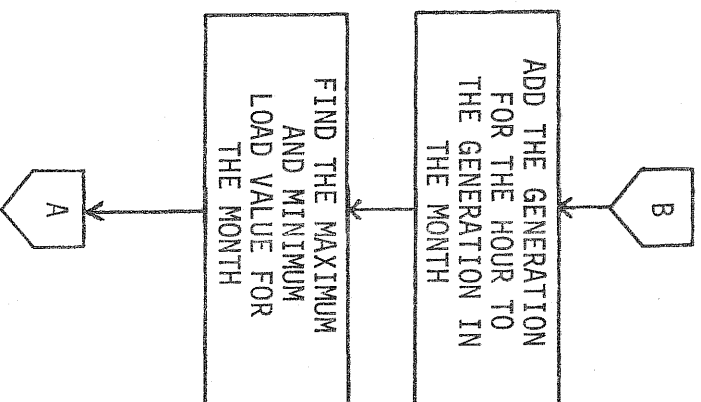
LODATA Routine

The function of this routine is to read and store the hourly load values for future use by the LDPROB routine.

The load values are read one day at a time from logical unit LDUNIT, which is defined in the MAIN routine as 10. These values are then stored in the array LOAD, which represents the year as 12 months each having 31 days with 24 hours. Subsequent reading of this array by-passes zero load values.

Also calculated in this routine are the number of hours in the month, HRSIP, the generation in the month, GENMO, the peak load of the month, PEAK(MO), and the minimum load for the month, BASE(MO).



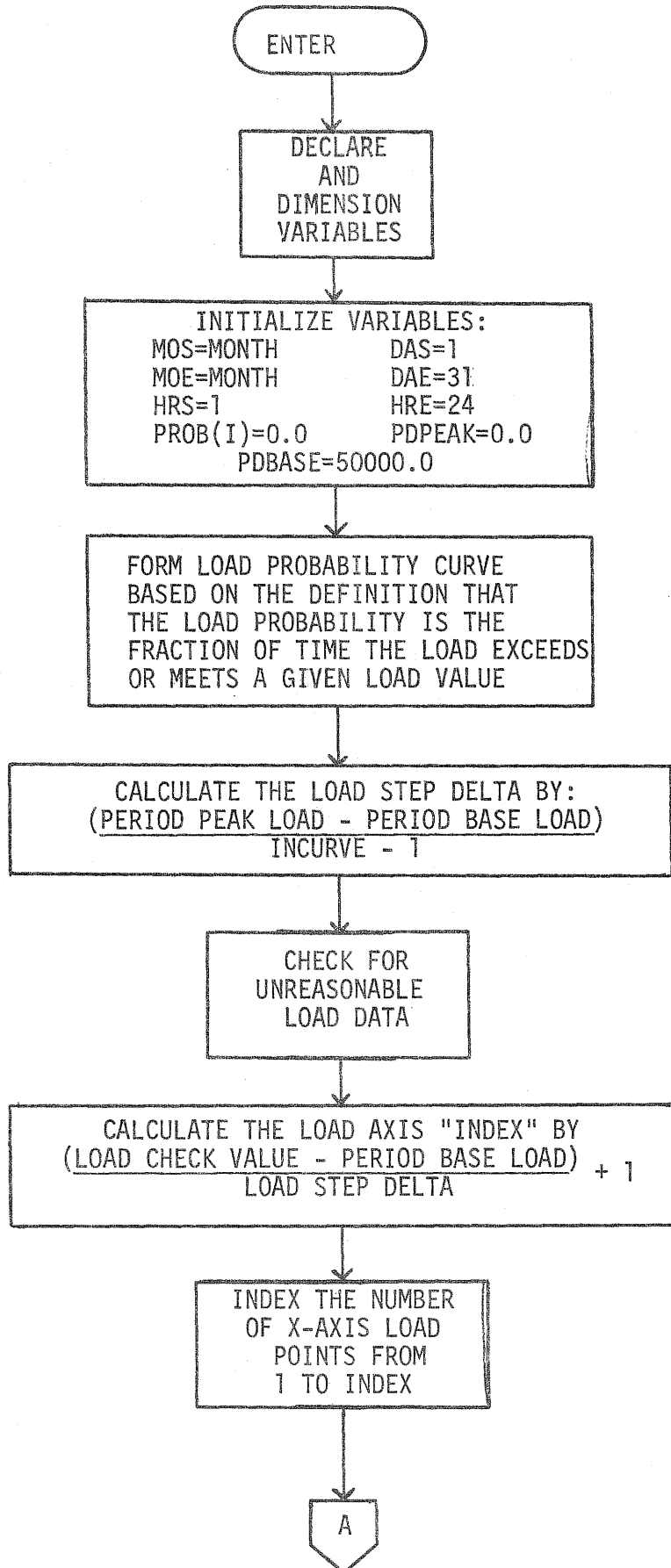


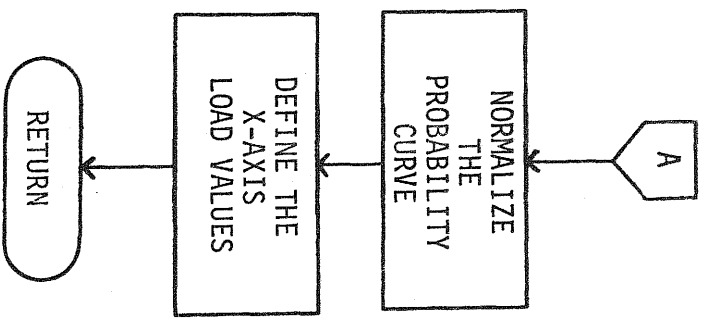
LDPROB Routine

The LDPROB routine calculates the load probability curve based on the hourly loads. The function of this routine is to calculate the load probability curve on a monthly basis for all the days and hours in the month. However, the programming is such that with some changes the load probability curve can be calculated for a variable time period.

The curve is calculated by identifying where the load value would be on the load x-axis of the curve. The y-axis values are incremented by one from the first point to the point where the load value falls. This physically means that for all load values less than or equal to the current value, the load was greater than or equal to the loads for one hour. This process continues until all the non-zero loads for the month have been processed.

The curve is then normalized to the number of hours during which the load is at or above the minimum load. Although not used by the module, the load-axis values are calculated.







APPENDIX A

A Detailed Description of the
PCS Module Algorithms



This appendix is Chapter 4 of
Development of Methodologies and Evaluation of the Effects
of Load Management and Plant Availability Improvements
on the Fuel Cost and Reliability
of an Electric Utility System

A
Dissertation

by

Christos Poseidon, Ph.D.
The Ohio State University

March, 1979

CHAPTER 4

METHODOLOGY FOR THE CALCULATION OF FUEL COST AND SYSTEM RELIABILITY

4.1 Introduction

The basic tool used for fuel costing and reliability calculations in this work is the MARC-IIIB Code previously developed at The Ohio State University [27]. For application of this code to various aspects of the present study, several modifications of this code were made to improve its accuracy and its efficiency. The objective of this chapter is to describe the basic algorithms of the MARC-IIIB Code and the modifications.

The probabilistic simulation used by the MARC Code for production costing and reliability calculations was originally developed by Baleriaux et al and later used by Booth, and adopted in the WASP (Wien Automatic System Planning) by Joy and Jenkins [10-14]. The major difference in the application of probabilistic simulation between MARC-IIIB and WASP is that in the former the load duration curve is expressed as a piece-wise linear function whereas in the latter it is represented by a Fourier series. Reliability can be calculated more accurately using piece-wise linear functions [16].

The author's most significant contribution in this chapter is the development of a new technique of probabilistic simulation which

is approximate but reduces computing time substantially. The second contribution of the author is the presentation of an analysis for multiple-block representation of generating units and the incorporation of two-block representation into the MARC-IIIB Code. In the MARC-IIIB Code the load duration curve is represented by a piece-wise linear function. The possibility of using two-block representation in conjunction with piece-wise linear functions was doubted by the authors of WASP [17] but the validity of the approach is shown in Section 4.3.

The basic aspects of probabilistic simulation using load duration curves are reported elsewhere [13,14]. However, it is necessary to outline the method before the author's modifications are described. This is done in Section 4.2. In Section 4.3 the algorithm for multiple-block representation of generating units is described, and applications are made to test its validity. The calculation of energy generation by multiple-block units makes use of the technique of deconvolution. The usefulness of this technique in a different application is demonstrated in Appendix C. In that application deconvolution is used to calculate the effect of each unit to system reliability. The new technique of approximate probabilistic simulation is described in Section 4.4. In Section 4.5 other important aspects of the MARC Code are discussed.

4.2 Probabilistic Simulation with One Loading Block Representation of Generating Units

With probabilistic simulation, the expected amount of energy generation by each unit is calculated using the system load duration

curve, the availability probability of each unit and the loading order of the system's units. The total fuel cost is then calculated.

In this method two indices of reliability may be defined. These are the "Loss-of-Load Probability", (LOLP), and the "Unserved Energy"

The first index, LOLP, signifies the amount of time that the system cannot satisfy the demand. It is frequently expressed as a fraction (or percentage) of the period of study, or in days per year. The second index, unserved energy, signifies the total amount of energy that the system will be unable to serve in the period of study.

