

MODIFICATIONS TO THE  
WIEN AUTOMATIC SYSTEM PLANNING PACKAGE (WASP)  
FOR IMPROVING POWER POOLING ANALYSIS

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## FOREWORD

This report concerns the use of the Wien Automatic System Planning Package (WASP) model, modified to meet the needs of the Florida Public Service Commission for improving power pooling analysis. It is important to note that the Tennessee Valley Authority (TVA) has developed and has the proprietary rights to the WASP model. Any commission, agency or other potential user of this model or any modifications thereof must first secure the permission of the TVA for its use.

This report was prepared by Dr. Shoichiro Nakamura and Mr. Spyridon Tzemos of The National Regulatory Research Institute (NRRI) under Contract No. EC-77-C-01-8683 with the U.S. Department of Energy (DOE), Economic Regulatory Administration, Division of Regulatory Assistance. The opinions expressed herein are solely those of the authors and do not reflect the opinions nor the policies of either the NRRI or DOE.

The NRRI is making this report available to those concerned with state utility regulatory issues since the subject matter presented here is believed to be of timely interest to regulatory agencies and to others concerned with utilities regulation.

The NRRI appreciates the cooperation of the Florida Public Service Commission with the authors in preparing this study and for their permission to make this information available to others interested in regulatory affairs.

Douglas N. Jones  
Director

## EXECUTIVE SUMMARY

This report summarizes the activities that were undertaken by the National Regulatory Research Institute (NRRI) in fulfillment of the Florida Technical Assistance Project for Power Pooling Studies under Contract No. EC-77-C-01-8683 with the U.S. Department of Energy (DOE). The work consisted of four tasks that were jointly agreed to by the Florida Public Service Commission (FPSC), NRRI and were approved by DOE.

The Wien Automatic System Planning (WASP) computer model was developed at the Oak Ridge National Laboratory for use by the International Atomic Energy Agency. Although WASP was originally intended to be used for optimal electric system expansion planning in under-developed or developing countries, the program was also adopted for use by several public utilities and state agencies in the United States. This trend necessitated the modifications made in this project so that WASP could best fit the needs of the Florida Public Service Commission.

The modifications made to WASP have improved the original version in the following ways:

1. A large generating system can now be represented adequately; and as a result, WASP can be used in power pooling studies on a state or regional level.
2. The accuracy of reliability calculations was increased so that the very small loss of load probabilities (high reliabilities) of aggregated generation systems can be estimated more precisely.
3. The cost algorithm was modified to provide the option of simulating investor-owned utilities accounting practices. Therefore, WASP results were compatible to those of private utilities, and the program can be used for comparative checks.
4. The input data algorithms were modified so that outages of generating units could be more precisely represented. Also, system load description data can be retrieved from the public utilities' data in an easier and more accurate way.

The modified WASP code was extensively tested with satisfactory results. During the on-site testing, further modifications were made in order to adapt the program to FPSC's computer facilities in the optimum way. The program algorithms were analyzed in detail so that FPSC's staff could gain adequate insight into the program and learn to use it properly. This modified version of WASP was made operational on the FPSC computer system in May of 1979.



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## CHAPTER 1

### INTRODUCTION

#### Background

In April 1978, the Florida Public Service Commission (FPSC) responded to a solicitation by NRRRI described in the Regulatory Assistance Program brochure with a request for technical assistance in the general research area of power pooling. At that time, the FPSC had recently acquired the Wien Automatic System Planning (WASP) model and was concerned with its direct applicability to conditions in Florida. The original intent for selecting WASP was to fulfill the FPSC responsibility under the Power Plant Siting Act, the Grid Bill, and general rate case investigations. After examination of the model, staff members of the FPSC concluded that WASP needed modification and identified several elements of the internal program that would have to be redesigned if the model were to satisfy the needs of the Commission.

#### The Request for Technical Assistance

The FPSC turned to the National Regulatory Research Institute (NRRRI) for technical assistance and submitted a statement of needs and requirements in April 1978. Specifically, the FPSC statement requested the following modification to the WASP code:

1. Change the form of load data input from fifth order polynomial to point-wise data.
2. Add an option which produces a levelized annual fixed charge.

3. Increase the limit of total number of units to 200, or 240 if possible.
4. Add an option to allow the user to specify seasonal maintenance by input.
5. Incorporate the forced outage rate as a function of age of the plant.
6. Evaluate the possibility of increasing the accuracy in dealing with spinning reserve.
7. Evaluate the possibility of increasing the accuracy of LOLP (loss-of-load-probability).

The project was selected for support by the NRRRI with funds provided by the U.S. Department of Energy (DOE) in October of 1978. Dr. Shoichiro Nakamura, a professor of Nuclear Engineering at The Ohio State University and a recognized authority on WASP, was selected to provide the technical assistance to the FPSC. A meeting was held at the FPSC in November of 1978 with the purpose of producing a work plan that would satisfy the staff and the program objectives of NRRRI.

#### Development of the Work Plan

As a result of that meeting, a work plan was developed that was agreed to by the staff of the FPSC and the NRRRI project team. The objective of the technical assistance effort was to modify the WASP model and the codes in accordance with the seven project items listed in the Commission's request for assistance. Among the seven items requested by the FPSC, items (1), (2), (4), and (5) were relatively simple, while items (3), (6), and (7) required careful study before starting any alteration of WASP. Item (3) was considered logical from the programming



point of view but could increase the core storage requirement significantly. Therefore, item (3) needed prior evaluation of the increased requirement for core space and compatability with the FPSC computer. Item (7) needed evaluation as to whether it was possible to accomplish this modification with the existing version of WASP. Item (7) was viewed as possible by adopting the piecewise polynomial developed previously at The Ohio State University. However, its compatability with WASP had to be evaluated in terms of memory requirements and increased computational time.

The NRRRI project team then proceeded to implement the technical assistance through a program composed of four tasks.

Task One: Evaluation of Feasibility of Modifications

At the end of Task One, it was necessary to assess:

- a. what the expanded number of generating units to be included in the program must be;
- b. whether it is possible to modify the spinning reserve treatment;
- c. whether the piecewise linear approximation should be incorporated into the existing WASP program.

Task Two: WASP Modifications

The purpose of this task was to reprogram WASP on The Ohio State University computer. This effort includes debugging and a series of alterations to the card decks of WASP.

Task Three: On-site Technical Assistance

The modified WASP was tested extensively on The Ohio State University computer to make sure the code worked properly with all different types of user's input. After

completing tests of WASP on The Ohio State University computer, the program will then be tested on FPSC's computer to make certain all the programs are operational. If any problems are encountered during the test, WASP will be readjusted for the FPSC computer. Therefore, a representative from NRRI will be made available for on-site consultation and assistance.

Task Four: Documentation of the Program Modifications

The modifications made to the program are to be clearly written and submitted to the staff of the FPSC.

The work plan specified that the NRRI project team produce three reports to be submitted to the FPSC. The first report was to contain research findings on (a) the number of generating units to be included in the program; (b) whether it is possible to modify the spinning reserve treatment; and (c) whether the piecewise linear approximation should be incorporated into the existing WASP program.

This first report was submitted to the FPSC in February of 1979 and required their formal approval before further work was continued on the project. A copy of the first report can be found in Appendix A of this final report. A second brief verbal report was provided to the FPSC by telephone relating the progress of modification and testing underway at The Ohio State University. The work plan also called for a final report to document in detail the results of the technical assistance effort, the modifications made to the code, and the nature of the reprogramming required of the WASP model. This document satisfied the final report requirement of the work plan and is presented as evidence of that effort.

Those readers not familiar with the original documentation and operation of WASP will better understand this report if References 1 and 2 in the bibliography are consulted.



CHAPTER 2  
IMPLEMENTATION OF THE WORK PLAN

This chapter summarizes the work performed as described in the implementation of the first three tasks of the work plan. Each task description is presented followed by a description of the activities associated with the implementation of that task. Where the presentation of material such as computer programs or documentation is found to be inappropriate, that material is cited in an attached appendix.

Task One: Evaluation of Feasibility of Modifications

The contractor will evaluate the feasibility of performing the WASP modifications suggested by FPSC within the time and budget constraints of this project.

The Wien Automatic System Planning (WASP) code was designed to determine the optimal generation expansion plan for an electric utility generating system. FPSC acquired WASP to fulfill their responsibility as described under the Power Plant Siting Act, Grid Bill and general rate case investigations. In order to apply WASP to these legislative requirements more effectively, FPSC requested the following modifications to the code:

1. Change the form of the load data input from fifth order polynomial to point-wise data.
2. Add on option by which the depreciation of generating plants is accounted for by a fixed charge rate rather than by salvage values.

3. Increase the limit of total number of units to 200, or 240 if possible.
4. Add on option to allow the user to specify seasonal maintenance by input.
5. Incorporate the forced outage rate as a function of age of the plant.
6. Evaluate the possibility of increasing the accuracy of LOLP (Loss-of-Load Probability).
7. Evaluate the possibility of increasing the accuracy in dealing with spinning reserve.

The first six modifications were determined to be feasible and were implemented under Task Two. Research on the seventh modification indicated that a more accurate treatment of spinning reserve was possible only if the current two-block representation of each generating unit was changed to three-block representation. Such a change required substantial reprogramming and would cause significant increase in computational time. It was concluded that, although a more elaborate treatment of spinning reserve was possible, it could not be incorporated in WASP within the time and budget constraints of this project.

#### Task Two: WASP Modifications

1. Modifications to Load Input Data.

The load data were the input for the LOADSY module of WASP. The data handling algorithm of LOADSY was modified to accept point-wise representation of the Load Duration Curve (LDC). Up to 1000 points may

be assigned by the user for the LDC representation. Since the computing time of LOADSY was not affected significantly by the number of points of LDC, it was recommended that the maximum number of points, namely 1000, be used for the best accuracy.

A detailed technical description of the LOADSY algorithm is presented in Appendix B, while the input format changes are listed in Appendix C.

## 2. Fixed Charge Rate Option in Capital Cost Calculations.

The capital cost component of electric generation by an expansion schedule is calculated in the DYNPRO module. The optimization was performed for a finite study period. (Under the original WASP assumption the remaining value of the plants, after the study period, is taken into consideration by assigning a salvage value at the end of the study period to each expansion alternative.)

The DYNPRO algorithm was modified to make the salvage value calculation optional and provide a Fixed Charge Rate (FCR) option that accounted for generating unit depreciation in accordance with private utility accounting procedures. The FCR was the factor which, "when multiplied by the capital cost of a facility, produced a levelized annual fixed charge reflecting return on investment, depreciation, taxes, insurance, retirement dispersion, and investment."<sup>1</sup>

In the modified DYNPRO version, the total cost of an expansion configuration is based on the sum of:

- a) the present worth of the total operating cost for all generating units during the study period;
- b) the present worth of the fixed charges of all generating units that were added to the system during the study period.

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<sup>1</sup> Page 7 in Reference 3 in the bibliography.

The fixed charges for each added generating unit were calculated for the life of the unit. The fixed charge rate is a user specified parameter.

A more technical description of the DYNPRO modifications is included in Reference 3 in the bibliography. The necessary input data changes are described in Appendix C. Table 1 shows the results of sample WASP runs with and without the FCR option. The input data used were identical to those for the predetermined run of Case 26 <sup>2</sup> except for the FCR option.

Table 1  
Objective Function for Case 26 With and Without the FCR Option

YEAR	OBJECTIVE FUNCTION (Thousands of Dollars)			
	No FCR	12% FCR	15% FCR	18% FCR
1982	926,130	1,044,330	1,140,266	1,236,201
1986	2,406,457	2,781,345	3,052,569	3,323,793
1990	3,831,580	4,387,459	4,803,992	5,218,662
1994	5,296,328	6,067,640	6,664,992	7,262,343

### 3. Increase of the Maximum Number of Generating Units

The total number of units that can be handled by WASP was increased from 100 to 270. The sum of the total number of units specified in the fixed and variable systems (FIXSYS and VARSYS modules respectively) was limited by programming considerations to 270. Since no more than 20 expansion alternatives could be specified in the variable system, at least 250 units would always be described by the fixed system.

<sup>2</sup> WASP sample runs in Reference 2 in the bibliography.



The increase in core memory requirement for each module is listed in Table 2.

Table 2  
Core Memory Increase Due to Change in the Maximum  
Number of Units in WASP

WASP MODULE	Additional Memory Requirements	
	STORAGE LOCATIONS	IBB BYTES
LOADSY	-	-
FIXSYS	170	680
VARSYS	-	-
CONGEN	680	2,720
MERSIM	9,350	37,400
DYNPRO	3,060	12,240

4. & 5. User Specification of Seasonal Maintenance Schedule and Incorporation of Forced Outage Rates as a Function of Plant Age.

Although modifications 4 and 5 are mentioned separately in Task One, they are described here simultaneously because they both are accomplished by the same auxiliary program.

Availability probability of a generating unit is defined as the probability a unit will be available when it is called to generate power. Thus, both scheduled maintenance and changes of the unit's forced outage rate affect the unit's availability probability. Since the system's LOLP calculation is based on the availability probability of each unit, the LOLP changes when the availability probability is modified.

The availability probability was originally defined in CONGEN as

$$P = 1 - \text{FOR}/100 \quad (1)$$

where P: generating unit availability probability

FOR: generating unit forced outage rate.

Hence, the maintenance outage effect was not taken into consideration.

Auxiliary program MATURE was written to create an adjusting factor for each generating unit availability probability so that it incorporated both scheduled maintenance effects and forced outage rate maturity with unit age.

The maintenance schedule for each unit is specified by the number of days required for maintenance in each period (usually four periods per year with a maximum of 12) of every year studied. An adjusting factor to the availability probability P, defined by eq. (1), is calculated as:

$$\text{PAD} = \left(1 - \frac{\text{DAYS}}{365/\text{NPER}}\right) \cdot \text{PMATUR} \quad (2)$$

where PAD: availability probability adjusting factor for each unit, each period of the year, for every year studied.

DAYS: number of days of scheduled maintenance for each unit, each period of the year, for every year studied.

PMATUR: forced outage rate adjusting factor for each unit, each year.

NPER: number of periods per year.

The default value for the adjusting factor PAD is 1.0. MATURE stores PAD in the MATURE.MAINT binary file through logical unit 35.

The modified CONGEN module of WASP (PWCONGEN, described in the next section) reads the PAD adjusting factors from the MATURE.MAINT binary

file and applies them to each unit's availability probability. The adjusted availability probability is:

$$p' = p \cdot \text{PAD} \quad (3)$$

where  $p'$ : the adjusted availability probability for each unit, in each period, for every year studied.

$p$ : as defined in eq. (1).

PAD: as defined in eq. (2).

Use of  $p'$  for LOLP calculation is a user option. Forced outage rate maturity adjustments for expansion candidates cannot be used in optimization runs but only in predetermined runs. This is because the a priori knowledge of the year when an expansion candidate comes in service is required for the compilation of the MATURE input data. Only then, is it possible to know the unit's age at each year of the study and make the necessary forced outage rate maturity adjustments. The same is true for scheduled maintenance since maintenance scheduling is possible only when the system generation mix is known. Forced outage rate maturity adjustments for the existing units are always meaningful because their age is always known.

Description of MATURE input data is provided in Appendix C.