Unserved energy is expressed in MWh. Neither of the above indices contain any information about the frequency of the system's inability to serve the demand. Both of these indices, however, can be used to evaluate the effect of various parameters on system reliability such as changes in load and unit availability.

In the remainder of this section fundamental aspects of probabilistic simulation for one-block units are discussed.

The method of probabilistic simulation is developed using the concepts of load duration, unit loading order, and unit availability probability.

Load duration is the number of hours in a period that the load on the system is equal to or exceeds a given load level. A load duration curve can be calculated using known or forecasted system hourly loads. A typical load duration curve is shown in Figure 4.1.

In this chapter the loading order of units will be assumed to be known. The loading order of units may be decided according to various strategies. Criteria which determine loading order usually include

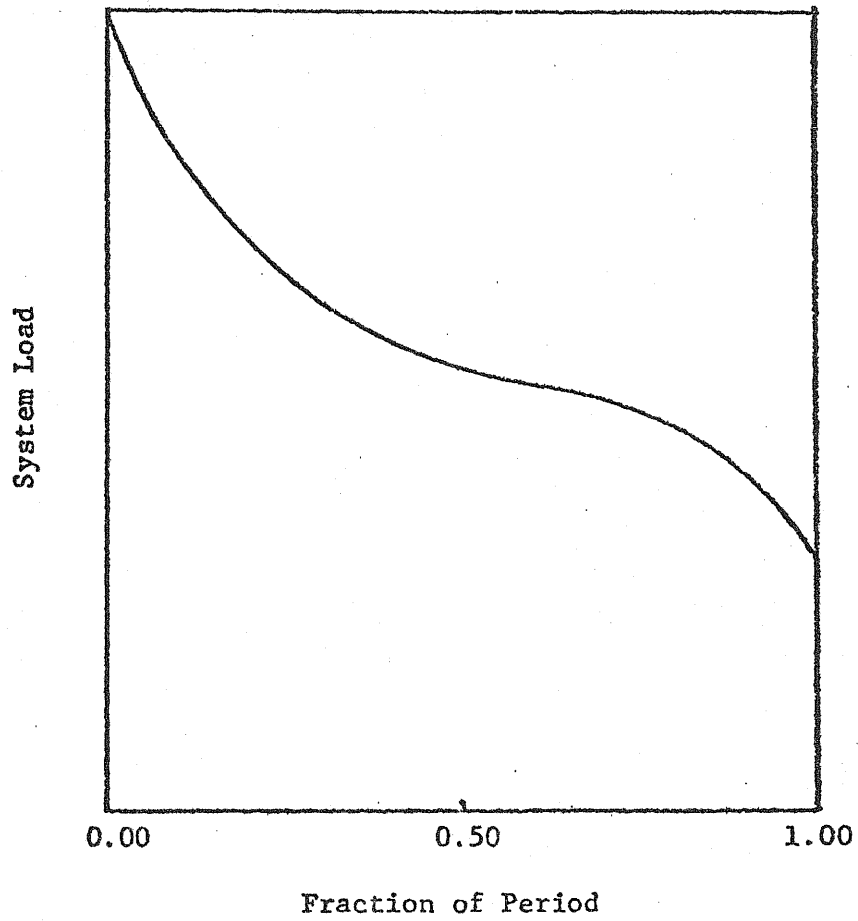


Figure 4.1 A Typical Load Duration Curve

reliability, economic and environmental factors. These factors may be weighted according to the amount of time that a unit is expected to operate in a given day. A more complete discussion of the method used to determine loading order in this work is given in Section 4.5.1.

For purposes of probabilistic simulation unit availability is defined as the "probability that a unit is able to generate electricity when needed" [14]. Frequently, this probability is defined in terms of the forced outage rate, and it is assumed that a unit can be either fully available or fully unavailable. The forced outage rate is defined as:

$$\text{FOR} = \frac{\text{Forced Outage Hours}}{\text{Service Hours} + \text{Forced Outage Hours}} \times 100 \quad (4.1)$$

Availability probability is then defined as

$$p = 1 - \frac{\text{FOR}}{100} \quad (4.2)$$

The definitions expressed by Eq. (4.1) and (4.2) are sufficient for the discussion of the principle of probabilistic simulation. In practical applications, however, partial deratings and maintenance outages are also considered in the definition of p . A more complete discussion about the definition of p in the present work is given in Section 4.5.2.

Assume that in a given time period, T hours, the loading order of N units of a system is

$$C_1, C_2, C_3, \dots, C_N$$

where C_i is the capacity (MW) of the i^{th} unit. We denote the availability probability of unit i by p_i . The probability that unit i is unavailable is

$$q_i = 1 - p_i \quad (4.3)$$

Here it is assumed that a unit is either fully available or fully unavailable. Assuming that the availability probability of each unit is 1, the energy generation of unit i in a period of time T may be calculated by

$$E_i = T \int_{a_i}^{b_i} L(x) dx \quad (4.4)$$

where

E_i = Energy generation of unit i , MWh

$L(x)$ = The "inverted", normalized, system load duration curve

T = The number of hours in the period

$$a_i = \sum_{j=1}^{j=i-1} C_j, \text{ MW}, \quad a_1 = 0$$

$$b_i = a_i + C_i, \text{ MW}$$

The inverted load duration curve, $L(x)$, and the amount of energy produced by unit i are illustrated in Figure 4.2.

If, however, $p_i \neq 1$, a load probability distribution function must be calculated for each unit. The load probability distribution

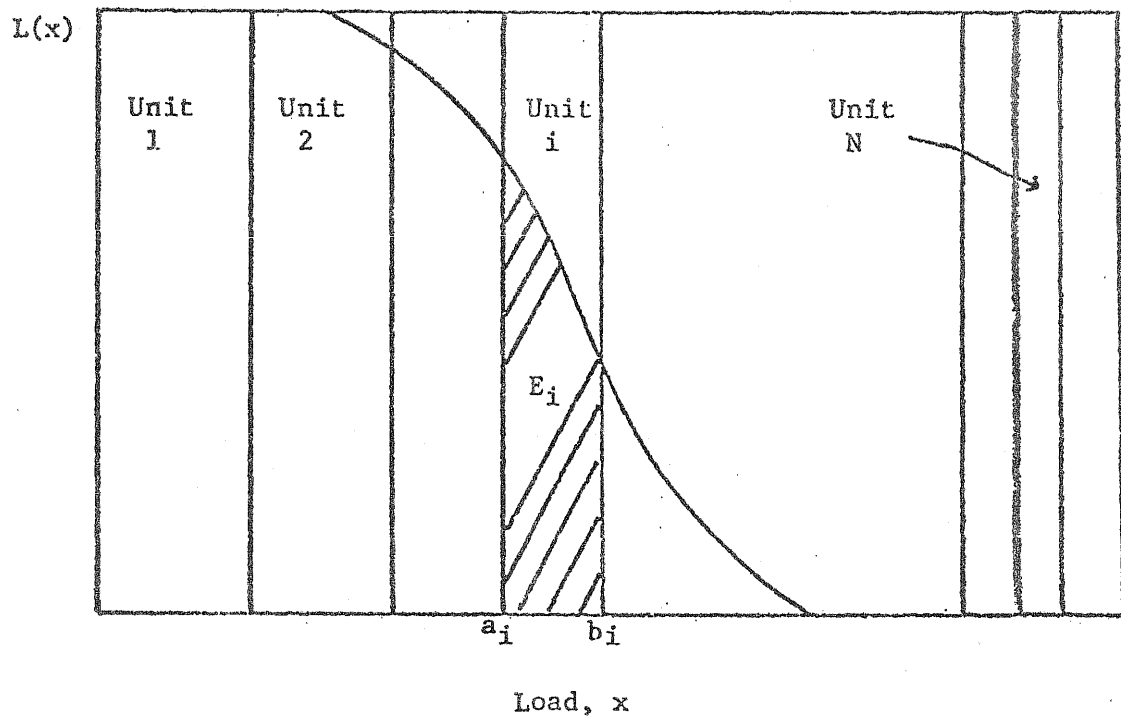


Figure 4.2 A Typical Inverted Load Duration Curve

for each unit depends on the system load distribution, $L(x)$, and on the availability probability and capacity of each unit with higher loading priority. For the first loaded unit, the load probability distribution function is equal to $L(x)$. The load probability distribution function for the remaining units can be found recursively by the following argument.