#### 6. Accuracy Increase in LOLP calculation

The accuracy of LOLP calculated by WASP was improved by switching the Fourier expansion of load curves originally used in the probabilistic simulation in CONGEN, to the piecewise polynomial expansion. The new version of CONGEN is henceforth called PWCONGEN (Piece-Wise CONfiguration GENERator). The effect of the maintenance outage was also incorporated into the LOLP calculation of PWCONGEN. The probabilistic simulation in

MERSIM was not changed but still used Fourier expansions for the following reasons: (1) the major objective of MERSIM was to calculate electric energy generated by each generating unit; (2) since MERSIM uses two-capacity block representations of generating units, the use of piecewise polynomial would substantially increase the total computing time; (3) having taken into consideration the maintenance outage effect in PWCONGEN, the LOLP calculated by PWCONGEN was theoretically equivalent to that by MERSIM; (4) the Fourier expansion provided sufficient accuracy to the energy calculations in MERSIM. The piecewise polynomial used in PWCONGEN did not increase the computing time considerably because energy generation was not calculated.

The accuracy of PWCONGEN was checked against a special case (a system consisting of identical units) where LOLP could be calculated analytically. The results of this comparison are shown in Table 3. The running time of PWCONGEN was compared with the original CONGEN. The results are listed in Table 4.

PWCONGEN also includes the option of adjusting the availability probability of the generating units; thus LOLP can be calculated with consideration for the effects of scheduled maintenance and forced outage rate maturity.

A detailed technical description of PWCONGEN is provided in Appendix B, while the input data description is given in Appendix C.

#### Task Three: On-Site Technical Assistance

The contractor will test the modified WASP on FPSC's computer in order to make certain all programs tested at The Ohio State University work at FPSC.

Table 3  
PWCONGEN Reliability Check

Number of Identical Plants	Number of Points for LDC Inversion	LOLP for Period 1					LOLP for Period 2				
		Exact %	CONGEN		PWCONGEN		Exact %	CONGEN		PWCONGEN	
			%	% Error	%	% Error		%	% Error	%	% Error
9	1,000	0.61514	0.6014	2.233	0.6151	$<10^{-4}$	1.95412	2.0895	6.928	1.9541	0.0005
9	500				0.6138	0.218				1.9510	1.159
13	1,000	0.11349	0.1203	6.000	0.1135	1.026	0.68860	0.6982	1.394	0.6883	0.042
13	500				0.1131	0.343				0.6856	0.435

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Table 4  
Running Time Comparison Between CONGEN and PWCONGEN\*

Number of FIXSYS Units	CONGEN CPU Seconds	PWCONGEN Run 1 CPU Seconds	PWCONGEN Run>1 CPU Seconds
7	1.68	15.50	12.00
110	2.68	68.93	14.78
220	4.04	131.60	14.98

\* VARSYS and LOADSY are identical in all cases.

The modified WASP package was transferred and tested by NRRI staff on FPSC's computer during the week of May 14-19, 1979. Several changes were necessary due to differences between the FORTRAN compilers of the OSU's AMDAHL and the FPSC's CDC computers.

The CDC's single precision representation of real numbers is equivalent to the double precision of AMDAHL. Therefore, all double precision variables were changed to single precision to avoid unnecessary core memory utilization. Accuracy tests on the CDC computer at the FPSC gave the results listed in Table 5.

Table 5  
Results of PWCONGEN Accuracy Tests on FPSC's CDC Computer

LOLP %	% ERROR
0.02	1.0
0.002	3.0
0.000008	6.0

Running procedures were demonstrated during the test at FPSC. All WASP modifications were carefully checked, and detailed instructions with regard to the modifications were given to the FPSC's staff. Additional details for the on-site testing of WASP are provided in Appendix E.

#### Task Four: Documentation of the Program Modifications

The contractor will prepare documentation of all modifications made to the code, alterations to input and output format, if any, and results of tests.

A detailed documentation of the WASP modifications is presented in Appendix B. The input data changes are described in the procedure manual contained in Appendix C, while the results of the test runs are listed in Appendix D. Appendix E contains the report for the on-site testing of modified WASP.





### CHAPTER 3

#### SUMMARY AND CONCLUSIONS

In power pooling studies, several public utilities are combined to form an aggregate electricity generating system. Such a system contains a large number (often greater than 100) of generating units. The original WASP model could accurately represent only up to 100 units. This constraint was relaxed and the modified WASP can handle up to 270 units, rendering it capable of representing large generating systems.

The loss-of-load-probability (LOLP) calculation by the original WASP was of questionable accuracy and abnormalities were experienced at small LOLP values. These defects were corrected in the modified WASP through the use of a piecewise linear approximation in the algorithm for LOLP calculation. Thus WASP can now be used to analyze power pools that exhibit high reliabilities where such an analysis with the original version would have been of questionable validity because of inaccuracies in the calculation of small LOLP values. Consideration of pollution control in dispatching and individual commitments of the public utilities may make the WASP generated maintenance schedule inapplicable in actual operating conditions. For this reason, the modified WASP provides an option for user specified maintenance schedules. Furthermore, the availability of the generating units can be more accurately represented by providing an option to make adjustments to unit availability because of maturity.

The user options for scheduled maintenance specification, unit availability adjustments for maturity, and fixed charge rate cost calculations in accordance with standard utility practices make the modified WASP compatible with expansion planning models that are currently in use. Therefore, public utility regulatory commissions can utilize WASP to verify the accuracy of the expansion planning models used by investor-owned utilities.

The extensive on-site testing of WASP provided FPSC staff with the necessary insight into the program so that the results can be correctly interpreted and utilized with confidence. A thorough understanding of the program algorithms is one of the major advantages of WASP when compared with other commercially available expansion models (such as the General Electric or the Westinghouse models) where the algorithms are proprietary. The FPSC is now in position to verify the validity of the results of expansion planning models submitted by public utility companies in support of their need for additional power plant construction.

Public utility regulatory commissions can use WASP to estimate the cash requirements for expansion of the electricity generating system. This information is necessary for power pooling financial analysis and in rate case investigations when corporate finance models (such as RAM-finance) are utilized to determine the cost of electricity.

Although the modifications made to WASP during this project have greatly increased its usefulness to public utility regulatory commissions, time and budget considerations limited the making of additional modifications. Several improvements were identified and endorsed by the FPSC staff and the NRRRI project team. Four major modifications were identified that could further enhance WASP.

1) The existing WASP literature is fragmented and outdated. The input data descriptions, although precise, provide no details on data compilation procedures and no information for their proper use or correct interpretation of the final results. Therefore, a substantial effort is required to update and combine the existing literature into a user oriented manual that would contain:

- a) Detailed algorithm description;
- b) Precise input data requirements;
- c) Data sources and proper usage of input data;
- d) Sample parametric sensitivity analysis so that the dependence of the output results on the various input parameters can be realized.

2) Research and further modifications are needed in the generating unit's depreciation algorithm in order to increase its accuracy and computational efficiency.

3) A financing feasibility constraint should be incorporated in WASP to assure that the projected optimum expansion plan is within the utility's financing capabilities. Such considerations would also increase computational efficiency by avoiding detailed simulation of expansion configurations that are not feasible.

4) Transmission limitations of utility interconnections should be incorporated in WASP so that power pools can be analyzed more realistically.

Confidence in the use of WASP by state utility regulatory commissions would be greatly enhanced by arranging for on-site technical assistance from experienced WASP users. The new capabilities of the modified WASP and the experience gained by the FPSC staff during the on-site testing

gave them the necessary confidence in the operation of the program so that it could be used in an upcoming rate case. NRRRI and FPSC staff agreed that similar on-site technical assistance or WASP workshops would be extremely valuable to other state utility regulatory commissions interested in the use of WASP as a regulatory analysis tool.

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APPENDIX A

First Report

of

Technical Assistance in Power Pooling

for

The Florida Public Service Commission

submitted by

S. Nakamura

## 1.0 Introduction

This report describes the research findings on the following three subjects as specified in the Approved Work Plan for The Florida Public Service Commission:

- a) the number of generating units to be included in the program;
- b) whether it is possible to modify the spinning reserve treatment; and,
- c) whether the piecewise linear approximation should be incorporated into the existing WASP program.

## 2.0 Findings and Conclusions

### 2.1 The Number of Generating Units to be Included in the Program

Examination of the WASP program has shown that the limit of total number of units can be easily increased to 240. Therefore, we will increase the limit to 240 as originally requested by FPSC.

### 2.2 The Spinning Reserve Treatment

A more elaborate treatment of spinning reserve requires a three-block representation of each generating unit as opposed to the current two-block representation. In order to change the current two-block representation to three-block representation, a substantial reprogramming is necessary. The computational efficiency from such a change will be significantly sacrificed. We conclude that, while a more elaborate treatment of spinning reserve in WASP is not impossible, it cannot be incorporated within the time and budget constraint of the present project.

However, we suggest that the FPSC can incorporate the effect of spinning reserve approximately through the loading order of base and peaking block of units.



### 2.3 Use of Piecewise Linear Approximation

Piecewise linear approximation provides much better accuracy for the probabilistic simulation that calculates loss-of-load probability and energy generation by each generating unit than the Fourier expansion that is currently used. FLSC has requested us to investigate the feasibility of replacing the Fourier expansion in WASP by the piecewise approximation.

Our computational study during December indicates that the piecewise linear approximation is several times more time consuming than the Fourier expansion if Fourier expansion in WASP is entirely replaced by the piecewise linear approximation. However, the accuracy of WASP can be increased significantly with little increase in computing time if piecewise polynomial approximation is adopted only in part of WASP. This is the case if only LOLPs for a large number of alternative configurations in one period are to be calculated. The former is the case in the subroutine MERSIM (Merge-Simulation subprogram) and the latter in the subroutine CONGEN (Configuration Generating subprogram). Based on this finding, we propose that the piecewise polynomial approximation be used in CONGEN while the Fourier expansion be retained in MERSIM. We also propose to incorporate the maintenance outage effect in the probabilistic simulation calculation in CONGEN.

Since no energy is calculated in CONGEN, the last equivalent load curves, all the alternative configuration in a period may be obtained only by convolution and deconvolution of a few units except the first alternative configuration. The computing time required for convolution or deconvolution is small compared with that

of an entire calculation. Therefore, the increase of computing time by adopting piecewise polynomial is minimal. CONGEN filters out those configurations that do not satisfy the LOLP test. If LOLP is calculated accurately in CONGEN, all the configurations passed to MERSIM have satisfied the LOLP test. Therefore, the user can rely on LOLP calculated in CONGEN rather than that calculated in MERSIM. In increasing the accuracy of LOLP calculation in CONGEN, incorporation of maintenance outage effect is essential.

### 3.0 Conclusion

The limit to the total number of units incorporated into WASP will be increased to 240.

No modification of WASP with regard to spinning reserve will be attempted in this study.

Piecewise polynomial approximation will be adopted in CONGEN in conjunction with maintenance schedule to increase the accuracy of the LOLP calculation.

## APPENDIX B

### B.1 LOADSY Technical Description of Program Modifications

Originally, the load data were supplied to the LOADSY module as a normalized Load Duration Curve (LDC) expressed by a fifth order polynomial. This representation of LDC was transformed into a point-wise linear representation by subroutine LOADS and stored in the TLD array which is defined as

$$TLD_j = \sum_{i=0}^5 C_i X_j^i \quad j = 1, NTH \quad (1)$$

$$\text{where } X_j = (j-1) \cdot \left(\frac{1}{NTH}\right) + \frac{1}{2} \quad (2)$$

$TLD_j$ : fraction of peak load at the  $j$ th point

$X_j$ : fraction of a period at  $j$ th point

$C_i$ :  $i$ th coefficient of fifth order polynomial ( $i = 0 - 5$ )

$NTH$ : number of points used for discretization

The original LOADSY algorithm used a fixed value of 720 for  $NTH$ .

In the modified LOADSY module, the input of LDC may be given directly in point-wise data ( $NTH \leq 1000$ ) for each period of the year. The input data for all periods are stored in the POL array. The load data of each period is transferred into the TLD array in subroutine LOADS.

The fifth order polynomial representation of LDC still remains an option in the modified LOADSY. Two additional modifications were made in LOADSY in order to facilitate the probabilistic simulation in PWCONGEN.

- a) The number of points used for the inversion of the LDC, called INVERT, can be specified by the user. INVERT must be less than or equal to 1,200.
- b) The inverted load duration curve (calculated in COEFF subroutine and

stored into the TLOD array) is transferred into binary disk file LOADDATA through logical unit 22.

### B.2 FIXSYS

The required increase of the number of units that can be handled by WASP led to the following changes in FISXYS:

1) Executable line 5:

DIMENSION MWC (101)

was changed to

DIMENSION MWC (271)

2) Executable line 70:

IF(NFP-100) 18,18,15

was changed to

IF(NFP-270) 18,18,15.

### B.3 VARSYS

No modifications were necessary in VARSYS.

### B.4 MATURE

A flow chart of the MATURE program is shown in Figure B.1.

### B.5 CONGEN

The following changes in dimensions were made:

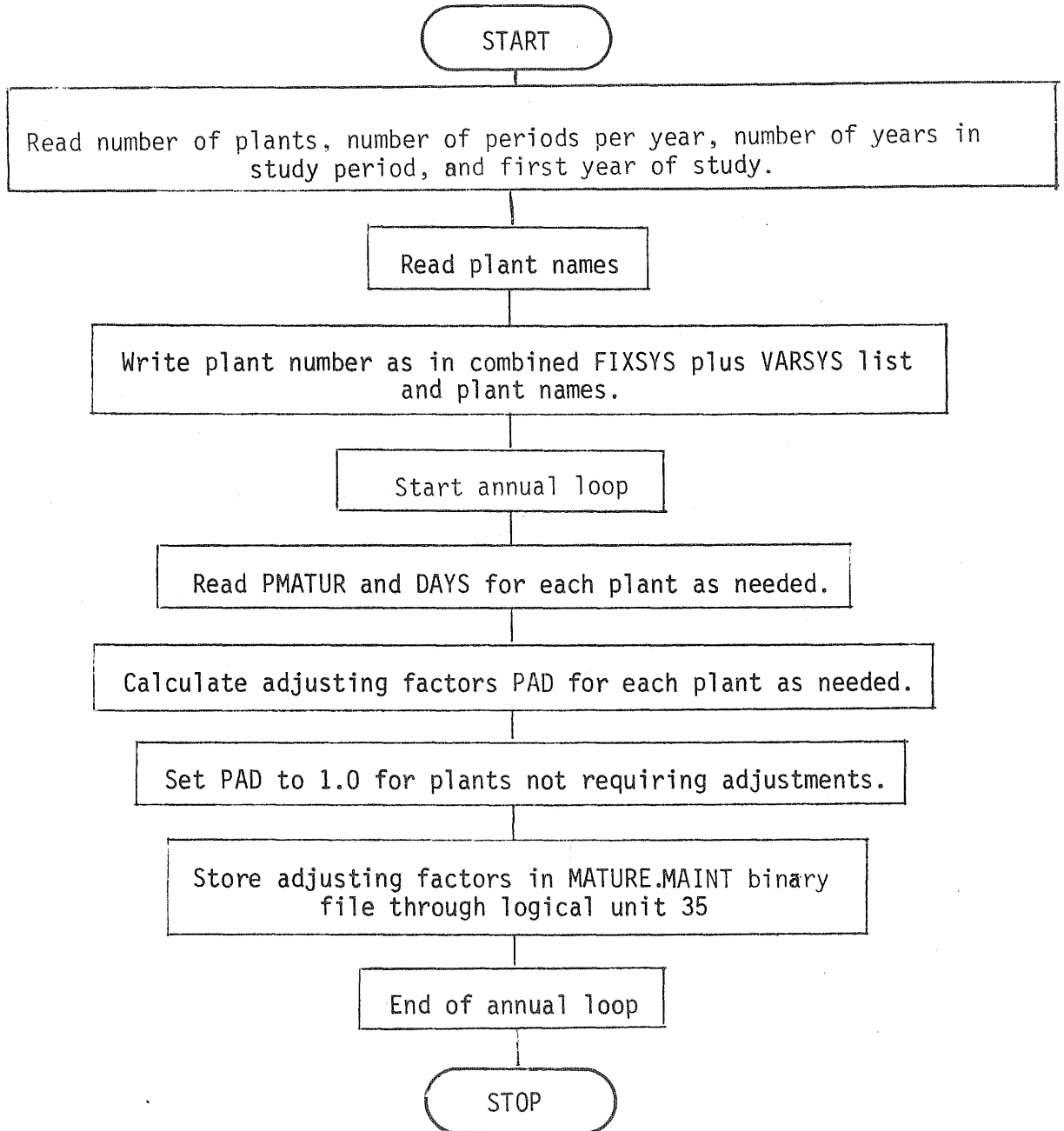
FOR (101) was changed to FOR (271)

NSETS (101) was changed to NSETS (271)

MWC (101) was changed to MWC (271)

NTYPE (101) was changed to NTYPE (271)

Figure B.1  
MATURE Flow Chart



## B.6 PWCONGEN

Probabilistic simulation successively generates Equivalent Load Duration Curves (ELDC) through convolutions. The  $j$ th ELDC is defined by the recurrence relation

$$\text{ELDC}_j(x) = p_j \cdot \text{ELDC}_{j-1}(x) + (1-p_j) \cdot \text{ELDC}_{j-1}(x-C_j) \quad (3)$$

where  $\text{ELDC}_j(x)$ : the  $j$ th equivalent load duration curve

$p_j$ : the  $j$ th unit availability probability

$C_j$ : the  $j$ th unit capacity

The ELDC for  $j=0$  is the original inverted load duration curve (also called load probability curve). After all  $N$  units in the system are convolved, LOLP is found as

$$\text{LOLP} = \text{ELDC}_N(X_C) \quad (4)$$

where LOLP: generating system's loss-of-load probability

$\text{ELDC}_N(X)$ : the  $N$ th equivalent load duration curve

$X_C$ : the system capacity

PWCONGEN uses eq.(3) to calculate each successive ELDC numerically using the piecewise linear representation of ELDC. This calculation is performed in subroutine PWADD.

Function PWFUN of PWCONGEN utilizes eq.(4) to find the system LOLP for each prospective expansion configuration.

A PWCONGEN run consists of two steps. In the first step the ELDC, convolving all the units of the fixed system, is generated and stored in the binary disk file FIXELDC through logical unit 32. In the second step, the fixed system ELDC is read from FIXELDC and the expansion candidate units are convolved. The LOLP for each expansion configuration is then calculated.

The two-step approach of PWCONGEN saves computing time because ELDC for the fixed system is calculated only once during the WASP optimization process. This is especially important when the fixed system involves a large number of units. The size of the array to store the ELDCs is limited to 3,000. If the normalized original inverted load duration curve is represented by the number of points "INVERT," then the maximum number of points for the final ELDC curve is

$$\text{MAXIMU} = \text{INVERT} \cdot \left(1 + \frac{X_c}{\text{Peak}}\right) \quad (5)$$

where MAXIMU: maximum number of points in ELDC representation

INVERT: number of points for the representation of the inverted load duration curve

$X_c$ : system capacity in MW

PEAK: system period peak in MW

If the maximum reserve margin specified in PWCONGEN is RES percent, the maximum system capacity allowed by the PWCONGEN reserve margin constraints is

$$X_{\text{max}} = \text{PEAK} \cdot \left(1 + \frac{\text{RES}}{100}\right) \quad (6)$$

Replacing  $X_c$  in eq.(5) with  $X_{\text{max}}$  from eq.(6) yields

$$\text{MAXIMU} = \text{INVERT} \cdot \left(2 + \frac{\text{RES}}{100}\right) \quad (7)$$

Both INVERT and RES are specified by the user and must be chosen so that the following constraints are satisfied:

$$\text{INVERT} \leq 1,200 \quad (8)$$

$$\text{MAXIMU} \leq 3,000$$

As INVERT is increased, the accuracy of the probabilistic simulation becomes higher but consumes more time. The effect of INVERT on LOLP accuracy and running time is shown in Table B.1.

The flow chart of subroutine PWLOLP is shown in Figure B.2.

#### B.7 MERSIM

Two kinds of modifications were made in MERSIM.

- a) The dimensions of the following arrays were changed:

##### Main Program

The dimensions of the arrays, MWB, MWC, ENERGY, NAME, NTYPE, MAINT, MAINCL, FOR, OMA, OMB, BHRT, FCST, FCSTF, CRMHRT, NSETS, LOCATN were changed from 101 to 271. The dimensions of arrays, AVLBTY, NOSETS, USBSF, UCBSL, UINCF, UINCL were changed from 100 to 270. Arrays, LORDER(200), NCONS(500), NORDER (500), PMAINT (100,12), INAME (202), ICLAS (202) were changed to LORDER (540), NCONS (1350), NORDER (1350), PMAINT (270,12), INAME (542), ICLAS (542).

##### Subroutine MAINTN

Arrays, MWC(101), NOSETS(100) were changed to MWC(271), NOSETS(270).

##### Subroutine ANSIM

Arrays, MWCS(100), MWBS(100) were changed to MWCS(270), MWBS(270).

##### Subroutine SIMUL

Arrays, ENGB(101), ENGP(101), EGEN(101), EPPK(101), NSETS(100), MWCS(100) were changed to ENGB(271), EPPK(271), NSETS(270), and MWCS(270).



Table B.1

Effect of INVERT on LOLP Accuracy and Computing Time

YEAR	INVERT	LOLP (%)		
		CONGEN	PWCONGEN	
1980	200		0.00035	
	500		0.00035	
	1,000	0.00789	0.00035	
1985	200		0.01619	
	500		0.01620	
	1,000	0.02133	0.01621	
1990	200		0.05153	
	500		0.05160	
	1,000	0.07559	0.05163	
1994	200		0.07512	
	500		0.07493	
	1,000	0.09894	0.07498	
Total CPU Time (Seconds)				
	200		Run 1	Run 2
	500		3.64	3.84
	1,000	1.68	8.05	7.01
			15.50	12.00

Figure B.2.  
Flow Chart for Subroutine PWLOLP

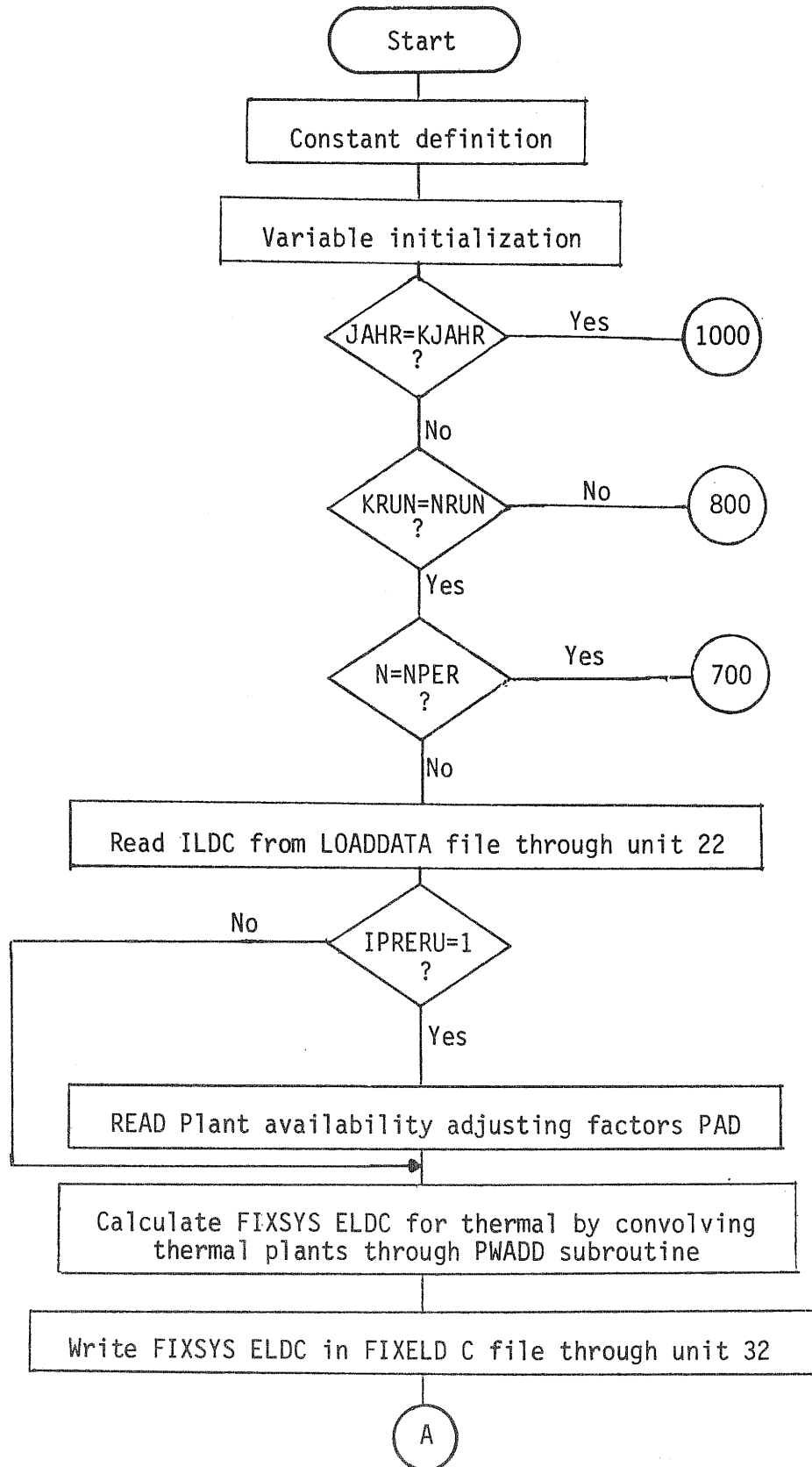


Figure B.2 (Cont'd)

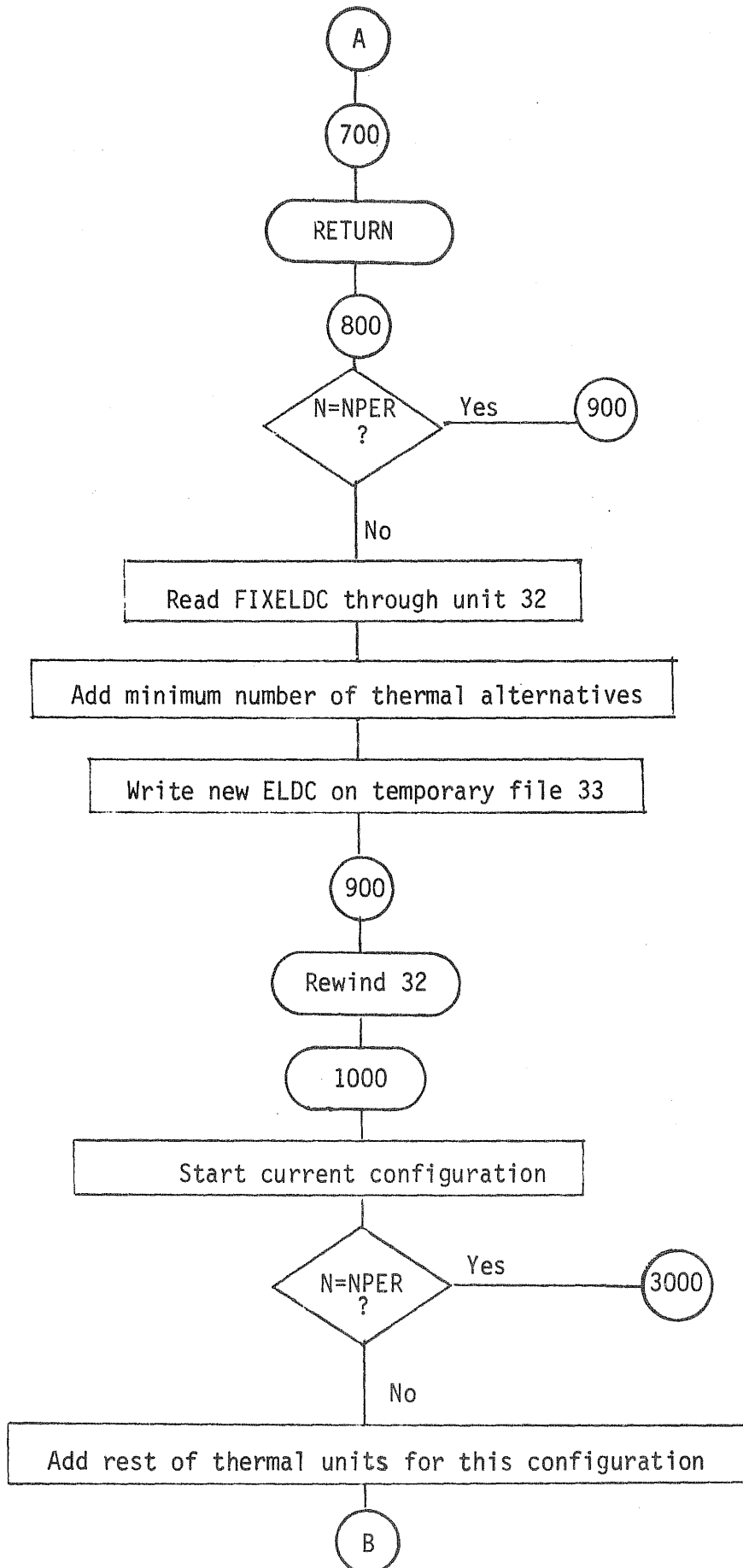
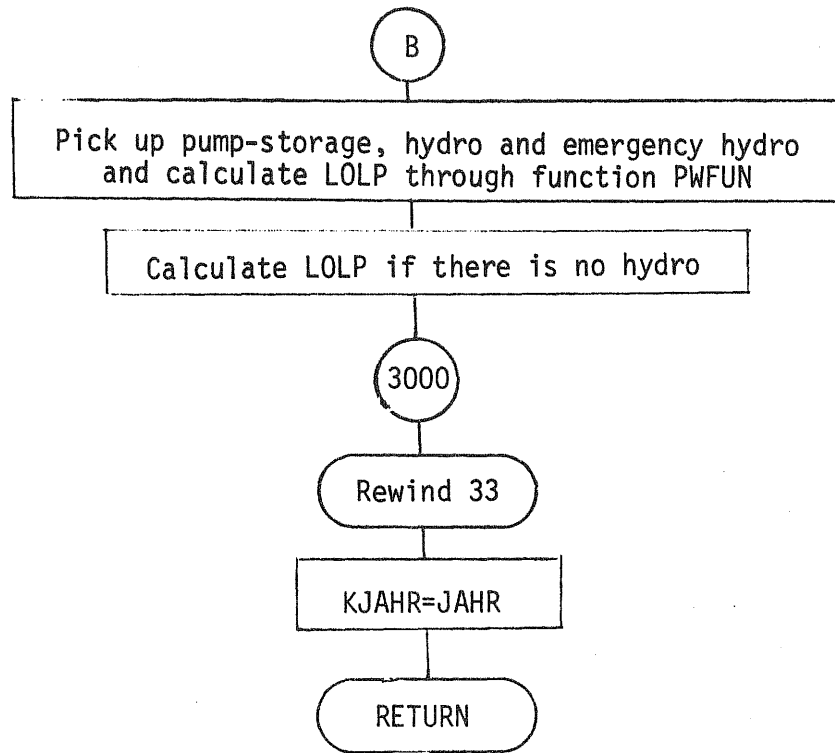


Figure B.2 (Cont'd)



Subroutine HYDALL

Array, NLIST(500), was changed to NLIST(1350).