The energy generated by unit 1 is

$$E_1 = p_1 T \int_0^{C_1} L(x) dx \quad (4.5)$$

where T is the length of the period in hours, x is in MW, and E_1 is in MWh. The amount of energy generated by unit 2 when unit 1 is available is

$$E_{21} = p_1 p_2 T \int_{C_1}^{C_1+C_2} L(x) dx \quad (4.6)$$

The amount of energy generated by unit 2 when unit 1 is not available is

$$E_{22} = q_1 p_2 T \int_0^{C_2} L(x) dx \quad (4.7)$$

Thus, the total amount of energy generated by unit 2 is given by

$$E_2 = E_{21} + E_{22}$$

By rearranging Eq. (4.6) and (4.7), it is seen that E_2 can also be expressed as

$$E_2 = p_2 T \int_{C_1}^{C_1+C_2} EL_1(x) dx \quad (4.8)$$

where

$$EL_1(x) = p_1 L(x) + q_1 L(x-C_1) \quad (4.9)$$

The function $EL_1(x)$ represents the load probability distribution function for unit 2. The remaining functions $EL_i(x)$ can be found similarly. These functions have been called "Equivalent Load Duration Curves", (ELDC). The concept of the ELDC facilitates the calculation of E_i because $EL_i(x)$ can be found by the general recursion relation

$$EL_i(x) = p_i EL_{i-1}(x) + q_i EL_{i-1}(x-C_i) \quad (4.10)$$

$$i = 1, 2, \dots N$$

where

$$EL_0(x) = L(x)$$

Using Eq. (4.10) the amount of energy generated by unit i , E_i , is calculated by

$$E_i = p_i T \int_{a_i}^{b_i} EL_{i-1}(x) dx \quad (4.11)$$

$$i = 1, 2, \dots N$$

where

$$a_i = \sum_{j=1}^{j=i-1} C_j, \quad a_1 = 0$$

and $b_i = a_i + C_i$

$$EL_0(x) = L(x)$$

A set of ELDC's is illustrated in Figure 4.3.

The last ELDC, $EL_N(x)$, includes the effect of outages of unit N. LOLP and Unserved Energy are calculated by

$$LOLP = EL_N(B) \tag{4.12}$$

$$\text{Unserved Energy} = T \int_B^{\infty} EL_N(x) dx \tag{4.13}$$

where

$$B = \sum_{i=1}^N C_i$$

The LOLP and Unserved Energy are also illustrated in Figure 4.3.

4.3 Multiple-Block Representation of Generating Units

The loading order of units as specified in Section 4.2 assumes that each unit is loaded to full capacity in one step. In the actual situation, depending upon a system's constraints and objectives (i.e., spinning reserve requirements, economic factors), a unit may be

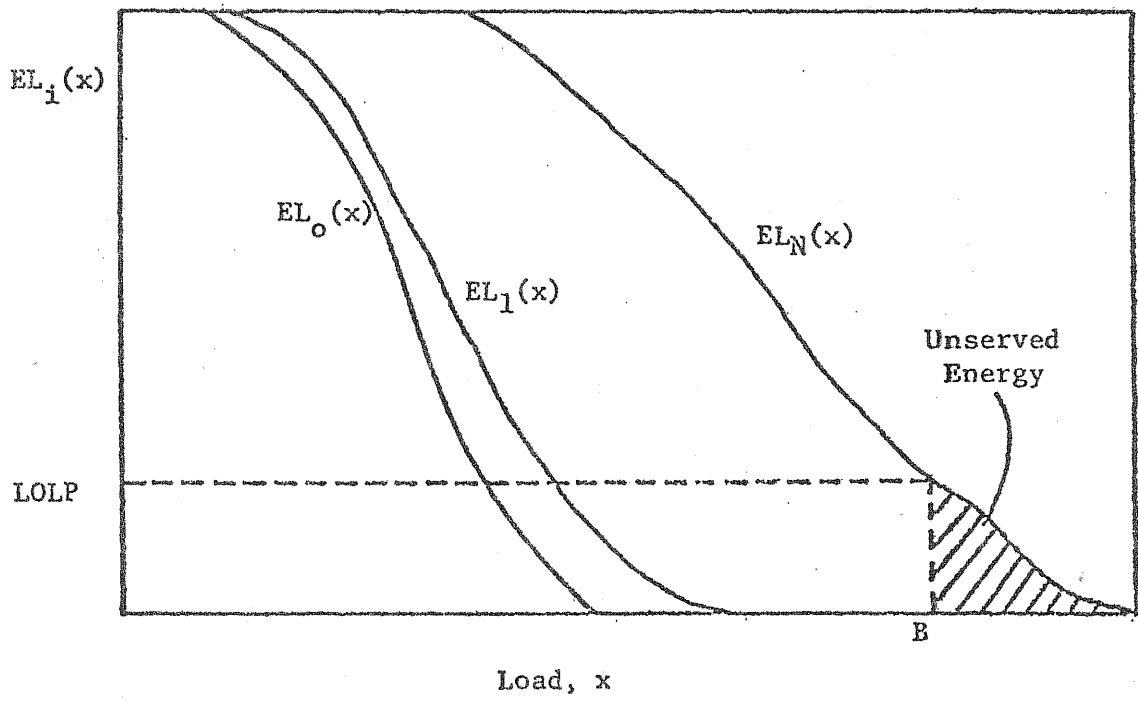


Figure 4.3 A Set of Equivalent Load Duration Curves

loaded up to a certain fraction of its capacity and then a different unit may be loaded before the previous unit is loaded to full capacity. In addition, assuming that suitable outage data are available, partial outages may be simulated by assigning different availability probabilities to different blocks of the same unit. It is, therefore, desirable to provide the MARC Code with the capability of multiple block representation of generating units.

Basic concepts which are useful for multiple loading block representation have been reported in [18,19]. Two block unit representation in conjunction with Fourier series representation of the load duration curve has been used in the WASP Code [15]. In this section the algorithm of multiple block representation is described and applications in conjunction with a piece-wise linear load duration curves are made. The use of piece-wise linear curves has been shown to lead to a more accurate calculation of system reliability [16].

4.3.1 Algorithm of Multiple Block Representation

For simplicity of explanation in the following derivation it is assumed that only one unit in the system is loaded in two steps (2-block representation). Further, it is assumed that both blocks have the same availability probability. At the end of this section the algorithm will be generalized to include units loaded in multiple steps and units with different availability probabilities assigned to each block.

A system is considered consisting of N units. The loading order of units and blocks is $C_1, C_2, \dots, C_{j-1}, C_{j1}, C_{j+1}, \dots, C_k, C_{j2}, C_h, C_{h+1}, \dots, C_N$ where C_i represents the capacity of block i. The series above indicates that units 1 through j-1 are represented by only one block. Unit j is represented by two blocks with capacities C_{j1} and C_{j2} of which only C_{j1} is loaded immediately after C_{j-1} . Following C_{j1} , the one-block units C_{j+1} through C_k are loaded, then C_{j2} is loaded, and then each of the remaining one-block units are loaded. The ELDC corresponding to each block (or unit) are termed $EL_0, EL_1, \dots, EL_{j-2}, EL_{j-1}, EL_j, \dots, EL_{k-1}, EL_k, EL_{h-1}, EL_h, \dots, EL_{N-1}$. The ELDC for blocks 1, 2, ... k are calculated according to the procedure of Section 4.2 as

$$\begin{aligned}
 EL_0(x) &= L(x) \\
 EL_1(x) &= p_1 EL_0(x) + q_1 EL_0(x-C_1) \\
 &\vdots \\
 EL_{k-1}(x) &= p_{k-1} EL_{k-2}(x) + q_{k-1} EL_{k-2}(x-C_{k-1})
 \end{aligned}
 \tag{4.14}$$

Energy generation by blocks 1, 2, ... k is calculated using Eq.

(4.14) as

$$E_n = p_n T \int_{a_n}^{b_n} EL_{n-1}(x) dx
 \tag{4.15}$$

$$n = 1, 2, \dots, k$$

where

$$a_n = \sum_{m=1}^{m=n-1} C_m, \quad a_1 = 0$$

$$b_n = a_n + C_n$$

If the same procedure were to be used to calculate the ELDC for C_{j2} and the amount of energy generated by C_{j2} , E_{j2} , this ELDC would include the effects of outages of C_{j1} , and the calculated energy generation would include energy generated by block j_2 in replacement of block j_1 when j_1 was unavailable. This is physically impossible since it has been assumed here that when j_1 is on outage j_2 must also be on outage. The effect of outages of block C_{j1} can be removed (deconvolved) from the load probability distribution for C_{j2} , $EL_k(x)$, by using the expression

$$\tilde{EL}_k(x) = \frac{EL_k(x) - q_j \tilde{EL}_k(x - C_{j1})}{P_j} \quad (4.16)$$

Equation (4.16) expresses the load probability distribution function if the effects of outages of C_{j1} are not included. The energy generated by j_2 is calculated by

$$E_{j2} = P_j T \int_{a_{j2}}^{b_{j2}} \tilde{EL}_k(x) dx \quad (4.17)$$

where $\tilde{EL}_k(x)$ is the modified distribution function,

and

$$a_{j2} = \sum_{m=1}^{m=k} C_m,$$

$$b_{j2} = a_{j2} + C_{j2}$$

For the calculation of the energy generation of subsequent units, the effect of the outages of (the total) unit C_j must be included in the distributions $EL_{h-1}(x)$, $EL_h(x)$, ..., $EL_N(x)$. Because of the recursive character of these functions, it is sufficient that the effect of outages of unit C_j be included in $EL_{h-1}(x)$. Thus,

$$EL_{h-1}(x) = p_j \tilde{EL}_k(x) + q_j \tilde{EL}_k(x - C_j) \quad (4.18)$$

where $C_j = C_{j1} + C_{j2}$

Using Eq. (4.18)

$$E_h = p_h T \int_{a_h}^{b_h} EL_{h-1}(x) dx \quad (4.19)$$

where

$$a_1 = \sum_{m=1}^{m=h-1} C_m,$$

and

$$b_h = a_h + C_h$$

the ELDC for the remaining units can be calculated as in Section 4.2.

When more than one unit is represented by two blocks, the above procedure can be applied to each such unit.

It is now supposed that the probability of operation at full capacity is p_1 , at a derated capacity, C_{j1} , is p_2 , and of unavailability is q so that

$$p_1 + p_2 + q = 1.0$$

Therefore,

$$P_{j1} = p_1 + p_2,$$

$$q_{j1} = q,$$

$$P_{j2} = p_1$$

The energy of the second block, capacity C_{j2} , must be calculated using $\tilde{E}L_k(x)$ which does not include the effects of outage of the first block, and is given by Eq. (4.16). For subsequent ELDC, the two blocks may be included into the distribution using

$$EL_{h-1}(x) = p_1 \tilde{E}L_k(x) + p_2 \tilde{E}L_k(x - C_{j2}) + q \tilde{E}L_k(x - C_{j1} - C_{j2}) \quad (4.20)$$

A plant may be loaded in more than two steps. In this case the calculation of energy generation can be made more accurately by multiple-block representation of plants in probabilistic simulation. Multiple block representation has been discussed in Reference [18]. In the following algorithm it is assumed that unit j is divided into n loading blocks, and that the availability probability of all blocks of unit j is the same (p_j). For simplicity of notation the ELDC for the $M+1^{\text{th}}$ block of unit j before removing the effects of outages of the first M blocks of j is termed as Y_1 . The ELDC after removing the effects of these blocks is termed as \tilde{Y}_1 . The ELDC for the unit (or block) which follows the $M+1^{\text{th}}$ block of unit j in loading order is termed as Y_2 . Assuming the same availability probability (2-state model) for all blocks of j ,

$$\tilde{Y}_1(x) = \frac{Y_1(x) - q_j \tilde{Y}_1(x - \sum_{i=1}^{i=M} C_{ji})}{p_j} \quad (4.21)$$

and

$$Y_2(x) = p_j \tilde{Y}_1(x) + q_j \tilde{Y}_1(x - \sum_{i=1}^{i=M+1} C_{ji}) \quad (4.22)$$

The function $\tilde{EL}_k(x)$ in Eq. (4.16) is formed from pre-calculated values of the same function. Numerically, Eq. (4.16) is written as

$$\tilde{EL}_k(x_i) = \frac{EL_k(x_i) - q_j \tilde{EL}_k(x_i - C_{j1})}{p_j} \quad (4.23)$$

where i indicates a point on the load axis. If, however,

$$C_{ji} < x_i - x_{i-1}$$

$\tilde{EL}_k(x_i)$ cannot be calculated in terms of $\tilde{EL}_k(x_i - C_{j1})$. In this case $\tilde{EL}_k(x_i)$ is calculated as follows [28]. Because \tilde{EL}_k is a piece-wise linear function, $\tilde{EL}_k(x_i)$ and $\tilde{EL}_k(x_{i-1})$ are points on a straight line. Thus, by interpolation

$$\tilde{EL}_k(x_i - C_{j1}) = \frac{x_{i-1} - x_i + C_{j1}}{x_{i-1} - x_i} \tilde{EL}_k(x_i) - \frac{C_{j1}}{x_{i-1} - x_i} \tilde{EL}_k(x_{i-1}) \quad (4.24)$$

By introducing Eq. (4.24) into Eq. (4.23), $\tilde{EL}_k(x - C_{j1})$ is eliminated and Eq. (4.24) is then solved for $\tilde{EL}_k(x_i)$.

4.3.2 Numerical Evaluation

The two-block representation algorithm was incorporated into the MARC-IIIB Code, for the case of equal availability probabilities (2-state model) of both blocks of the same unit. A listing of the algorithm is provided in Appendix B. This algorithm was validated using three tests. In the first test, the function $\tilde{EL}_k(x)$ was first calculated according to the algorithm described, and then it was recalculated omitting block j_1 . The two functions were found

to be equal at all points. In some cases, however, computer truncation error was observed. This error was eliminated by using "double precision". This test proves that Eq. (4.16) produces the correct function, $\tilde{EL}_k(x)$ when block j1 is removed from the distribution $EL_k(x)$. In the second test, the energy generated by block j2 was calculated by first considering j2 as the second block of unit j, and then by considering j2 as an independent unit. In both cases j1 and j2 were assigned the same availability probability. It was found that in the first case the energy generation of j2 was less. This result agrees with what would be expected, since in the second case, block j2 can generate additional energy in replacement of j1, when j1 is on outage. In the third test, the energy generation of unit h (the next one to j2 in loading order) was calculated by first considering j1 and j2 as blocks of the same unit and then by considering one unit with capacity C_j , $C_j = C_{j1} + C_{j2}$. In both cases the calculated energy generation of unit h was the same. This result agrees with what was expected, since the amount of energy generated by unit h (and hence system reliability) are independent of whether unit j is loaded in one or two steps.

An additional application of deconvolution is discussed in Appendix C.

4.4 A New Technique of Approximate Probabilistic Simulation:

Group Representation of Generating Units

Certain types of studies, such as the expansion planning of a generating system or the evaluation of different levels of availability improvements or load management on system economics, frequently require the repetitive application of probabilistic simulation. In such studies, a large number of alternative scenarios must be evaluated for generating cost and reliability comparisons. Such evaluations require the computation of a large number of ELDC. For this reason, a large fraction of the computing cost associated with such studies is due to the repetitive application of the probabilistic simulation method. It is, therefore, desirable to develop techniques whereby this cost will be reduced.

In this section a new technique of probabilistic simulation devised by the author is presented [20]. With this technique energy generation, LOLP, and unserved energy are calculated at a reduced computational time and cost. This technique consists of aggregating individual generating units into groups of units and then applying the method of probabilistic simulation to groups of units. Thus, instead of calculating an ELDC for each unit, only one such is calculated for each group. As a result, a substantial reduction in computational time is observed.

4.4.1 Algorithm of Group Representation

Consider a system of N units the loading order of which is

$$C_1, C_2, \dots, C_N$$

where C_i is the capacity of unit i . The availability probability of unit i is p_i . In the present grouping technique the N units are aggregated into groups with the loading order within each group and between groups maintained. ELDC are constructed only for groups of units and not for each unit. This is done by an appropriate definition of group capacity and group availability probability. Once such group parameters are defined, a group is treated as an "equivalent" unit in the standard probabilistic simulation. A group may contain any number of units.

The system load duration curve is denoted by $L(x)$, while the ELDC for group j by $ELG_{j-1}(x)$. The function $ELG_{j-1}(x)$ and the position of group j in loading order are shown in Figure 4.4. The capacities of the n units of group j are denoted by

$$C_1^j, C_2^j, \dots, C_n^j$$

The group capacity is defined as the sum of the capacities of the units in group j . Group availability probability is defined here as

$$p^j = \frac{\text{Energy generated by group } j \text{ in period } T}{\text{Energy required from group } j \text{ in period } T} \quad (4.25)$$

The calculation of P^j is described later in this section. Using the definition of Eq. (4.25), the ELDC for group $j+1$, $ELG_j(x)$, is calculated by