Subroutine MILORD

The dimensions of arrays, MWCS, MWBS, DMWC, DMWB, and DSMW were changed from 100 to 270.

- b) The control variable NUMRUN was inserted after executable statement 32 in the MAIN program. At the first MERSIM run for a specific set of FIXSYS, VARSYS, and LOADSY, NUMRUN must be 1. At any subsequent run, NUMRUN  $\neq$  1. This control variable eliminates the need for an initial creation of a "null" binary disk file 16.

#### B.8 DYNPRO

Two kinds of modifications were made in DYNPRO.

- a) Array dimension changes.

Main program

The dimensions of the arrays, PLIFE, NAME, NTYPE, MWC, COSTL, COSTF, COST2L, and COST2F were changed from 101 to 271. In relation to this, the 12th executable statement was changed from

```
DO 100 I = 1, 101
```

to

```
DO 100 I = 1, 271
```

Subroutine CAPITL

Array, NTYPE(101), was changed to NTYPE(271).

- b) The fixed charge rate option was incorporated in DYNPRO as described in Ref. (3) in the bibliography of the main report.



Appendix C  
Modifications to WASP-2B User's Manual

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The modifications described in this appendix refer to the "User's Manual for WASP-2B" (also known as WASP-2, version 76-1). See Reference 2 in the Bibliography of the main report.

### C.1. Job Control Language (JCL) Modifications

- 1) The first part of Figure 2.1, creating a "null" SIMULNEW file, is not necessary.
- 2) Figure 2.3 should be replaced with Figure C.1. There are two substantial differences between the two tables other than those necessary because of differences between IAEA's and OSU's computers:
  - a) LOADSY JCL of modified WASP-2B require binary file 22 (LOADDATA)
  - b) PWCONGEN JCL of modified WASP-2B require binary files 22 (LOADDATA) and 32 (FIXELDC).

### C.2. Input Data Modifications.

#### C.2.1 LOADSY input data

Replace Table 2.1 with Table C.1. Card types 2 and 4 represent the load duration curve. Either of them can be used each year but not both together. If the load duration curve for a specific year is the same as for the previous year, type 2 or 4 cards are not required.

#### C.2.2. FIXSYS input data

There were no modifications in FIXSYS input data.

#### C.2.3. VARSYS input data

There were no modifications in VARSYS input data.

#### C.2.4. CONGEN input data

There were no modifications in CONGEN input data.

#### C.2.5. MERSIM input data

Add card type AØ to Table 2.5.

Type No.	Cols.	Format	Name	Type of Information
AØ	1-4	I	NUMRUN	The first time MERSIM is run with a specific set of FIXSYS, VARSYS, CONGEN or PWCONGEN, and MATURE runs, it must be NUMRUN = 1. NUMRUN ≠ 1 for all subsequent runs.



Figure C.1  
JCL for Modified WASP-2B

LOADSY JCL

```
// REGION=300K
/*JOBPARM LINES=10000
//LOADSY EXEC FTG1G,PARM='LET,NORES,NOMAP'
//SYSLIN DD DSN='TS0904.TS0904.LOADSYS.OBJ',DISP=SHR
//GO.FT12F001 DD DSN=TS0904.LOADUCU,
//  DISP=(OLD,KEEP),UNIT=USERDA,SPACE=(TRK,(1,1)),
//  DCB=(RECFM=VBS,LRECL=2292,BLKSIZE=2296)
//FT22F001 DD DSN=TS0904.LOADDATA,
//  DISP=(NEW,CATLG),UNIT=USERDA,SPACE=(TRK,(60,1),RLSE),
//  DCB=(RECFM=VBST,LRECL=24048,BLKSIZE=24052)
//GO.SYSIN DD *
*****          LOADSY DATA          *****
/*
//
```

FIXSYS JCL

```
// REGION=190K
/*JOBPARM LINES=10000
//FIXSYS EXEC FTG1G,PARM='LET,NORES,NOMAP'
//SYSLIN DD DSN='TS0904.TS0904.FIXSYS.OBJ',DISP=SHR
//GO.FT10F001 DD DSN=TS0904.FIXPLANT,
//  SPACE=(TRK,(1,1)),UNIT=USERDA,
//  DCB=(RECFM=VSB,BLKSIZE=176,LRECL=172),DISP=(OLD,KEEP)
//GO.SYSIN DD *
*****          FIXSYS DATA          *****
/*
//
```

VARSYS JCL

```
// REGION=190K
/*JOBPARM LINES=10000
//VARSYS EXEC FTG1G,PARM='LET,NORES,NOMAP'
//SYSLIN DD DSN='TS0904.TS0904.VARSYS.OBJ',DISP=SHR
//GO.FT11F001 DD DSN=TS0904.VARPLANT,
//  SPACE=(TRK,(1,1)),UNIT=USERDA,
//  DCB=(RECFM=VSB,BLKSIZE=176,LRECL=172),DISP=(OLD,KEEP)
//GO.SYSIN DD *
*****          VARSYS DATA          *****
/*
//
```

Figure C.1 (Con't.)

MATURE JCL

```
// REGION=190K
/*JOBPARM LINES=10000
//MATURE EXEC PROC=FORTRUN
//CMP.SYSIN DD *
***** MATURE PROGRAM *****
/*
//GO.FT35F001 DD DSN=TS0904.MATURE.MAINT,
// SPACE=(TRK,(16,1),RLSE),DCB=(RECFM=VBS,LRECL=12960,BLKSIZE=12964),
// DISP=(OLD,KEEP)
//GO.SYSIN DD *
***** MATURE DATA *****
/*
//
```

CONGEN JCL

```
// REGION=350K,TIME=2
/*JOBPARM LINES=10000,CARDS=10000
//CONGEN EXEC FTGIG,PARM='LET,NORES,NOMAP'
//SYSLIN DD DSN='TS0904.TS0904.CONGEN.OBJ',DISP=SHR
//GO.FT10F001 DD DSN=TS0904.FIXPLANT,DISP=(OLD,KEEP)
//GO.FT11F001 DD DSN=TS0904.VARPLANT,DISP=(OLD,KEEP)
//GO.FT12F001 DD DSN=TS0904.LOADDUUCU,DISP=(OLD,KEEP)
//GO.FT13F001 DD DSN=TS0904.EXPANALT,DISP=(OLD,KEEP)
//FT23F001 DD DSN=88A,DISP=(,DELETE),SPACE=(TRK,(4,1)),
// UNIT=SYSDA,DCB=(RECFM=VBS,LRECL=2404,BLKSIZE=7216)
//GO.SYSIN DD *
***** CONGEN DATA *****
/*
//
```

PWCONGEN RUN 1 JCL

```
// REGION=350K,TIME=2
/*JOBPARM LINES=10000,CARDS=10000
//PWCON1 EXEC FTGIG,PARM='LET,NORES,NOMAP',TIME=3
//SYSLIN DD DSN='TS0904.TS0904.PWCONGEN.OBJ',DISP=SHR
//GO.FT10F001 DD DSN=TS0904.FIXPLANT,DISP=(OLD,KEEP)
//GO.FT11F001 DD DSN=TS0904.VARPLANT,DISP=(OLD,KEEP)
//GO.FT12F001 DD DSN=TS0904.LOADDUUCU,DISP=(OLD,KEEP)
//GO.FT13F001 DD DSN=TS0904.EXPANALT,DISP=(OLD,KEEP)
//GO.FT22F001 DD DSN=TS0904.LOADDATA,DISP=(OLD,KEEP)
//GO.FT32F001 DD DSN=TS0904.FIXELDC,
// DISP=(NEW,CATLG),UNIT=USERDA,SPACE=(TRK,(60,1),RLSE),
// DCB=(RECFM=VBST,LRECL=24048,BLKSIZE=24052)
//FT23F001 DD DSN=88A,DISP=(,DELETE),SPACE=(TRK,(4,1)),
// UNIT=SYSDA,DCB=(RECFM=VBS,LRECL=2404,BLKSIZE=7216)
//FT33F001 DD DSN=88B,DISP=(,DELETE),SPACE=(TRK,(24,1)),UNIT=SYSDA,
// DCB=(RECFM=VBST,LRECL=24048,BLKSIZE=24052)
//GO.FT35F001 DD DSN=TS0904.MATURE.MAINT,DISP=(OLD,KEEP)
//GO.SYSIN DD *
***** PWCONGEN RUN 1 DATA *****
/*
```

Figure C.1 (Con't.)

PWCONGEN RUN 2 JCL

```
//PWCON2 EXEC FTG1G,PARM='LET,NORES,NOMAP'  
//SYSLIN DD DSN='TS0904.TS0904.PWCONGEN.OBJ',DISP=SHR  
//GO.FT10F001 DD DSN=TS0904.FIXPLANT,DISP=(OLD,KEEP)  
//GO.FT11F001 DD DSN=TS0904.VARPLANT,DISP=(OLD,KEEP)  
//GO.FT12F001 DD DSN=TS0904.LOADDUUCU,DISP=(OLD,KEEP)  
//GO.FT13F001 DD DSN=TS0904.EXPANALT,DISP=(OLD,KEEP)  
//GO.FT32F001 DD DSN=TS0904.FIXELDC,DISP=(OLD,KEEP)  
//GO.FT35F001 DD DSN=TS0904.MATURE.MAINT,DISP=(OLD,KEEP)  
//FT23F001 DD DSN=66A,DISP=(,DELETE),SPACE=(TRK,(4,1)),  
// UNIT=SYSDA,DCB=(RECFM=VBS,LRECL=2404,BLKSIZE=7216)  
//FT33F001 DD DSN=66B,DISP=(,DELETE),SPACE=(TRK,(24,1)),UNIT=SYSDA,  
// DCB=(RECFM=VBST,LRECL=24048,BLKSIZE=24052)  
//GO.SYSIN DD *  
***** PWCONGEN RUN 2 DATA *****  
/*
```

MERSIM JCL

```
//MERSIM EXEC FTG1G,PARM='LET,NORES,NOMAP'  
//SYSLIN DD DSN='TS0904.TS0904.MERSIM.OBJ',DISP=SHR  
//GO.FT08F001 DD SYSOUT=A  
//GO.FT09F001 DD DUMMY  
//GO.FT10F001 DD DSN=TS0904.FIXPLANT,DISP=(OLD,KEEP)  
//GO.FT11F001 DD DSN=TS0904.VARPLANT,DISP=(OLD,KEEP)  
//GO.FT12F001 DD DSN=TS0904.LOADDUUCU,DISP=(OLD,KEEP)  
//GO.FT13F001 DD DSN=TS0904.EXPANALT,DISP=(OLD,KEEP)  
//GO.FT15F001 DD DSN=TS0904.SIMULNEW,DISP=(OLD,KEEP)  
//GO.FT16F001 DD DSN=TS0904.SIMULOLD,DISP=(OLD,KEEP)  
//GO.SYSIN DD *  
***** MERSIM DATA *****  
/*
```

DYNPRO JCL

```
//DYNPRO EXEC FTG1G,PARM='LET,NORES,NOMAP'  
//SYSLIN DD DSN='TS0904.TS0904.DYNPRO.OBJ',DISP=SHR  
//GO.FT08F001 DD SYSOUT=A  
//GO.FT09F001 DD DUMMY  
//GO.FT07F001 DD DSN=TS0904.OSDYNDAT,DISP=(OLD,KEEP)  
//GO.FT10F001 DD DSN=TS0904.FIXPLANT,DISP=(OLD,KEEP)  
//GO.FT11F001 DD DSN=TS0904.VARPLANT,DISP=(OLD,KEEP)  
//GO.FT12F001 DD DSN=TS0904.LOADDUUCU,DISP=(OLD,KEEP)  
//GO.FT13F001 DD DSN=TS0904.EXPANALT,DISP=(OLD,KEEP)  
//GO.FT15F001 DD DSN=TS0904.SIMULNEW,DISP=(OLD,KEEP)  
//GO.FT18F001 DD DSN=TS0904.EXPANREP,DISP=(OLD,KEEP)  
//GO.SYSIN DD *  
/*  
***** DYNPRO DATA *****  
//
```

Table C.1  
Types of Data Cards Used in LOADSY

Type No.	Columns	Format	Name	Type of Information
A	1-4	I	NPER	Number of periods (seasons) per year (2 to 12). Cols 1 & 2 must be blank.
	5-8	I	NOCOF	Number of cosine terms in Fourier approximation of load duration curve (100 maximum, 50 recommended). Col.5 must be blank.
	9-12			Must remain blank
	13-16	I	NNTH	Number of points for load duration curve representation
	17-20	I	INVERT	Numbers of points used for inverted load duration curve representation.
B	1-8	F	PKMW	Annual peak load (MW)
	9-14	I	JAHR	Year number
1	1-4	I	INDEX	Index number (1 indicates end of data for this year; 2 indicates that one type-2 card follows for each season; 3 indicates that one or two type-3 cards follow; 4 indicates that (NNTH/5) + 1 cards follow). Cols. 1-3 must be blank.
2	1-12	F		$a_0$ (normally 1.0)
	13-24	F		$a_1$
	25-36	F		$a_2$
	37-48	F		$a_3$
	49-60	F		$a_4$
	61-72	F		$a_5$
3	1-8, 9-16, etc. for each period	F	PUPPK	Ratio of peak load in period 1 to annual peak, up to 10 numbers per card. For 11 or 12 periods per year, use the first one or two fields of a second type-3 card. For 4 periods for example, only the first 4 fields would be used. One of the ratios should be 1.0.

Table C.1  
Types of Data Cards Used in LOADSY (Con't.)

Type No.	Columns	Format	Name	Type of Information
4	1-16, 17-32, etc.	F		Point-wise representation of load duration curve. Use NNTH/5 cards for NNTH points for each period. Add NPER/5 cards at the end for the minimum load in each period. For example, if NNTH=720 and NPER=2, 289 cards will be needed.

### C.2.6. DYNPRO input data

Add card type 19 to Table 2.6.

Type No.	Columns	Format	Name	Type of Information
19	1-4, 5-8, etc.	F	LFCR	Levelized Fixed Charge Rate (LFCR) for each expansion candidate. LFCR = 0 or blank cause default to original method using total cost and salvage calculation.

### C.2.7. PWCONGEN input data

Add card type A to Table 2.4 that describes the CONGEN input data.