$$ELG_j(x) = P^j ELG_{j-1}(x) + Q^j ELG_{j-1}(x - GRC_j) \quad (4.26)$$

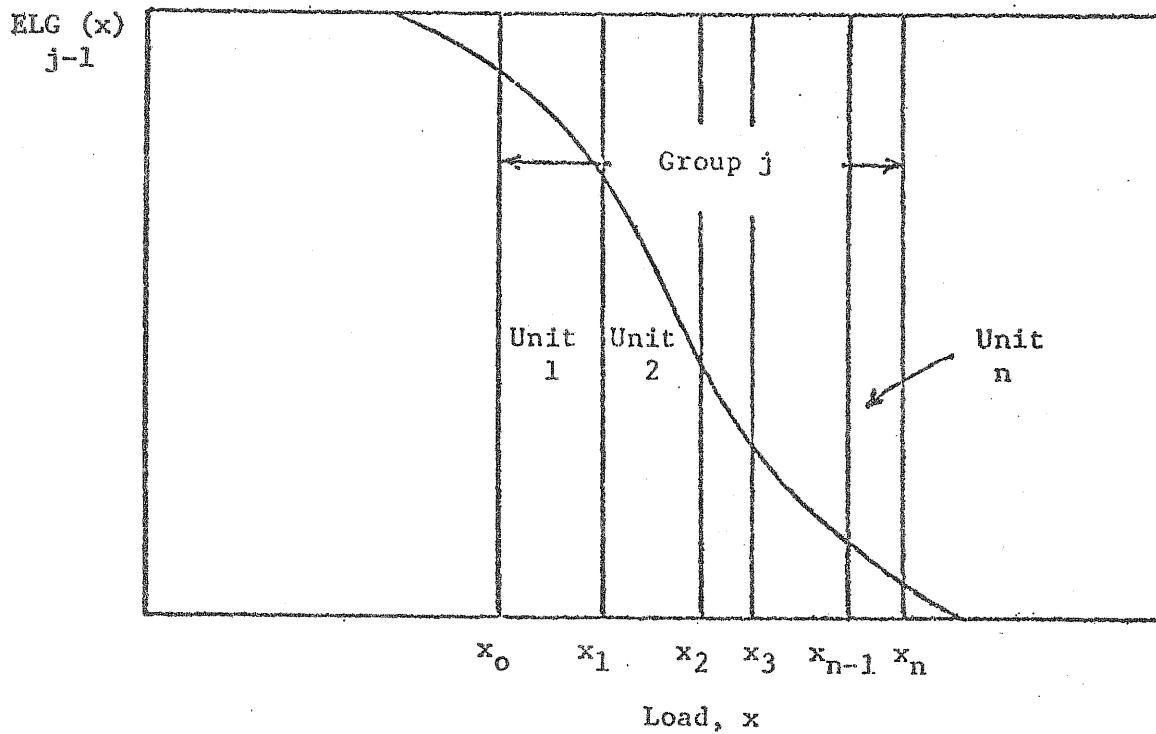


Figure 4.4 The Equivalent Load Duration Curve
for Group j

where

$$Q^j = 1 - P^j ,$$

$$GRC_j = \sum_{i=1}^{i=n} C_i^j ,$$

and

$$ELG_0(x) = L(x)$$

The group availability probability, P^j , is calculated concurrently with the energy of the units in group j as follows. Group j contains n units. Initially, the first two units of the group are considered. The capacities of these units are C_1^j and C_2^j , and their availability probabilities are p_1^j and p_2^j respectively. The expected energy generation of these units is

$$E_1^j = p_1^j T \int_{x_0}^{x_1} ELG_{j-1}(x) dx \quad (4.27)$$

and

$$E_2^j = p_1^j p_2^j T \int_{x_1}^{x_2} ELG_{j-1}(x) dx + p_1^j p_2^j T \int_{x_0}^{x_0+C_2^j} ELG_{j-1}(x) dx \quad (4.28)$$

respectively. In Eq. (4.27) and (4.28), $ELG_{j-1}(x)$ is the ELDC for group j . The limits of the integrals in Eq. (4.27) and (4.28) are shown in Figure 4.4. Next, unit 1 and unit 2 are combined and represented by an equivalent unit having capacity $C_1^j + C_2^j$ and equivalent availability P_{12}^j given by

$$P_{12}^j = \frac{(E_1^j + E_2^j)}{\int_{x_0}^{x_2} \text{ELG}_{j-1}(x) dx} \quad (4.29)$$

The energy generated by the third unit is calculated by the same procedure as for E_2^j in Eq. (4.28):

$$E_3^j = P_{12}^j P_3^j T \int_{x_2}^{x_3} \text{ELG}_{j-1}(x) dx + Q_{12}^j P_3^j T \int_{x_0}^{x_0 + C_3^j} \text{ELG}_{j-1}(x) dx \quad (4.30)$$

Next, units 1, 2 and 3 are combined and represented by an equivalent unit of capacity $C_1^j + C_3^j$ and equivalent availability P_{123}^j given by

$$P_{123}^j = \frac{(E_1^j + E_2^j + E_3^j)}{\int_{x_0}^{x_3} \text{ELG}_{j-1}(x) dx} \quad (4.31)$$

This procedure is repeated until the last unit in the group is included. Then the group availability probability, P^j , is set equal to $P_{12\dots n}^j$. The LOLP and unserved energy are calculated as in the standard technique using $\text{ELG}_N(x)$.

As seen from Eq. (4.27) through (4.31), the calculation of each $P_{12\dots j}^j$, $2 \leq k \leq n$, requires the evaluation of two integrals but does not require the calculation of ELDC for individual units. Therefore, this procedure reduces computing time. However, a disadvantage is that the approximation which is used for the calculation of E_3^j , as well as for E_4^j , etc., introduces an error which propagates and affects the accuracy of all the remaining computations. As the number of units in each group increases, the

computing time savings increases while the error also increases. This error is, however, smaller if the capacity of units in a group is small. This is particularly important in dealing with peaking units because their capacities are very small and their contribution to the system's energy generation is very small while the computing time needed for the computation of their ELDC is the same as for larger units.

4.4.2 Numerical Evaluation

In order to test the validity of the proposed technique and its effectiveness in reducing computing time, the technique was implemented into a generating system simulation program and applied to a test system. A listing of this program is provided in Appendix D. A piece-wise linear interpolation method is used in the program to represent ELDC. The reduction in computing time and error relative to the standard technique are evaluated for different ways of grouping of the generating units. The capacity of each unit owned by the utility and the availability probability of each unit are listed in loading order in Table 4.1. The inverted load duration curve of the system in the period of simulation is shown in Figure 4.5. The cases of grouping to which the technique was applied are shown in Table 4.2. Case 1 is the reference case where no grouping is used. In Cases 2 through 5, the last 11 units, namely unit 19 through 29, are combined into 4, 3, 2 and 1 groups, respectively. The boundary between two adjacent groups is shown by a dotted horizontal bar in Table 4.2. In Cases 6 through 9, the last 20 units, namely units 10 through 29, are combined into 9, 7, 5 and 4 groups, respectively.

TABLE 4.1
SYSTEM PLANT PARAMETERS

Unit Number	Unit Capacity, MW	Availability Probability
1	218.50	0.67
2	180.00	0.89
3	202.30	0.83
4	204.75	0.79
5	204.75	0.78
6	204.75	0.80
7	132.00	0.86
8	140.00	0.84
9	140.00	0.84
10	67.00	0.95
11	61.00	0.95
12	60.00	0.93
13	67.00	0.92
14	67.00	0.92
15	67.00	0.95
16	14.00	0.74
17	11.00	0.84
18	149.00	0.84
19	14.00	0.79
20	3.85	0.90
21	28.00	0.93
22	21.00	0.89
23	17.00	0.93
24	17.00	0.95
25	17.00	0.93
26	17.00	0.93
27	21.00	0.87
28	21.00	0.91
29	8.00	1.00*

*purchase power contract

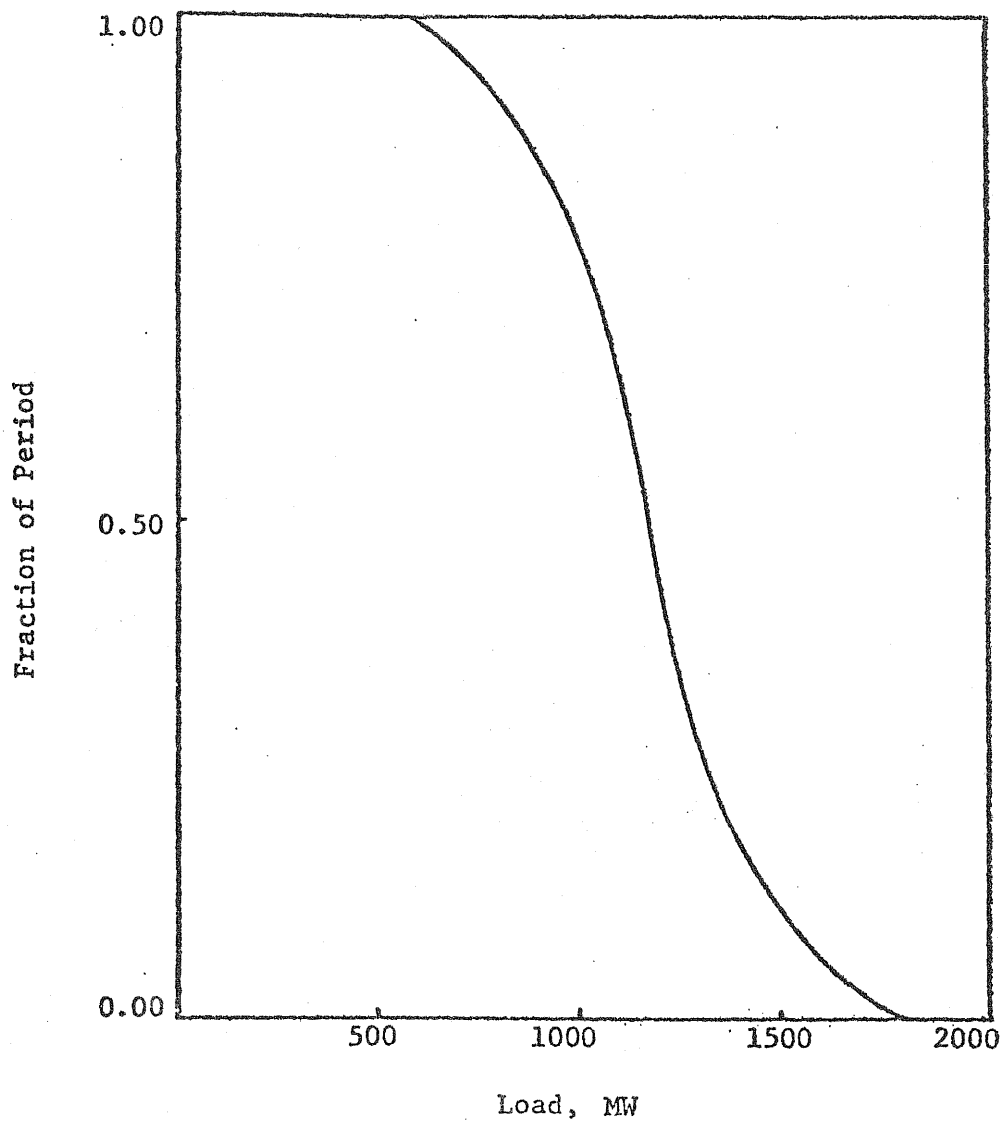


Figure 4.5 The Inverted Load Duration Curve
of the System Considered

TABLE 4.2
ARRANGEMENT OF UNITS ACCORDING TO NINE DIFFERENT
GROUPING SCHEMES
(Each Entry Represents the Capacity of a Group in MW)

	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6	Case 7	Case 8	Case 9
No. of Groups	29	22	21	20	19	18	16	14	13
218.50	218.50	218.50	218.50	218.50	218.50	218.50	218.50	218.50	218.50
180.00	180.00	180.00	180.00	180.00	180.00	180.00	180.00	180.00	180.00
202.30	202.30	202.30	202.30	202.30	202.30	202.30	202.30	202.30	202.30
204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75
204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75
204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75	204.75
132.00	132.00	132.00	132.00	132.00	132.00	132.00	132.00	132.00	132.00
140.00	140.00	140.00	140.00	140.00	140.00	140.00	140.00	140.00	140.00
140.00	140.00	140.00	140.00	140.00	140.00	<u>140.00</u>	<u>140.00</u>	<u>140.00</u>	<u>140.00</u>
67.00	67.00	67.00	67.00	67.00	67.00	<u>128.00</u>	<u>128.00</u>	188.00	255.00
61.00	61.00	61.00	61.00	61.00	61.00	<u>127.00</u>	<u>127.00</u>	-----	-----
60.00	60.00	60.00	60.00	60.00	60.00	-----	-----	-----	-----
67.00	67.00	67.00	67.00	67.00	67.00	134.00	134.00	201.00	-----
67.00	67.00	67.00	67.00	67.00	67.00	-----	-----	-----	308.00
14.00	14.00	14.00	14.00	14.00	14.00	-----	-----	-----	-----
11.00	11.00	11.00	11.00	11.00	11.00	25.00	25.00	174.00	-----
149.00	<u>149.00</u>	<u>149.00</u>	<u>149.00</u>	<u>149.00</u>	<u>149.00</u>	<u>149.00</u>	<u>149.00</u>	-----	-----
14.00	-----	-----	-----	-----	-----	-----	-----	-----	-----
3.85	48.85	48.85	-----	-----	-----	48.85	-----	-----	-----
28.00	-----	-----	83.85	-----	-----	-----	83.85	83.85	83.85
21.00	-----	-----	-----	-----	-----	-----	-----	-----	-----
17.00	55.00	72.00	-----	187.85	55.00	-----	-----	-----	-----
17.00	-----	-----	-----	-----	-----	-----	-----	-----	-----
17.00	55.00	-----	-----	-----	55.00	-----	-----	-----	101.00
21.00	-----	-----	101.00	-----	-----	-----	101.00	101.00	-----
21.00	-----	67.00	-----	-----	-----	-----	-----	-----	-----
21.00	29.00	-----	-----	-----	-----	29.00	-----	-----	-----
8.00	-----	-----	-----	-----	-----	-----	-----	-----	-----

Entries in Table 4.2 show the capacity of each group in Cases 1 through 9.

The error relative to Case 1 in the calculated energy generation by each unit, is shown in Table 4.3. By observing Cases 2 through 5 in Table 4.3, the following tendencies may be recognized. First, the amount of error increases as the size of groups increases, i.e., the errors in Case 5 are larger than those in Cases 2 through 4. Second, the error increases in the loading order, although this rule does not strictly apply. Those two tendencies are observed also in Cases 6 through 9. By comparing Cases 2 and 6, where the grouping schemes for units 19 through 29 are identical, it can be seen that grouping units in an early loading order increases the errors for the units in a later loading order. Similar comparisons may be made between Cases 4 and 7, or Cases 4 and 8 or Cases 4 and 9.

The last row of Table 4.3 shows the percent error in the total energy generation calculated for each case. This error is less than or equal to 0.01% for all the grouping schemes tested. This high accuracy in the total energy generation is due to the fact that only relatively small units, whose contribution to the total energy generation is small because of their small capacities as well as their low loading priorities, are grouped.

Figure 4.6 shows the error in LOLP as well as the computing time for each case relative to the reference case. The CPU time for Case 2 is approximately 70% of Case 1, (or 30% saving) while that for Case 9 is 34% (or 66% saving). The error in LOLP for Cases 2 through 5 is less than 1%, while the error for Cases 6 through

Entries in Table 4.2 show the capacity of each group in Cases 1 through 9.

The error relative to Case 1 in the calculated energy generation by each unit, is shown in Table 4.3. By observing Cases 2 through 5 in Table 4.3, the following tendencies may be recognized. First, the amount of error increases as the size of groups increases, i.e., the errors in Case 5 are larger than those in Cases 2 through 4. Second, the error increases in the loading order, although this rule does not strictly apply. Those two tendencies are observed also in Cases 6 through 9. By comparing Cases 2 and 6, where the grouping schemes for units 19 through 29 are identical, it can be seen that grouping units in an early loading order increases the errors for the units in a later loading order. Similar comparisons may be made between Cases 4 and 7, or Cases 4 and 8 or Cases 4 and 9.

The last row of Table 4.3 shows the percent error in the total energy generation calculated for each case. This error is less than or equal to 0.01% for all the grouping schemes tested. This high accuracy in the total energy generation is due to the fact that only relatively small units, whose contribution to the total energy generation is small because of their small capacities as well as their low loading priorities, are grouped.

Figure 4.6 shows the error in LOLP as well as the computing time for each case relative to the reference case. The CPU time for Case 2 is approximately 70% of Case 1, (or 30% saving) while that for Case 9 is 34% (or 66% saving). The error in LOLP for Cases 2 through 5 is less than 1%, while the error for Cases 6 through

TABLE 4.3

PERCENT ERROR IN THE CALCULATION OF ENERGY GENERATION

(Blank entries indicate no grouping. Boxes indicate groups of units).

Case Number	1	2	3	4	5	6	7	8	9
Number of Groups	29	22	21	20	19	18	16	14	13
Unit Number									
10						0.0	0.0	0.0	0.0
11						0.0	0.0	0.0	0.0
12						-0.1	-0.1	-0.1	-0.1
13						-0.1	-0.1	-0.3	-0.3
14						-0.5	-0.5	-0.5	-1.2
15						-0.1	-0.1	-0.4	-0.7
16						0.0	0.0	-0.4	-0.3
17						0.0	0.0	-0.4	-0.4
18						0.0	0.0	-0.1	0.0
19		0.0	0.0	0.0	0.0	0.6	0.6	0.2	-1.9
20		0.0	0.0	0.0	0.0	0.7	0.7	0.3	-1.7
21		0.0	0.0	0.0	0.0	0.8	0.8	0.7	-1.2
22		-0.1	-0.1	-0.1	-0.1	0.8	0.8	1.2	-0.3
23		-0.1	-0.1	-0.1	-0.1	0.8	0.6	1.2	0.1
24		-0.1	-0.1	-0.3	-0.3	0.7	0.5	1.3	0.8
25		-0.1	-0.1	-0.3	-0.4	0.7	0.6	1.5	1.7
26		-0.1	-0.2	-0.2	-0.4	1.0	0.9	1.7	2.7
27		-0.1	-0.1	-0.1	-0.5	1.2	1.2	2.1	3.7
28		-0.1	-0.1	-0.2	-0.7	1.5	1.4	2.6	4.8
29		-0.1	-0.2	-0.3	-0.9	1.7	1.6	3.1	5.6
Error in Total									
Energy, %		< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	0.01