Type No.	Cols.	Format	Name	Type of Information
A	1-4	I	NRUN	NRUN = 1, PWCONGEN creates the FIXED system Equivalent Load Duration Curve (FIXELDC) NRUN≠1, the LOLP for expansion alternatives is calculated. For each set of FIXSYS, VARSYS, LOADSY and MATURE, NRUN = 1 only once. All other runs must have NRUN ≠ 1.
	5-8	I	INVERT	Number of points used for the representation of the inverted load duration curve. (Maximum = 1200)
	9-12	I	IPRERU	IPRERU = 1, the plant availability changes option is in effect. IPRERU≠1 no changes of plant availability are possible.

### C.2.8. MATURE input data

Table D.2 shows the input data card types used by MATURE. One type 3 card must be used for each power plant for which maintenance or forced outage will be modified. The combined FIXSYS and VARSYS plant order must be preserved. No adjustments are possible for hydro or pump storage plants. Add one blank card after all changes each year. The

Table C.2 MATURE Input Data

Type No.	Columns	Format	Name	Type of Information
1	1-4	I	NFP	Number of plants in the combined FIXSYS plus VARSYS list. (Maximum = 270)
	5-6	I	NPER	Number of periods per year. (Maximum = 12)
	7-8	I	NYEARS	Number of years in study period. (Maximum = 30)
	9-12	I	NYEAR	The first year of the study period.
2	1-4,9-12, etc.	A4,4X	PLANT	Plant names as described in FIXSYS and VARSYS. Ten names per card separated by ten 4-column blank fields. NFP/10 cards are required. (For example, if NFP = 28, there will be 3 cards out of which the third will contain only 8 plant names.)
3	1-3	I	I	Plant number as found in the combined FIXSYS plus VARSYS list.
	7-12	F	PMATUR	Maturity adjusting factor.
	13-16, 17-20,etc.	F	DAYS	Days of scheduled maintenance each period.

blank card will indicate the end of input for current year. This process must be repeated for each year. If no adjustments are required for a specific year, a blank card would indicate so.

### C.3. Sample input data

Table C.3 lists the input data used to obtain the output listed in Appendix D. These input data are similar to IAEA's case-26 predetermined run (listed in the reference procedures manual). Use of MATURE for plant availability adjustments changed the results.

DYNPRO input data using LFCR  $\neq$  0.0 are not presented here though a DYNPRO output with LFCR = 15.0% for all plants is provided in Appendix D.



Table C.3  
Input Data for Sample Runs of Modified WASP-2B

LOADSY DATA

2 50 7201000  
1647. 1980  
3  
.8782 1.0  
4

0.997978969566060.993975551893300.990023272646210.986121670969050.98227028845300  
0.978468669130210.974716359467910.971012908362560.967357867133880.96375078951900  
0.960191231666570.956678752130810.953212911865670.949793274218870.94641940492608  
0.943090872104950.939807246249260.936568100222970.933373009254390.93022155093022  
0.927113305189700.924047854318680.921024782943730.918043678026230.91510412885651  
0.912205727047920.909348066530920.906530743547230.903753356643890.90101550666735  
0.898316796757650.895656832342410.893035221131020.890451573108720.88790550053068  
0.885396617916110.882924542042370.880488891939080.878089288882200.87572535638814  
0.873396720207890.871103008321050.868843850930030.866618880454050.86442773152334  
0.862270040973150.860145447837930.859053593345370.855994120910550.85396667613000  
0.851970906775860.850006462789890.848072996277670.846170161502650.84429761488074  
0.842455014971950.840642022479470.838858300238780.837103513214230.83537732849269  
0.833679415277580.832009444893050.830367090728020.828752028330320.82716393537078  
0.825602491337310.824067378219050.822558279800420.821074882005250.81961687282090  
0.818183942292310.816775782516150.815392087634890.814032553830920.81269687932065  
0.811384764348600.810095911181520.809830024102470.807586809404960.80636597537498  
0.805167232345200.803990292568970.802834870334520.801700681898960.80058744549448  
0.799494881322390.798422711547230.797370660290880.796338453626690.79532581957352  
0.794332488089890.793358191068070.792402662328180.791465637612280.79054685457849  
0.789646052795090.788762973734610.787897360767950.787048959158440.78621751605601  
0.785402780491230.784604503369450.783822437464870.783056337414670.78230595971312  
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Table C.3 (Continued)

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 0.596553039513300.596228552820470.595892457005460.595544535199650.59518456876411

.595 .595  
 1  
 1936. 1981  
 1  
 2274. 1982  
 1  
 2669. 1983  
 1  
 3129. 1984  
 1  
 3666. 1985  
 3

Table C.3. (Continued)

.9237	1.0					
2						
	1.0	-3.27689	15.08061	-32.55363	30.9992	-10.70771
	1.0	-3.27689	15.08061	-32.55363	30.9992	-10.70771
1						
4290.	1986					
1						
5017.	1987					
1						
5863.	1988					
1						
6845.	1989					
1						
7985.	1990					
3						
.9545	1.0					
2						
	1.0	-3.51974	16.19426	-34.83805	33.05702	-11.37309
	1.0	-3.51974	16.19426	-34.83805	33.05702	-11.37309
1						
9307.	1991					
1						
10837.	1992					
1						
12609.	1993					
1						
14658.	1994					
1						

END OF LOADSY DATA

Table C.3 (Continued)

FIXSYS DATA

1980	2													
FHYD	1	159	324	0.	0.	0.	0.	5 0	0.0	0	0	2051.	.30	0.0
FEMH	1	44	44	2262.	2262.	10.	980.	-199	0.0	0	0	0.	.30	
FQ1H	5	34	100	2490.	2190.	10.	700.	210	3.0	28	100	0.	2.30	0.0
FQ50	8	25	50	2618.	2326.	10.	700.	210	3.0	28	50	0.	3.00	0.0
FD25	3	20	25	2175.	1800.	10.	980.	420	1.0	14	25	0.	.85	0.0
FGTH	5	29	97	6322.	2262.	10.	980.	172	2.5	14	50	0.	.52	0.0
FPST	0							6 0					.325	

1.0000	0.8750			
1.0000	0.7707			
0.5427	0.4573			
0.8841	1.0000			
3				
1.0000	1.0000	1.0000	1.0000	0.6000
0.5000	0.9500	0.8200	0.9000	0.2500
1.5000	1.1500	1.2600	1.1000	0.1500
.85	.88			

HYDRO CONDITIONS  
 NORMAL YEAR  
 DRY YEAR  
 WET YEAR

- 2
- 3
- 2
- 1 1980
- 1 1981
- 3
- 5
- 3
- 1 1982
- 1 1983
- 1 1984
- 1 1985
- 1 1986
- 1 1987
- 1 1988
- 1 1989
- 1 1990
- 1 1991
- 1 1992
- 1 1993
- 1 1994

END OF FIXSYS DATA

Table C.3 (Continued)

VARSYS DATA													
	2	9											
N600	400	600	2568.	2363.	0.	142.	0 5	12.0	42	600	0.	0.99	0.
N10H	667	1000	2566.	2361.	0.	134.	0 5	16.0	42	1000	0.	0.73	0.
C300	100	300	2480.	2180.	450.	0.0	310	7.0	35	300	0.	1.20	
C600	200	600	2460.	2160.	450.	0.0	310	12.0	42	600	0.	0.71	0.
C10H	334	1000	2440.	2140.	450.	0.0	310	16.0	42	1000	0.	0.56	
O600	200	600	2440.	2140.	10.	700.	210	10.0	42	600	0.	0.67	0.
GT2H	58	192	6322.	2262.	10.	980.	173	1.25	14	50		0.52	
VHYD	4												
	233	233	1500.										
				0			1982						
	1.00		0.67										
	1.00		0.67										
	0.59		0.41										
	0.00		0.00										
	0	349	780.	92			1984						
	1.0000		0.9748										
	0.		0.										
	0.3987		0.6013										
	0.8816		1.0000										
	106	616	2611.	138			1986						
	1.0000		0.8300										
	1.0000		0.3206										
	0.6702		0.3298										
	0.8837		1.0000										
	150	600	2800.	0			1990						
	1.0000		0.8000										
	1.0000		0.6761										
	0.5961		0.4039										
	0.0		0.0										
VPST	5												
	240	240	218.		0.85		0.88			1984			
	240	240	218.		0.85		0.88			1985			
	240	240	218.		0.85		0.88			1985			
	240	240	218.		0.85		0.88			1986			
	240	240	218.		0.85		0.88			1986			
END OF VARSYS DATA													



Table C.3 (Continued)

CONGEN DATA									
7	READ PERIOD AND ANNUAL CRITICAL LOLP								
6	1.0	1.0							
1	READ OPTION MODE								
5	CALCULATION OF LOLP AND CHECKING AGAINST CLOLP'S								
0									
4	READ MINIMUM AND MAXIMUM RESERVE MARGINS (%)								
3	0.	50.							
0	0	0	0	0	0	0	0	0	0
2	MAXIMUM ADDITIONAL NUMBER OF CANDIDATE UNITS								
0	0	0	0	0	0	0	0	0	0
1980	MINIMUM NUMBER OF CANDIDATE UNITS								
2	0	0	1	0	0	0	0	0	0
1981									
2	0	0	2	0	0	0	0	1	0
1982									
2	0	0	4	0	0	0	0	1	0
1983									
2	0	0	4	0	0	0	0	2	0
1984									
2	0	0	4	1	0	0	0	2	1
1985									
2	1	0	4	1	0	0	0	2	2
1986									
2	1	0	4	2	0	0	0	2	2
1987									
2	1	0	4	5	0	0	0	2	2
1988									
2	1	0	4	7	0	0	0	2	2
1989									
2	2	0	4	7	0	0	0	2	3
1990									
2	2	2	4	7	0	0	0	2	3
1991									
2	2	4	4	7	0	0	0	2	3
1992									
2	2	7	4	7	0	0	0	2	3
1993									
2	2	9	4	7	0	0	0	2	3
1994									

END OF CONGEN DATA

Table C.3 (Continued)

PWCONGEN RUN 1 DATA									
11000	1								
7	1.0	1.0	READ PERIOD AND ANNUAL CRITICAL LOLP						
6	READ OPTION MODE								
1	CALCULATION OF LOLP AND CHECKING AGAINST CLOLP'S								
5									
0									
4	READ MINIMUM AND MAXIMUM RESERVE MARGINS (%)								
	0.	50.							
3	MAXIMUM ADDITIONAL NUMBER OF CANDIDATE UNITS								
0	0	0	0	0	0	0	0	0	0
2	MINIMUM NUMBER OF CANDIDATE UNITS								
0	0	0	0	0	0	0	0	0	0
1980	2	0	0	0	0	0	0	0	0
1981	2	0	0	2	0	0	0	0	1
1982	2	0	0	4	0	0	0	0	1
1983	2	0	0	4	0	0	0	0	2
1984	2	0	0	4	1	0	0	0	2
1985	2	1	0	4	1	0	0	0	2
1986	2	1	0	4	2	0	0	0	2
1987	2	1	0	4	5	0	0	0	2
1988	2	1	0	4	7	0	0	0	2
1989	2	2	0	4	7	0	0	0	2
1990	2	2	2	4	7	0	0	0	2
1991	2	2	4	4	7	0	0	0	2
1992	2	2	7	4	7	0	0	0	2
1993	2	2	9	4	7	0	0	0	2
1994	2	2	9	4	7	0	0	0	2

END OF PWCONGEN RUN 1 DATA

Table C.3 (Continued)

```

PWCONGEN RUN2 DATA
21000 1
7 1.0 1.0 READ PERIOD AND ANNUAL CRITICAL LOLP
6 READ OPTION MODE
5 CALCULATION OF LOLP AND CHECKING AGAINST CLOLP'S
0
4 READ MINIMUM AND MAXIMUM RESERVE MARGINS (%)
3 0. 50.
0 0 0 0 MAXIMUM ADDITIONAL NUMBER OF CANDIDATE UNITS
2 MINIMUM NUMBER OF CANDIDATE UNITS
0 0 0 0 0 0 0 0 0
1980
2
0 0 1 0 0 0 0 0 0
1981
2
0 0 2 0 0 0 0 1 0
1982
2
0 0 4 0 0 0 0 1 0
1983
2
0 0 4 0 0 0 0 2 0
1984
2
0 0 4 1 0 0 0 2 1
1985
2
1 0 4 1 0 0 0 2 2
1986
2
1 0 4 2 0 0 0 2 2
1987
2
1 0 4 5 0 0 0 2 2
1988
2
1 0 4 7 0 0 0 2 2
1989
2
2 0 4 7 0 0 0 2 3
1990
2
2 2 4 7 0 0 0 2 3
1991
2
2 4 4 7 0 0 0 2 3
1992
2
2 7 4 7 0 0 0 2 3
1993
2
2 9 4 7 0 0 0 2 3
1994
END OF PWCONGEN RUN 2 DATA

```

Table C.3 (Continued)

MATURE DATA									
16 2151980									
FHYD	FEMH	FO1H	FO50	FD25	FGTH	FPST	N600	N10H	C300
C600	C10H	O600	GT2H	VHYD	VPST				
1	0.9								
3	0.9								
4	0.9								
11	0.9								
									END 1980
2	1.1								
4	1.1								
5	0.9								
6	1.1								
10	1.1								
									END 1981
1		20.							
5		20.							
									END 1982
									END 1983
									END 1984
1		20.							
5		20.							
									END 1985
									END 1986
									END 1987
									END 1988
1	0.9	20.	20.						
6	0.9	20.	20.						
									END 1989
									END 1990
									END 1991
									END 1992
									END 1993
									END 1994
END OF MATURE DATA									

Table C.3 (Continued)

MERSIM DATA

```

1
1980 1980
2          READ LOADING ORDER OPTION
-1.0
9      8      12      11      10 1009 1008      13      3      4 1012 1011
1010 1013 1003 1004      5      14      6 1005 1014 1006      7
3          READ MULTIPLIER ON FOREIGN COSTS
1.2
4          OUTPUT OPTION
0          MINIMUM PRINTOUT
5          DECREASE NUMBER OF FOURIER COEFFICIENTS
20
6          READ DISCOUNT RATE (%) FOR ALL LOCAL OPERATING COSTS
0.0
7          READ DISCOUNT RATE (%) FOR ALL FOREIGN OPERATING COSTS
0.0
10         DECREASE NUMBER OF HYDRO CONDITIONS TO ONE
3         (3 IS USED FOR DEMONSTRATING ERROR MESSAGE)
1980
2          READ LOADING ORDER OPTION
1.0-0.03      1      0      AUTOMATIC LOADING ORDER TO FULFILL SPIN-RESER. REQUIREM.
9      8      12      11      10      13      3      4      5      14      6      7
10
1
8          READ DISCOUNT RATES (%) ON PLANT TYPES; LOCAL AND FOREIGN
0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
9          READ ESCALATION FACTORS ON PLANT TYPES; LOCAL AND FOREIGN
1.0      1.0      1.0      1.0      1.0      1.0      1.0      1.0
1.0      1.0      1.0      1.0      1.0      1.0      1.0      1.0
1981
1982
1983
1984
2
1.0-0.05      0      1
1985
1986
1987
1988
1989
2
1.0-0.03      0      1
1990
1991
1992
1993
1994
END OF MERSIM DATA

```

Table C.3 (Continued)

DYNPRO DATA									
1980	1980	15							
0	1								
	1994		8.	8.					
15			READ DISCOUNT RATE (%) ON FOREIGN OPERATING COSTS						
	8.0								
14			READ DISCOUNT RATE (%) ON LOCAL OPERATING COSTS						
	8.0								
3			READ MULTIPLIER ON FOREIGN COSTS						
1.2									
17			READ MULTIPLIERS ON DOMESTIC AND FOREIGN OPERATING COSTS						
	1.00	1.00	1.00	1.00	1.10	1.00	1.00	1.00	
	1.00	1.00	1.00	1.00	1.10	1.00	1.00	1.00	
16			READ SALVAGE VALUE OPTION						
1			SINKING FUND OPTION						
2			READ THERMAL PLANT CAPITAL COST DATA						
	134.	586.	30.	0.0	86.0	24.0	8.0		1N600
	108.	480.	30.	0.0	79.0	24.0	8.0		2N10H
	65.	327.	30.	0.0	0.0	15.8	5.0		3C300
	51.	261.	30.	0.0	0.0	15.7	5.0		4C600
	43.	227.	30.	0.0	0.0	15.7	5.0		5C10H
	47.	239.	30.	0.0	0.0	15.7	5.0		60600
	33.	132.	20.	0.0	0.0	8.0	2.0		7GT2H
			50.						
	387.	258.				25.0	8.0		8VHYD1
	231.	154.				12.2	4.0		8VHYD2
	513.	342.				25.0	8.0		8VHYD3
	945.	630.				25.0	8.0		8VHYD4
			50.						
	364.	78.				24.0	6.0		9VPST1
	91.	78.				12.0	3.0		9VPST2
	91.	78.				12.0	3.0		9VPST3
	1000.	100.				26.0	7.0		9VPST4
	270.	100.				13.0	3.5		9VPST5
12			READ CRITICAL LOLP						
	1.0								
13			READ NUMBER OF SOLUTIONS TO REPORT						
	5								
18			READ OUTPUT OPTION						
	0		IAEA OPTION						
6			READ MAXIMUM BUILDING CONSTRAINT ON CANDIDATE UNITS						
10	10	10	10	10	10	10	10	10	
19									
1	1980								
1	1981								
1	1982								
1	1983								
1	1984								
1	1985								
1	1986								
1	1987								
1	1988								
1	1989								
1	1990								
1	1991								
1	1992								
1	1993								
1	1994								
END OF DYNPRO DATA									

## Appendix D

### Sample Output of Modified WASP-2B

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D.1. LOADSY sample output

THE NUMBER OF POINTS USED TO INVERT THE LD CURVE IS 1000  
THE MAXIMUM LENGTH OF THE E L D CURVE IS 2500

NUMBER OF FOURIER COEFF. IS 50  
HOURS IN PERIOD 4380.0  
LOADS FOR THIS PUN DEVELOPED FOR 2 PERIODS/YEAR



PEAK LOAD FOR YEAR 1980 IS 1647.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.878200 1.000000

PERIOD 1

PEAK LOAD 1446.4 MW MIN. LOAD 860.6 MW  
PIECEWISE-LINEAR LDC REPRESENTATION, WITH 720 POINTS

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 4452.4 GWH  
FOURIER SERIES 4452.5 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

FOURIER COEFFICIENTS FOR THIS PERIOD

CONSTANT, ACC IS 0.8812537

COEFFICIENTS OF COSINE TERMS ARE

0.6152533	0.1104627	-0.1530903	-0.0877959	0.0436816	0.0576932	0.0002386	-0.0285864	-0.0126941	0.0074655
-0.0095098	0.0024106	0.0012477	-0.0021541	-0.0086378	-0.0038816	0.0098663	0.0103612	-0.0053236	-0.0132841
-0.0117778	0.0113696	0.0075743	-0.0060373	-0.0095413	-0.0001894	0.0074776	0.0034778	-0.0032049	-0.0037811
-0.0005720	0.0014104	0.0022015	0.0016987	-0.0009842	-0.0035351	-0.0018438	0.0030671	0.0044159	-0.0006578
-0.0052186	-0.0022948	0.0038603	0.0042218	-0.0011598	-0.0042429	-0.0014186	0.0025714	0.0026168	-0.0002950

PERIOD 2

PEAK LOAD 1647.0 MW MIN. LOAD 980.0 MW  
PIECEWISE-LINEAR LDC REPRESENTATION, WITH 720 POINTS

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 5069.9 GWH  
FOURIER SERIES 5070.4 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

FOURIER COEFFICIENTS FOR THIS PERIOD

CONSTANT, ACC IS 0.8812537

COEFFICIENTS OF COSINE TERMS ARE

0.6152533	0.1104627	-0.1530903	-0.0877959	0.0436816	0.0576932	0.0002386	-0.0285864	-0.0126941	0.0074655
-0.0095098	0.0024106	0.0012477	-0.0021541	-0.0086378	-0.0038816	0.0098663	0.0103612	-0.0053236	-0.0132841
-0.0117778	0.0113696	0.0075743	-0.0060373	-0.0095413	-0.0001894	0.0074776	0.0034778	-0.0032049	-0.0037811
-0.0005720	0.0014104	0.0022015	0.0016987	-0.0009842	-0.0035351	-0.0018438	0.0030671	0.0044159	-0.0006578
-0.0052186	-0.0022948	0.0038603	0.0042218	-0.0011598	-0.0042429	-0.0014186	0.0025714	0.0026168	-0.0002950

0.01465  
-0.01281  
-0.003718  
-0.0002950

ANNUAL SUMMARY

ENERGY DEMAND  
POLYMERIAL  
FOURIER SERIES 9522.3 GWH  
9523.3 GWH

ANNUAL LEAD FACTOR  
POLYMERIAL  
FOURIER SERIES 66.00  
66.01

\*\*\*\*\* END OF DATA FOR YEAR 1980 \*\*\*\*\*

PEAK LOAD FOR YEAR 1981 IS 1936.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.878200 1.000000

PERIOD 1

PEAK LOAD 1700.2 MW MIN. LOAD 1011.6 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 5233.6 GWH  
FOURIER SERIES 5234.2 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

PERIOD 2

PEAK LOAD 1936.0 MW MIN. LOAD 1151.9 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 5959.5 GWH  
FOURIER SERIES 5960.1 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 11193.2 GWH  
FOURIER SERIES 11194.3 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 66.00  
FOURIER SERIES 66.01

\*\*\*\*\* END OF DATA FOR YEAR 1981 \*\*\*\*\*

PEAK LOAD FOR YEAR 1982 IS 2274.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.878200 1.000000

PERIOD 1

PEAK LOAD 1997.0 MW MIN. LOAD 1188.2 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 6147.4 GWH  
FOURIER SERIES 6148.0 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

PERIOD 2

PEAK LOAD 2274.0 MW MIN. LOAD 1353.0 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 7000.0 GWH  
FOURIER SERIES 7000.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 13147.3 GWH  
FOURIER SERIES 13148.7 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 66.00  
FOURIER SERIES 66.01

\*\*\*\*\* END OF DATA FOR YEAR 1982 \*\*\*\*\*

PEAK LOAD FOR YEAR 1983 IS 2669.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.978200 1.000000

PERIOD 1

PEAK LOAD 2343.9 MW MIN. LOAD 1394.6 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 7215.2 GWH  
FOURIER SERIES 7215.9 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

PERIOD 2

PEAK LOAD 2669.0 MW MIN. LOAD 1588.1 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 8215.9 GWH  
FOURIER SERIES 8216.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 15431.1 GWH  
FOURIER SERIES 15432.7 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 66.00  
FOURIER SERIES 66.01

\* \* \* \* \* END OF DATA FOR YEAR 1983 \* \* \* \* \*

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PEAK LOAD FOR YEAR 1984 IS 3129.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.978200 1.000000

PERIOD 1

PEAK LOAD 2747.9 MW MIN. LOAD 1635.0 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 8458.7 GWH  
FOURIER SERIES 8459.6 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

PERIOD 2

PEAK LOAD 3129.0 MW MIN. LOAD 1861.8 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 9631.9 GWH  
FOURIER SERIES 9632.9 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 70.28  
FOURIER SERIES 70.29

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 18090.6 GWH  
FOURIER SERIES 18092.5 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 66.00  
FOURIER SERIES 66.01

\*\*\*\*\* END OF DATA FOR YEAR 1984 \*\*\*\*\*

PEAK LOAD FOR YEAR 1985 IS 3666.0 MW

PERIOD PEAK LOADS AS FRACTICN. OF ANNUAL PEAK LOAD  
0.923700 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 3386.3 MW MIN. LOAD 1833.9 MW

ENERGY UNDER LOAD DURATION CURVE

POLYNOMIAL 5866.8 GWH  
FOURIER SERIES 5866.3 GWH

PERIOD LOAD FACTOR, PERCENT

POLYNOMIAL 66.52  
FOURIER SERIES 66.52

FOURIER COEFFICIENTS FOR THIS PERIOD

CONSTANT, ADD IS 0.8633615  
COEFFICIENTS OF COSINE TERMS ARE

0.6079188	0.1239694	-0.1350559	-0.0902357	0.0244641	0.0491803	0.0112987	-0.0154666	-0.0118187	-0.0018494
-0.0037392	0.0027318	-0.0107662	0.0056099	-0.0111748	-0.0136094	0.0034873	0.0150837	0.0058163	-0.0096960
-0.0106020	0.0017335	0.0088998	0.0036289	-0.0033250	-0.0038687	-0.0015081	0.0002991	0.0024067	0.0034547
0.0005002	-0.0043273	-0.0043963	0.0017560	0.0061448	0.0022185	-0.0045379	-0.0047711	0.0039336	0.0043765
0.0021413	-0.0017397	-0.0026974	-0.0009533	0.0008523	0.0017514	0.0016014	-0.0003056	-0.0026357	-0.0023463

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 3666.0 MW MIN. LOAD 1985.4 MW

ENERGY UNDER LOAD DURATION CURVE

POLYNOMIAL 10681.8 GWH  
FOURIER SERIES 10681.3 GWH

PERIOD LOAD FACTOR, PERCENT

POLYNOMIAL 66.52  
FOURIER SERIES 66.52

FOURIER COEFFICIENTS FOR THIS PERIOD

CONSTANT, ADD IS 0.8633615  
COEFFICIENTS OF COSINE TERMS ARE

0.6079188	0.1239694	-0.1350559	-0.0902357	0.0244641	0.0491803	0.0112987	-0.0154666	-0.0118187	-0.0018494
-0.0037392	0.0027318	-0.0107662	0.0056099	-0.0111748	-0.0136094	0.0034873	0.0150837	0.0058163	-0.0096960
-0.0106020	0.0017335	0.0088998	0.0036289	-0.0033250	-0.0038687	-0.0015081	0.0002991	0.0024067	0.0034547
0.0005002	-0.0043273	-0.0043963	0.0017560	0.0061448	0.0022185	-0.0045379	-0.0047711	0.0039336	0.0043765
0.0021413	-0.0017397	-0.0026974	-0.0009533	0.0008523	0.0017514	0.0016014	-0.0003056	-0.0026357	-0.0023463

.8187 -0.0018494  
18163 -0.0096960  
14067 0.0034647  
19036 -0.0043765  
16357 -0.0020463

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 20548.6 GWH  
FOURIER SERIES 20547.7 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 63.99  
FOURIER SERIES 63.98

\*\*\*\*\* END OF DATA FOR YEAR 1985 \*\*\*\*\*



PEAK LOAD FOR YEAR 1986 IS 4290.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.923700 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 3962.7 MW MIN. LOAD 2146.1 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 11546.2 GWH  
FOURIER SERIES 11545.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 4290.0 MW MIN. LOAD 2323.4 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 12500.0 GWH  
FOURIER SERIES 12499.4 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 24046.2 GWH  
FOURIER SERIES 24045.1 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 63.99  
FOURIER SERIES 63.98

\*\*\*\*\* END OF DATA FOR YEAR 1986 \*\*\*\*\*

PEAK LOAD FOR YEAR 1987 IS 5017.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.923700 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 4634.2 MW MIN. LOAD 2505.8 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 13502.9 GWH  
FOURIER SERIES 13502.3 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 5017.0 MW MIN. LOAD 2717.1 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 14618.3 GWH  
FOURIER SERIES 14617.6 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 28121.2 GWH  
FOURIER SERIES 28119.9 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 63.99  
FOURIER SERIES 63.98

\*\*\*\*\* END OF DATA FOR YEAR 1987 \*\*\*\*\*

PEAK LOAD FOR YEAR 1988 IS 5863.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.923700 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 5415.7 MW MIN. LOAD 2933.0 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 15779.8 GWH  
FOURIER SERIES 15779.1 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 5863.0 MW MIN. LOAD 3175.3 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 17083.3 GWH  
FOURIER SERIES 17082.5 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 32863.1 GWH  
FOURIER SERIES 32861.7 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 63.99  
FOURIER SERIES 63.98

\*\*\*\*\* END OF DATA FOR YEAR 1988 \*\*\*\*\*

PEAK LOAD FOR YEAR 1989 IS 6845.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.923700 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 6322.7 MW MIN. LOAD 3424.3 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 18422.8 GWH  
FOURIER SERIES 18422.0 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.276890 15.080610 -32.553630 30.999200 -10.707710

PEAK LOAD 6845.0 MW MIN. LOAD 3707.1 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 19944.6 GWH  
FOURIER SERIES 19943.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 66.52  
FOURIER SERIES 66.52

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 38367.4 GWH  
FOURIER SERIES 38365.7 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 63.99  
FOURIER SERIES 63.98

\*\*\*\*\* END OF DATA FOR YEAR 1989 \*\*\*\*\*

PEAK LOAD FOR YEAR 1990 IS 7985.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.954500 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 7621.7 MW MIN. LOAD 3966.3 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 21518.4 GWH  
FOURIER SERIES 21521.8 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

FOURIER COEFFICIENTS FOR THIS PERIOD  
CONSTANT, ACC IS 0.8472258

COEFFICIENTS OF COSINE TERMS ARE									
0.6026988	0.1356580	-0.1227057	-0.0933205	0.0124651	0.0447416	0.0166878	-0.0093284	-0.0098517	-0.0037525
-0.0053346	-0.0012518	0.0118991	0.0118947	-0.0062254	-0.0167119	-0.0048947	0.0120939	0.0121633	-0.0025020
-0.0111560	-0.0046847	0.0046166	0.0053033	0.0014730	-0.0009289	-0.0023745	-0.0033437	-0.0013212	0.0035488
0.0054462	0.0002653	-0.0060912	-0.0046495	0.0027456	0.0060286	0.0017325	-0.0036834	-0.0038719	-0.0003673
0.0025047	0.0020450	0.0005437	-0.0009539	-0.0023021	-0.0017696	0.0012486	0.0034454	0.0015649	-0.0025236

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 7985.0 MW MIN. LOAD 4155.4 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 22544.2 GWH  
FOURIER SERIES 22547.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

FOURIER COEFFICIENTS FOR THIS PERIOD  
CONSTANT, ACC IS 0.8472258

COEFFICIENTS OF COSINE TERMS ARE									
0.6026988	0.1356580	-0.1227057	-0.0933205	0.0124651	0.0447416	0.0166878	-0.0093284	-0.0098517	-0.0037525
-0.0053346	-0.0012518	0.0118991	0.0118947	-0.0062254	-0.0167119	-0.0048947	0.0120939	0.0121633	-0.0025020
-0.0111560	-0.0046847	0.0046166	0.0053033	0.0014730	-0.0009289	-0.0023745	-0.0033437	-0.0013212	0.0035488
0.0054462	0.0002653	-0.0060912	-0.0046495	0.0027456	0.0060286	0.0017325	-0.0036834	-0.0038719	-0.0003673
0.0025047	0.0020450	0.0005437	-0.0009539	-0.0023021	-0.0017696	0.0012486	0.0034454	0.0015649	-0.0025236