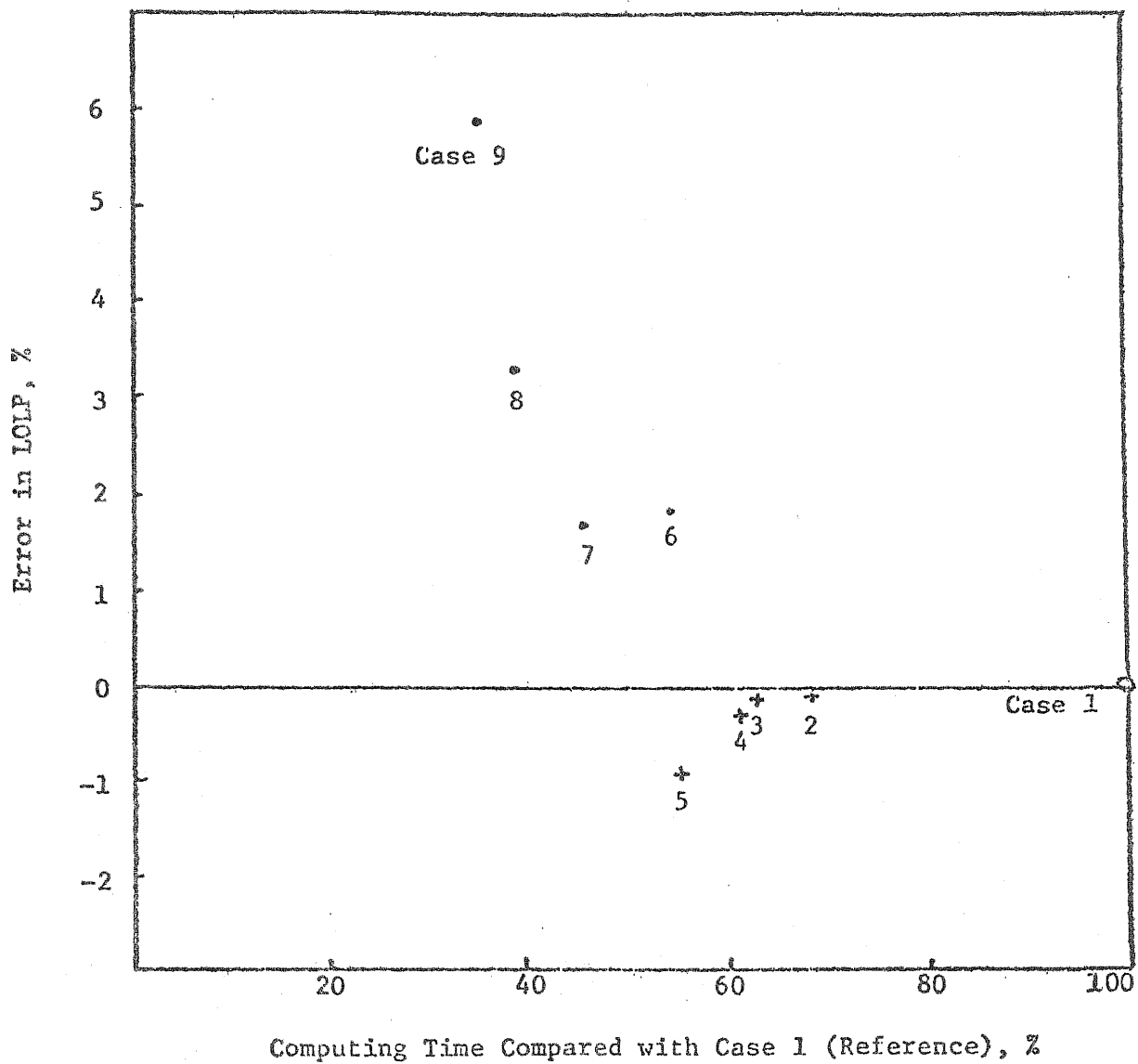


Figure 4.6 Computing Time and Error in LOLP

9 is spread between 1% and 6%. The error in LOLP less than 10% is considered to be small in system planning because a projected LOLP for any given system is subject to much greater error due to uncertainty in load forecasting and outage rates.

4.4.3 Conclusion

An algorithm to combine generating units into large equivalent units was derived in conjunction with probabilistic simulation of generating system operation. Test results show that the number of ELDC to be calculated in a probabilistic simulation can be easily reduced with a computing time saving of 30% to 70% without introducing a significant amount of error. The proposed method is most successfully used to increase the computing efficiency in dealing with small peaking units whose contribution to the system is minimal but for which it takes the same computational cost to form individual ELDC as it does for larger units.

The computational costs are compared based on the probabilistic simulation using the piece-wise polynomial representation of ELDC's. If another type of expansion of ELDC's is used, the amount of computing cost saving by the grouping scheme will be different. Nevertheless, the effectiveness of the grouping method is not affected by the type of the mathematical representation of ELDC's in the computer program.

4.5 Implementation of the Method of Probabilistic Simulation for Fuel Costing and Reliability Calculations

The methodologies described in Sections 4.2, 4.3 and 4.4 have been implemented into computer programs for the calculation of

fuel costs and system reliability. The methods of Section 4.2 and 4.3 are incorporated into the MARC Code. The grouping technique has been incorporated into a different program, similar to MARC. Both of these programs require similar data. For this section such data requirements and certain auxiliary techniques for the implementation of probabilistic simulation are discussed.

Implementation of probabilistic simulation techniques requires knowledge of expected system loads, loading order of units, and availability probabilities. The estimation of expected loads is a forecasting problem and will not be addressed in this work. The discussion in this section will focus on

- (1) A technique for the determination of the loading order of units, and
- (2) A technique for the determination of unit availability probability.

The author has contributed to the development of the second technique.

4.5.1 Determination of the Loading Order of Units

The method of probabilistic simulation requires as its input the specification of the loading order of units. This order is assumed to be fixed in each interval (period) of study. When the loading order is not provided by the input, an auxiliary technique is used to generate the loading order. This auxiliary technique simulates unit commitment based on the criterion of maintaining sufficient spinning reserve to overcome the (single) contingency of the largest committed unit. Such unit may be divided into up to two blocks (segments). Base units are committed first, cycling units next, and peaking units last. Within each of these three

groups (Base, Cycling, Peaking), dispatching is performed based on the order of increasing fuel cost [27].

4.5.2 Determination of Unit Availability Probability

The method of probabilistic simulation requires as its input the probability that a unit will be available to operate when needed (availability probability). A unit may be partially or fully unavailable either due to failure of one of its components or because of scheduled (or planned) maintenance.

A measure of unavailability due to failure is the Equivalent Forced Outage Rate, EFOR, defined in Reference [24] as:

$$EFOR = \frac{FOH + EFOH}{FOH + EFOH + SH} \times 100 \quad (4.32)$$

where FOH = forced outage hours

$$EFOH = \frac{\sum \text{forced partial outage hours} \times \text{size of reduction}}{\text{maximum dependable capacity}}$$

SH = the total number of hours the unit was actually operated with breakers closed to the station bus.

By defining the probability of failure, q , to be identical with $\frac{EFOR}{100}$, the probability that a unit will not be unavailable due to failure when called upon, P_f , is

$$P_f = 1 - q \quad (4.33)$$

It is assumed here that a unit can be either fully available or fully unavailable. For the context of probabilistic simulation, forced outages are regarded as randomly distributed. Thus, q is regarded as a constant throughout each period of study.

A unit which is on maintenance must not be included in the capacity of the system during the period of maintenance. However, because it is impractical to coordinate the periods of simulation with the periods of maintenance, an alternative technique is used. Maintenance time is assumed to be uniformly distributed throughout each period of simulation. (In this work the typical duration of a period is on the order of three months.) Thus, if a unit has m days of maintenance in a period of K days, the "maintenance outage probability" of this unit in the particular period is defined to be equal to $\frac{m}{K}$. The probability that this unit will not be on maintenance in the same period, P_m , is defined as

$$P_m = 1 - \frac{m}{K} \quad (4.34)$$

Using Equations (4.33) and (4.34), availability probability is calculated in this study by

$$P = (1-q) \left(1 - \frac{m}{K}\right) \quad (4.35)$$

When the maintenance schedule is not known, it is simulated in this study as follows: The total maintenance space required in the year, MS , is defined as

$$MS = \sum_{i=1}^N C_i D_i \quad (4.36)$$

where

MS = the total maintenance space required, MWh

C_i = the capacity of unit i , MW

D_i = the number of hours required for maintenance
of unit i in the year,

N = the total number of units in the system.

The quantity MS is allocated to each period of the year based on the criterion of equalizing reserves between periods. The maintenance space allocated to each period is further allocated to each type of (base, cycling, peaking) unit so that the fraction of the maintenance space allocated to each type of unit in each period is equal to the fraction of maintenance space of the period to the total maintenance space in the year. The maintenance space allocated to each type of unit in each period is further allocated to each unit in the order of unit capacity [27].

4.6 Summary

In this chapter techniques of probabilistic simulation of generating system operation were developed. Probabilistic simulation is used by the MARC computer program to calculate energy generation and system reliability in the evaluations of Chapter 5. In the MARC program the load duration curve is represented by a piece-wise linear function and generating units are represented by two blocks.

Algorithms of probabilistic simulation which were developed in this chapter include:

1. one-block representation of generating units,
2. multiple-block representation of generating units,
3. two-state model of availability probability,
4. three-state model of availability probability.

A new technique of probabilistic simulation suitable for repetitions application of probabilistic simulation was developed. This technique is approximate but it was shown to reduce computing time by up to 66% with error in the LOLP spread between 0 and 6% and insignificant error in the calculation of energy generation.

Implementation of probabilistic simulation in the MARC code was discussed with emphasis on the algorithms for the determination of plant loading order and availability probability.

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APPENDIX B

Description of Data Elements
in the Unit Data Files

FOSSIL AND NUCLEAR UNIT
DATA ELEMENT DESCRIPTIONS
ANNUAL INFORMATION

DATA
ELEMENT
NOTATION

DATA DESCRIPTIONS

CN	A single digit company number 1 = Appalachian Power Company, 2 = Delmarva Power and Light Company, 3 = Potomac Edison Company, 4 = Potomac Electric Power Company, 5 = Virginia Electric Power Company
VSCC NUMBER	The six digit unit identification number which uniquely identifies the unit relative to all units of companies serving Virginia is listed. This number will be assigned.
UNIT NAME	The unique name of the unit up to 20 characters is given left justified in the field.
FRAC OWNED	The fraction of the unit owned or leased by the reporting company is given. This number is calculated based on the maximum dependable capacity of the unit such that the maximum capacity available to the reporting company is the fraction of unit ownership times the maximum capacity of the unit. Field length is four characters including the decimal point.
UT	The type of unit is given. Enter one of the following numbers: 1 steam-fossil 2 steam-nuclear 3 diesel 4 gas turbine 5 jet engine
LT	The unit loading type is given. Enter one of the following numbers: 1 Base 2 Intermediate (Cycling) 3 Peaking
FUELS	
P	The primary fuel used by the unit for generation is reported. Enter one of the following numbers:

- 1 coal
- 2 nuclear
- 3 light oil (No. 2)
- 4 heavy oil (No. 4 and 6)
- 5 natural gas
- 6 gasoline/jet fuel
- 9 other

A

The alternate or secondary fuel used for generation is listed. Enter one of the following numbers:

- 1 coal
- 2 nuclear
- 3 light oil (No. 2)
- 4 heavy oil (No. 4 and 6)
- 5 natural gas
- 6 gasoline/jet fuel
- 9 other
- 0 no alternate fuel used

I

The fuel used for ignition is listed. Enter the appropriate number from the above list.

ON-LINE
MO

The month that the unit went into commercial service is given. Enter 01-12

YR

The year that the unit went into commercial service is given. Enter four digits of the year.

OFF-LINE
MO

The month that the unit is expected to be retired from commercial service is listed. If not known, enter 12.

YR

The year that the unit is expected to be retired from commercial service is given. If not known, enter 1999.

ANNUAL
EQUIV
AVAIL

The annual unit equivalent availability factor is given for the reporting year. The equivalent availability (EEI definitions) is defined using,

$$EA = \frac{AH - (EFOH + ESOH)}{PH}$$

where AH is equal to service hours plus reserve shutdown hours, EFOH is the equivalent forced outage hours

$$EFOH = \frac{\sum TFO_i * SFO_i}{V_i \cdot MDC}$$

where TFO_i is the length in hours of the i^{th} capacity derating, SFO_i is the size in MW of the i^{th} capacity derating where the product of TFO_i and SFO_i summed over all such partial forced outages, and MDC is the unit's maximum dependable capacity in MW; ESOH is the equivalent scheduled outage hours

$$ESOH = \frac{\sum_j (TOS_j * SSO_j)}{MDC}$$

where TSO_j is the length of the j^{th} derating due to planned or scheduled outage in hours; SSO_j is the size of the corresponding derating in MW. PH is the number of hours in the period. Field length is four characters including decimal point.

CAPACITY
COST

The capacity cost of the unit expressed in dollars per KW is given. This number is calculated by dividing the cost of the unit (land and land rights plus structure and improvements plus equipment costs) by the nameplate rating of the unit expressed in KW. In the case of nuclear plants this cost does not include the cost of the initial fuel loading. Field length is four characters (right justified in its field).

CAPACITY
WIN

The maximum dependable capacity in MW which the unit can produce over a four hour or longer period of time under minimum ambient restrictions. Field length is four characters (right justified in its field).

SUM

The maximum dependable capacity in MW modified for ambient limitations for a specified period of the year. Field length is four characters (right justified in its field).

FOSSIL AND NUCLEAR UNIT
DATA ELEMENT DESCRIPTIONS
MONTHLY INFORMATION

DATA
ELEMENT
NOTATION

DATA DESCRIPTIONS

MO

The two digits of the reporting month are given.

YR

The last two digits of the reporting year are given.

VSCC
NUMBER

The unit identification number is given.

CAPACITY AND HEAT
RATE BY LOADING
BLOCK

The heat rate curve of each unit is represented at three points MW1, MW2 and MW3 (in MW), as HTRT1, HTRT2 and HTRT3, (in Btu/kwh), respectively. MW1 represents the minimum (flame-out) load, MW3 the maximum dependable capacity, and MW2 an intermediate point. The field length for each of MW1 and MW2 is three characters, for MW3 is four characters (right justified each value), and for each of HTRT1, HTRT2 and HTRT3 is five characters. When a unit's heat rate curve is not available set MW1 = 1/2 MW3 and MW2 = 3/4 MW3, and set HTRT1, HTRT2 and HTRT3 equal to the heat rate at maximum dependable capacity.

MONTHLY
EQUIV
AVAIL

The equivalent availability for the unit for the reporting month. This value is calculated using the same technique as the annual equivalent availability and outage data for the reporting month. Field length is four characters including decimal point.

FUEL COST

The weighted average fuel cost burned in the unit during the reporting month in $\text{\$/10}^6$ Btu is reported for the

PRIMARY

primary fuel and the

SECONDARY

alternate fuel

to the nearest hundredth of a cent. For each of the numbers field length is six characters.

FRAC
GEN
BY PRI

The fraction of energy generation by the unit attributed to the primary fuel. Field length is four characters including decimal point.

DISPATCHING
ORDER BY
LOADING BLOCK

Each unit is loaded in three steps (loading blocks) of capacity MW1, MW2 - MW1, and MW3 MW2. The values BK1, BK2 and BK3 represent the relative loading order of each block in the system dispatching for the reporting month. Field length for each of BK1, BK2 and BK3 is three characters and is right justified in the field. Representation of loading in less than three steps can be made by numbering the adjacent blocks consecutively.

HYDRO UNIT
DATA ELEMENT DESCRIPTIONS
ANNUAL INFORMATION

DATA
ELEMENT
NOTATION

DATA DESCRIPTIONS

CN	A single digit company number 1 = Appalachian Power Company, 2 = Delmarva Power and Light Company, 3 = Potomac Edison Company, 4 = Potomac Electric Power Company, 5 = Virginia Electric Power Company
VSCC NUMBER	The six digit unit identification number which uniquely identifies the unit relative to all units of companies serving Virginia is listed. This number will be assigned.
UNIT NAME	The unique name of the unit up to 20 characters is given.
FRAC OWNED	The fraction of the unit owned or leased by the reporting company is given. This number is calculated based on the maximum dependable capacity of the unit such that the maximum capacity available to the reporting company is the fraction of unit ownership times the maximum capacity of the unit. Field length is four characters.
UT	The type of unit is given. Enter "6"
LT	The unit loading type is given. Enter "4"
HT	The type of hydro unit is given. Enter one of the following numbers: 1 run-of-river 2 pumped storage 3 river reservoir
P	The primary fuel used by the unit for generation is reported. Enter "7"
ON-LINE MO	The month that the unit went into commercial service is given. Enter 01-12.

YR	The year that the unit went into commercial service is given. Enter four digits of the year.
OFF-LINE MO	The month that the unit is expected to be retired from commercial service is listed. If not known, enter 12.
YR	The year that the unit is expected to be retired from commercial service is given. If not known, enter 1999.
CAPACITY COST	The capacity cost of the unit expressed in dollars per KW is given. This number is calculated by dividing the cost of the unit (land and land rights plus structure and improvements plus equipment costs) by the nameplate rating of the unit expressed in KW. Field length is four characters.
CAPACITY MAX	The maximum dependable capacity in MW which the unit can produce subject to the most favorable flow conditions. Field length is four characters.
MIN	The minimum dependable capacity in MW. Field length is four characters.

HYDRRO UNIT
DATA ELEMENT DESCRIPTIONS
MONTHLY INFORMATION

DATA
ELEMENT
NOTATION

DATA DESCRIPTIONS

MO	The two digits of the reporting month are given.
YR	The last two digits of the reporting year are given.
VSCC NUMBER	The unit identification number is given. Field length is six characters.
CAPACITY LOADING BLOCKS	MW1, MW2 and MW3 represent loading points of the unit and BK1, BK2 and BK3 the order of loading of blocks in the system dispatching table (see discussion in data description for Fossil and Nuclear units). Field length for each of MW1, MW2 and MW3 is four characters (right justified in the field).
DISPATCHING ORDER BY LOADING BLOCK	Each unit is loaded in three steps (loading blocks) of capacity MW1, MW2 - MW1, and MW3 MW2. The values BK1, BK2 and BK3 represent the relative loading order of each block in the system dispatching for the reporting month. Field length for each of BK1, BK2 and BK3 is three characters and is right justified in the field. Representation of loading in less than three steps can be made by numbering the adjacent blocks consecutively.
GENERATION BY UNIT	The net generation of the unit is reported in MWh. Field length is seven characters (right justified in the field).
PUMPING ENERGY	If the unit is a pumped storage unit the amount of energy in MWh used for pumping water uphill is reported. Field length is seven characters (right justified in the field).

AVE PUMP
COSTS

For a pumped storage unit the average cost of the energy used for pumping the water uphill in \$/MWh to the nearest cent is reported. Field length is six characters including decimal point.