79

1

-0.0037525  
 -0.0025020  
 0.0035488  
 -0.0000673  
 -0.0025236

-0.0037525  
 -0.0025020  
 0.0035488  
 -0.0000673  
 -0.0025236

ANNUAL SUMMARY

ENERGY DEMAND  
 POLYNOMIAL                    44062.6 GWH  
 FOURIER SERIES                44069.5 GWH

ANNUAL LOAD FACTOR  
 POLYNOMIAL                    62.99  
 FOURIER SERIES                63.00

\*\*\*\*\* END OF DATA FOR YEAR 1990 \*\*\*\*\*

PEAK LOAD FOR YEAR 1991 IS 9307.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.954500 1.030000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 8883.5 MW MIN. LOAD 4623.0 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 25081.0 GWH  
FOURIER SERIES 25084.9 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 9307.0 MW MIN. LOAD 4843.4 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 26276.6 GWH  
FOURIER SERIES 26280.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 51357.7 GWH  
FOURIER SERIES 51365.7 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 62.99  
FOURIER SERIES 63.00

\*\*\*\*\* END OF DATA FOR YEAR 1991 \*\*\*\*\*

PEAK LOAD FOR YEAR 1992 IS 10837.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.954500 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 10343.9 MW MIN. LOAD 5393.0 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 29204.2 GWH  
FOURIER SERIES 29208.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 10837.0 MW MIN. LOAD 5635.6 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 30596.3 GWH  
FOURIER SERIES 30601.1 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 59800.5 GWH  
FOURIER SERIES 59809.8 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 62.99  
FOURIER SERIES 63.00

\*\*\*\*\* END OF DATA FOR YEAR 1992 \*\*\*\*\*



PEAK LOAD FOR YEAR 1993 IS 12609.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD

0.954500 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 12035.3 MW MIN. LOAD 6263.2 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 33979.4 GWH  
FOURIER SERIES 33984.7 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 12609.0 MW MIN. LOAD 6561.7 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 35599.2 GWH  
FOURIER SERIES 35604.8 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 69578.6 GWH  
FOURIER SERIES 69589.5 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 62.99  
FOURIER SERIES 63.00

\*\*\*\*\* END OF DATA FOR YEAR 1993 \*\*\*\*\*

PEAK LOAD FOR YEAR 1994 IS 14658.0 MW

PERIOD PEAK LOADS AS FRACTION OF ANNUAL PEAK LOAD  
0.954500 1.000000

PERIOD 1  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 13991.1 MW MIN. LOAD 7280.9 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 39501.2 GWH  
FOURIER SERIES 39507.4 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

PERIOD 2  
POLYNOMIAL COEFFICIENTS ARE  
1.000000 -3.519740 16.194260 -34.838050 33.057020 -11.373090

PEAK LOAD 14658.0 MW MIN. LOAD 7628.0 MW

ENERGY UNDER LOAD DURATION CURVE  
POLYNOMIAL 41384.2 GWH  
FOURIER SERIES 41390.6 GWH

PERIOD LOAD FACTOR, PERCENT  
POLYNOMIAL 64.46  
FOURIER SERIES 64.47

ANNUAL SUMMARY

ENERGY DEMAND  
POLYNOMIAL 80885.4 GWH  
FOURIER SERIES 80898.6 GWH

ANNUAL LOAD FACTOR  
POLYNOMIAL 62.99  
FOURIER SERIES 63.00

\*\*\*\*\* END OF DATA FOR YEAR 1994 \*\*\*\*\*

FIRST YEAR ? NO. OF SEASONS  
1980 2

CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		
NO. OF SETS	MIN. LOAD MW	CAP. CITY MW	BASE LOAD MW	AVGE INCR HEAT RATE	FUEL COSTS CENTS/MILLION	DMSTC	FORGN	TYPE	F CRCD T N	FRCD AGE RATE	DAYS SCHL MAIN	MAIN CLAS	ENRGY GWH	07M (FIX)	07M (VAR)	FULL LOAD HEAT RATE	UNIT COSTS (\$/MWH)	GENERATION BASE DOM	BASE FRGN	FLD DOM	FLD FRGN	
1	EHYD	1	159	324	0.	0.	0.0	0.0	5	0	0.0	0	0	2051.	0.300	0.0	0.	0.0	0.0	0.0	0.0	0.0
2	FE4H	1	44	44	2262.	2262.	10.00	980.00	-1	99	0.0	0	0	0.	0.300	0.0	2262.	0.2	22.2	0.2	22.2	
3	ED1H	5	34	100	2490.	2190.	10.00	700.00	2	10	3.00	28	100	0.	2.300	0.0	2292.	0.2	17.4	0.2	16.0	
4	FG50	8	25	50	2618.	2326.	10.00	700.00	2	10	3.00	28	50	0.	3.000	0.0	2472.	0.3	18.3	0.2	17.3	
5	ED25	3	20	25	2175.	1800.	10.00	980.00	4	20	1.00	14	25	0.	0.850	0.0	2100.	0.2	21.3	0.2	20.6	
6	FGTH	5	29	97	6322.	2262.	10.00	980.00	1	72	2.50	14	50	0.	0.520	0.0	3476.	0.6	62.0	0.3	34.1	
7	EPST	0	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.	0.325	0.0	0.	0.0	0.0	0.0	0.0	
8		0	0	0	0.	0.	0.0	0.0	0	0	0.0	0	0	0.	0.0	0.0	0.	0.0	0.0	0.0	0.0	

HYDRO SEASONAL FACTORS, CAPACITY MULTIPLIER, BASE CAP MULTIPLIER, ENERGY ALLOCATION

1.0000 0.8750  
1.0700 0.7707  
0.5427 0.4573

HYDRO CAPACITY FACTORS 78.4 75.5

EMERGENCY HYDRO CAPACITY SEASONAL MULTIPLIERS  
0.8541 1.0000

MULTIPLIERS ON HYDRO SEASONAL FACTORS FOR 3 CONDITION(S)

BASFAC	TOTFAC	ENGFAC	EMGFAC	PROB
1.0000	1.0000	1.0000	1.0000	0.6000
0.5000	0.5000	0.8200	0.9000	0.2500
1.5000	1.1500	1.2600	1.1000	0.1500

PUMPED STORAGE--PUMP EFF, GEN EFF, CYCLE EFF.  
0.8500 0.8800 0.7480

INDEX  
ADD 2 SETS TO PLANT 3

INDEX 1

SYSTEM FIXED CAPACITY SUMMARY	
HYDRO CAPACITY	324 283
EMERGENCY HYDRO CAPACITY	38 44
PUMP STORAGE CAPACITY	0 0
ALL OTHER CAPACITY	1660 1660
TOTAL CAPACITY	2022 1987

END OF DATA FOR YEAR 1980 \* \* \* \* \*

INDEX 1  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1660 1660  
 TOTAL CAPACITY 2022 1987  
 END OF DATA FOR YEAR 1981 \* \* \* \* \*

INDEX 2  
 RETIRE 3 UNITS FROM PLANT 5

INDEX 1  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912  
 END OF DATA FOR YEAR 1982 \* \* \* \* \*

INDEX 1  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912  
 END OF DATA FOR YEAR 1983 \* \* \* \* \*

INDEX 1  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912  
 END OF DATA FOR YEAR 1984 \* \* \* \* \*

INDEX 1  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912  
 END OF DATA FOR YEAR 1985 \* \* \* \* \*

INDEX  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1986 \* \* \* \* \*

INDEX  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1987 \* \* \* \* \*

INDEX  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912

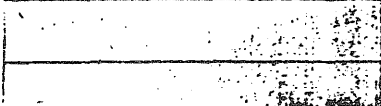
END OF DATA FOR YEAR 1988 \* \* \* \* \*

INDEX  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1989 \* \* \* \* \*

INDEX  
 SYSTEM FIXED CAPACITY SUMMARY  
 HYDRO CAPACITY 324 283  
 EMERGENCY HYDRO CAPACITY 38 44  
 PUMP STORAGE CAPACITY 0 0  
 ALL OTHER CAPACITY 1585 1585  
 TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1990 \* \* \* \* \*



INDEX  
SYSTEM FIXED CAPACITY SUMMARY  
HYDRO CAPACITY 324 283  
EMERGENCY HYDRO CAPACITY 38 44  
PUMP STORAGE CAPACITY 0 0  
ALL OTHER CAPACITY 1585 1585  
TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1991 \* \* \* \* \*

INDEX  
SYSTEM FIXED CAPACITY SUMMARY  
HYDRO CAPACITY 324 283  
EMERGENCY HYDRO CAPACITY 38 44  
PUMP STORAGE CAPACITY 0 0  
ALL OTHER CAPACITY 1585 1585  
TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1992 \* \* \* \* \*

INDEX  
SYSTEM FIXED CAPACITY SUMMARY  
HYDRO CAPACITY 324 283  
EMERGENCY HYDRO CAPACITY 38 44  
PUMP STORAGE CAPACITY 0 0  
ALL OTHER CAPACITY 1585 1585  
TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1993 \* \* \* \* \*

INDEX  
SYSTEM FIXED CAPACITY SUMMARY  
HYDRO CAPACITY 324 283  
EMERGENCY HYDRO CAPACITY 38 44  
PUMP STORAGE CAPACITY 0 0  
ALL OTHER CAPACITY 1585 1585  
TOTAL CAPACITY 1947 1912

END OF DATA FOR YEAR 1994 \* \* \* \* \*

2		9		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE		CARD IMAGE	
NO. OF SETS	MIN. LOAD MW	CAP- CITY MW	BASE LOAD HEAT RATE	AVGE INCR HEAT RATE	FUEL COSTS CENTS/MILLION	DMSTC	FORGN	TYPE	L C T	FRCD OUT-AGE	DAYS SCHL MAIN	EMRGY GWH	Q?M (FIX)	Q?M (VAR)	FULL LOAD HEAT RATE	UNIT COSTS \$/MWH	GENERATION BASE FLO	BASE FLO DOM	FLO FRGN	FLO FRGN	
1	4600	0	400	600	2568.	2363.	0.0	142.00	0	5	12.00	42	600	0.	0.990	0.0	2500.	0.0	3.6	0.0	3.5
2	H10H	0	667	1000	2566.	2361.	0.0	134.00	0	5	16.00	42	1000	0.	0.730	0.0	2498.	3.0	3.4	0.0	3.3
3	C300	0	100	300	2480.	2180.	450.00	0.0	3	10	7.00	35	300	0.	1.200	0.0	2280.	11.2	0.0	10.3	0.0
4	C600	0	200	600	2460.	2160.	450.00	0.0	3	10	12.00	42	600	0.	0.710	0.0	2260.	11.1	0.0	10.2	0.0
5	C10H	0	334	1000	2440.	2140.	450.00	0.0	3	10	16.00	42	1000	0.	0.560	0.0	2240.	11.0	0.0	10.1	0.0
6	O500	0	200	600	2440.	2140.	10.00	700.00	2	10	10.00	42	600	0.	0.670	0.0	2240.	0.2	17.1	0.2	15.7
7	GT2H	0	58	192	6322.	2262.	10.00	980.00	1	73	1.25	14	50	0.	0.520	0.0	3488.	0.6	62.0	0.3	34.2
8	VHYD	4	0	0	0.	0.	0.0	0.0	5	0	0.0	0	0	0.	0.0	0.0	0.	0.0	0.0	0.0	0.0
PROJECT DATA																					
233	233	1500.	0	0.0	0.0	1982	1														
1.0000	0.6700																				
1.0000	0.6700																				
0.5900	0.4100																				
0.0	0.0																				
CUMULATIVE OPTIONAL HYDRO ADDITION COMSTS THRU PROJ 1 YEAR AVAILAELE 1982																					
BASE CAP.	233	CAPACITY	233	ANNUAL ENERGY	1500.00	AVAIL. EMERGENCY CAPACITY	0														
1.0000	0.6700																				
1.0000	0.6700																				
0.5900	0.4100																				
0.0	0.0																				
PROJECT DATA																					
0	349	780.	92	0.0	0.0	1984	1														
1.0000	0.6748																				
0.0	0.0																				
0.3587	0.6013																				
0.8816	1.0000																				
CUMULATIVE OPTIONAL HYDRO ADDITION COMSTS THRU PROJ 2-YEAR AVAILAELE 1984																					
BASE CAP.	233	CAPACITY	582	ANNUAL ENERGY	2280.00	AVAIL. EMERGENCY CAPACITY	92														
1.0000	0.8528																				
1.0000	0.6700																				
0.5246	0.4754																				
0.8816	1.0000																				

00

106

PROJECT DATA																					
106	416	2611	138	0.0	0.0	1986	1														
1.0000	0.8300																				
1.0000	0.3206																				
0.6702	0.3298																				
0.8837	1.0000																				
CUMULATIVE OPTIONAL HYDRO ADDITION CONSTS THRU PROJ 3 YEAR AVAILABLE 1986																					
BASE CAP.	339	CAPACITY	1198	ANNUAL ENERGY	4891.00	AVAIL. EMERGENCY CAPACITY	230														
1.0000	0.8411																				
1.0000	0.5607																				
0.6023	0.3977																				
0.8829	1.0000																				
PROJECT DATA																					
150	600	2800	0	0.0	0.0	1990	1														
1.0000	0.8000																				
1.0000	0.6761																				
0.5961	0.4039																				
0.0	0.0																				
CUMULATIVE OPTIONAL HYDRO ADDITION CONSTS THRU PROJ 4 YEAR AVAILABLE 1990																					
BASE CAP.	489	CAPACITY	1798	ANNUAL ENERGY	7691.00	AVAIL. EMERGENCY CAPACITY	230														
1.0000	0.8274																				
1.0000	0.5961																				
0.6000	0.4000																				
0.8829	1.0000																				
9	VPST	5	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.0	0.325	0.0	0.	0.0	0.0	0.0	0.0
PROJECT DATA																					
240	240	218.	0	0.8500	0.8800	1984	0														
CUMULATIVE, EFFECTIVE, OPTIONAL P. STGE. CONSTS THRU PROJ 1 YEAR AVAILABLE 1984																					
PUMP CAP	240	GEN. CAP.	240	MAXIMUM ENERGY	218.00	GWH, CYCLE EFF.	0.748														
PROJECT DATA																					
240	240	218.	0	0.8500	0.8800	1985	0														
CUMULATIVE, EFFECTIVE, OPTIONAL P. STGE. CONSTS THRU PROJ 2 YEAR AVAILABLE 1985																					
PUMP CAP	480	GEN. CAP.	480	MAXIMUM ENERGY	436.00	GWH, CYCLE EFF.	0.748														
PROJECT DATA																					
240	240	218.	0	0.8500	0.8800	1985	0														
CUMULATIVE, EFFECTIVE, OPTIONAL P. STGE. CONSTS THRU PROJ 3 YEAR AVAILABLE 1985																					
PUMP CAP	720	GEN. CAP.	720	MAXIMUM ENERGY	654.00	GWH, CYCLE EFF.	0.748														
PROJECT DATA																					
240	240	218.	0	0.8500	0.8800	1986	0														
CUMULATIVE, EFFECTIVE, OPTIONAL P. STGE. CONSTS THRU PROJ 4 YEAR AVAILABLE 1986																					
PUMP CAP	960	GEN. CAP.	960	MAXIMUM ENERGY	872.00	GWH, CYCLE EFF.	0.748														
PROJECT DATA																					
240	240	218.	0	0.8500	0.8800	1986	0														
CUMULATIVE, EFFECTIVE, OPTIONAL P. STGE. CONSTS THRU PROJ 5 YEAR AVAILABLE 1986																					
PUMP CAP	1200	GEN. CAP.	1200	MAXIMUM ENERGY	*****	GWH, CYCLE EFF.	0.748														



D.4. MATURE sample output

T

COMBINED FIXSYS AND VARSYS PLANT LIST

1 FHYD 2 FF4H 3 FO1M 4 FO50 5 FO25 6 FGTH 7 FPST 8 N600 9 N10M 10 C300  
 11 C600 12 C10H 13 O600 14 G12H 15 WHYD 16 VPST 17 18 19 20

PLANT ADJUSTING FACTORS

YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
	1	FHYD	0.900	0.900
	3	FO1H	0.900	0.900
	4	FO50	0.900	0.900
	11	C600	0.900	0.900
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
	2	FEMH	1.100	1.100
	4	FO50	1.100	1.100
	5	FD25	0.900	0.900
	6	FGTH	1.100	1.100
	10	C300	1.100	1.100
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
	1	FHYD	0.0	0.0
	5	FD25	0.0	0.0
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
	1	FHYD	0.0	0.0
	5	FD25	0.0	0.0
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
	1	FHYD	0.801	0.801
	6	FGTH	0.801	0.801
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	
YEAR:	PLANT NUMBER	PLANT NAME	ADJUSTING FACTORS FOR EACH PERIOD	

NUMBER OF PMCONGEN RUNS IS 1  
 NUMBER OF POINTS FOR TLDC REPRESENTATION IS 1000  
 PLANT AVAILABILITY CHANGES OPTION IN EFFECT

NUMBER OF ALTERNATIVES FROM WHICH TO CHOOSE IS 9  
 NUMBER OF PERIODS IN YEAR IS 2  
 NUMBER OF FOURIER COEFF. IS 50

NAME	NO. OF SETS	MIN. LOAD MW	CAP. CITY MW	BASE LOAD HEAT RATE	AVGE INCR HEAT RATE	FUEL COSTS		TYPE	L C N	FRCD OUT-AGE RATE	DAYS SCHL MAIN	MAIN CLAS	ENRGY GWH	Q2M (FIX)	Q2M (VAR)	
						DMSTC	FORGN									
FIXED SYSTEM																
1	FHYD	1	159	324	0.	0.	0.0	0.0	5	0	0.0	0	0	2051.	0.300	0.0
2	FEMH	1	44	44	2262.	2262.	10.00	980.00	-1	99	0.0	0	0	0.	0.300	0.0
3	FOIH	5	34	100	2490.	2190.	10.00	700.00	2	10	3.00	28	100	0.	2.300	0.0
4	FC50	8	25	50	2618.	2326.	10.00	700.00	2	10	3.00	28	50	0.	3.000	0.0
5	FD25	3	20	25	2175.	1800.	10.00	980.00	4	20	1.00	14	25	0.	0.850	0.0
6	FGTH	5	29	97	6322.	2262.	10.00	980.00	1	72	2.50	14	50	0.	0.520	0.0
7	FPST	0	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.	0.325	0.0
VARIABLE SYSTEM																
8	N600	0	400	600	2568.	2363.	0.0	142.00	0	5	12.00	42	600	0.	0.990	0.0
9	N10H	0	667	1000	2566.	2361.	0.0	134.00	0	5	16.00	42	1000	0.	0.730	0.0
10	C300	0	100	300	2480.	2180.	450.00	0.0	3	10	7.00	35	300	0.	1.200	0.0
11	C600	0	200	600	2460.	2160.	450.00	0.0	3	10	12.00	42	600	0.	0.710	0.0
12	C10H	0	334	1000	2440.	2140.	450.00	0.0	3	10	16.00	42	1000	0.	0.560	0.0
13	O600	0	200	600	2440.	2140.	10.00	700.00	2	10	10.00	42	600	0.	0.670	0.0
14	GT2H	0	58	192	6322.	2262.	10.00	980.00	1	73	1.25	14	50	0.	0.520	0.0
15	VHYD	4	0	0	0.	0.	0.0	0.0	5	0	0.0	0	0	0.	0.0	0.0
16	VPST	5	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.	0.325	0.0

POSITION OF HYDRO EMERG.H. PUMPED STG

1 2 7

INDEX READ 7  
INDEX READ 6  
INDEX READ 5  
INDEX READ 4  
INDEX READ 3  
INDEX READ 2  
INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1980

MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000

OPTIGN FOR MODE OF GENERATION (IOPGN) 1

MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000

FIXED CAPACITY--OTHER, HYDRO, EHYD, PSICE

1660 324 38 0  
1660 283 44 0

CRITICAL PERIOD IS 2 CAPACITY RANGE IS 1647 2470

INST. CAP. DURING CRIT PER 1987.0

MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION

THIS IS THE FIRST PWCCNGEN RUN AND LOLP VALUES ARE MEANINGLESS

1 1 1987 2.52261 0.6262 4.4310 0.0 0.0 0 0 0 0 0 0 0 0

CONFIGURATIONS THIS YEAR 1  
CONFIGURATIONS THROUGH THIS YEAR 1

END OF YEAR 1980

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1981  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 1 0 0 0 0 C 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 C 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (TOPN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY - OTHER, HYDRO, FHYD, PSTGE

1660 324 38 0  
 1660 293 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 1936 2904  
 INST. CAP DURING CRIT PER 2287.0

MINIMUM NUMBER OF FOURTR. COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER. IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED CONFIGURATION																	
THIS IS THE FIRST PHCCGEN RUN AND LOLP VALUES ARE MEANINGLESS																							
2	1	2287	4.86542	1.5672	8.1637	0.0	0.0	0	0	1	0	0	0	0	0	0	0						

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 2  
 \* \* \* \* \* END OF YEAR 1981 \* \* \* \* \*

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INDEX READ 2  
INDEX READ 1  
CONDTICS GOVERNING ALTERNATIVE GENERATION, YEAR 1982  
MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 2 0 0 0 0 1 0  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
OPTION FOR MODE OF GENERATION (IOPIN) 1  
MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
FIXED CAPACITY--OTHER, HYDR, EHYD, PSTGE  
1585 324 38 0  
1585 283 44 0  
CRITICAL PERIOD IS 2 CAPACITY RANGE IS 2274 3411  
INST. CAP DURING CRIT PER 2668.1  
MINIMUM NUMBER OF EQUIV. COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION
THIS IS THE FIRST PWCCNGEN RUN AND LOLP VALUES ARE MEANINGLESS					
3	1	2668	*****	*****	0.0 0.0 0 0 2 0 0 0 0 1 0
0	0	2	0	0	0 1 0
1	1	1	1	1	0
CONFIGURATIONS THIS YEAR 1					
CONFIGURATIONS THROUGH THIS YEAR 3					
* * * * * END OF YEAR 1982 * * * * *					

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1983  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 0 0 0 0 1 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (ICPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, HYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 2669 4003  
 INST. CAP DURING CRIT PER 3268.1  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT. PER. IS 5

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION  
 THIS IS THE FIRST PWCONGEN RUN AND LOLP VALUES ARE MEANINGLESS  
 4 1 3268 \*\*\*\*\* \*\*\*\*\* 0.0 0.0 0 0 4 0 0 0 0 1 0  
 0 0 4 C 0 0 1 0  
 1 1 1 1 1 1 1

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 4  
 \*\*\*\*\* END OF YEAR 1983 \*\*\*\*\*

07

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1984  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 0 0 0 0 2 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (IOPIN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 3129 4693  
 INST. CAP DURING CRIT PER 1700.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE IC CAP LOLP SEASCHAL LOLP ACCEPTED CONFIGURATION  
 THIS IS THE FIRST PWCCNGEN RUN AND LCLP VALUES ARE MEANINGLESS  
 5 1 3700 \*\*\*\*\* \*\*\*\*\* \*\*\*\*\* 0.0 0.0 0 0 4 0 0 0 0 2 0  
 0 0 0 0 0 2 0  
 CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 5  
 \* \* \* \* \* END OF YEAR 1984 \* \* \* \* \*



INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1985  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 1 0 0 0 2 1  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (LOPIN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 3666 5499  
 INST. CAP DURING CRIT PER 4540.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION  
 THIS IS THE FIRST PWCCNGEN RUN AND LOLP VALUES ARE MEANINGLESS  
 5 0 1 4540 \*\*\*\*\* \*\*\*\*\* 0.0 0.0 0 0 4 1 0 0 0 2 1  
 0 0 4 1 0 0 2 1 1 1  
 CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 6  
 \* \* \* \* \* END OF YEAR 1985 \* \* \* \* \*

```

INDEX READ 2
INDEX READ 1
CONDITIONS GOVERNING ALTERNATIVE GENERATION YEAR 1986
MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 1 0 0 0 2 2
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000
ORIGN.FCR MODE OF GENERATION (IDPTN) 1
MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000
FIXED CAPACITY--OTHER, HYDR, EHYD, PSTGE
1585 324 44 0
1565 283 22 0
CRITICAL PERIOD IS 2 CAPACITY RANGE IS 4290 6435
INST. CAP DURING CRIT PER 5383.3
MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE IC CAP LOLP SEASCNAL LOLP ACCEPTED CONFIGURATION
THIS IS THE FIRST PWCCNEN RUN AND LOLP VALUES ARE MEANINGLESS
7 1 5380 ***** ***** ***** 0.0 0.0 1 0 4 1 0 0 0 2 2
1 0 4 1 0 0 0 2 2
1 1 1 1 1 1
CONFIGURATIONS THIS YEAR 1
CONFIGURATIONS THROUGH THIS YEAR 7
***** END OF YEAR 1986 *****

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001

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1987  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 2 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, HYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 5017 7525  
 INST. CAP DURING CRIT PER 5980.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION
THIS IS THE FIRST PCONGEN RUN AND LOLP VALUES ARE MEANINGLESS					
8	1	5980	*****	*****	0.0 0.0 1 0 4 2 0 0 0 2 2
1	0	4	2	0 0 0 2 2	
1	1	1	1	1	
CONFIGURATIONS THIS YEAR 1					
CONFIGURATIONS THROUGH THIS YEAR 8					
***** END OF YEAR 1987 *****					

INDEX READ 2  
INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1988

MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 5 0 0 0 2 2  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
OPTION FOR MODE OF GENERATION (TOP IN)

MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE

1585 324 38 0  
1585 283 44 0  
CRITICAL PERIOD IS 2 CAPACITY RANGE IS 5863 8794  
INST. CAP DURING CRIT PER 7780.3

MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE IC CAP LOLP SEASCHAL LOLP ACCEPTED CONFIGURATION

THIS IS THE FIRST PWCCGEN RUN AND LOLP VALUES ARE MEANINGLESS  
9 1 7780 \*\*\*\*\* \*\*\*\*\* \*\*\*\*\* 0.0 0.0 1 0 4 5 0 0 0 2 2  
1 0 4 5 0 0 0 2 2

CONFIGURATIONS THIS YEAR 1  
CONFIGURATIONS THROUGH THIS YEAR 9  
\* \* \* \* \* END OF YEAR 1988 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1989  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 7 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 374 38 0  
 1585 293 44 0

CRITICAL PERIOD IS 2 CAPACITY RANGE IS 6845 10267  
 INST. CAP DURING CRIT PER 8980.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION  
 THIS IS THE FIRST PHCCNGEN RUN AND LOLP VALUES ARE MEANINGLESS  
 10 1 8980 \*\*\*\*\* \*\*\*\*\* \*\*\*\*\* 0.0 0.0 1 0 4 7 0 0 0 2 2  
 1 0 4 7 C C 0 2 2  
 1 1 1 1 1 1  
 CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 10  
 \* \* \* \* \* END OF YEAR 1989 \* \* \* \* \*

INDEX READ 2  
INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION YEAR 1990

MINIMUM REQUIRED OF EACH ALTERNATIVE 2 0 4 7 0 0 0 2 3  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 C 0 0 0 C 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
OPTION FOR MODE OF GENERATION (TOPIN) 1

MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000

FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
1565 324 38 0  
1565 283 44 0

CRITICAL PERIOD IS 2 CAPACITY RANGE IS 7985 11977  
INST. CAP DURING CRIT PER 9820.3

MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION

THIS IS THE FIRST PHCCNGEN RUN AND LOLP VALUES ARE MEANINGLESS  
1 1 9820 \*\*\*\*\* \*\*\*\*\* 0.0 0.0 2 0 4 7 0 0 0 2 3  
2 0 4 7 C 0 0 2 3  
1 1 1 1 1 1 1 1

CONFIGURATIONS THIS YEAR 1  
CONFIGURATIONS THROUGH THIS YEAR 11  
\* \* \* \* \* END OF YEAR 1990 \* \* \* \* \*

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INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1991  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 2 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.0000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.0000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 2A 0  
 1585 293 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 9307 13960  
 INST. CAP DURING CRIT PER 11820.3  
 MINIMUM NUMBER OF EQUIP. COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION
12	1	11820	*****	*****	0.0 0.0 2 2 4 7 0 0 0 2 3
2	2	4	7	0 0 0	2 3
1	1	1	1	1	1

THIS IS THE FIRST PWCONGEN RUN AND LOLP VALUES ARE MEANINGLESS  
 CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 12  
 \* \* \* \* \* END OF YEAR 1991 \* \* \* \* \*

INDEX READ 2

INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1992

MINIMUM REQUIRED OF EACH ALTERNATIVE 2 4 4 7 0 0 0 2 3

MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0

RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000

OPTION FOR MODE OF GENERATION (TOPIN) 1

MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500

ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000

FIXED CAPACITY--OTHER, HYDRO, CHYD, PSTGE

1585 324 38 0

1585 283 44 0

CRITICAL PERIOD IS 2 CAPACITY RANGE IS 10837 16255

INST. CAP DURING CRIT PER 13820.3

MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION

THIS IS THE FIRST PWCCNGEN RUN AND LOLP VALUES ARE MEANINGLESS

13 4 1 13820 \*\*\*\*\* \*\*\*\*\* \*\*\*\*\* 0.0 0.0 2 4 4 7 0 0 0 2 3

1 1 1 1 1 1 1 1 1

CONFIGURATIONS THIS YEAR 13

CONFIGURATIONS THROUGH THIS YEAR \* \* \* \* \* END OF YEAR 1992 \* \* \* \* \*



INDEX READ 2  
INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1993

MINIMUM REQUIRED OF EACH ALTERNATIVE 2 7 4 7 0 0 0 2 3  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
OPTION FOR MODE OF GENERATION (TOPIN) 1

MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000

FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE

1585 324 38 0  
1585 283 44 0

CRITICAL PERIOD IS 2 CAPACITY RANGE IS 12609 18913

INST. CAP DURING CRIT PER 16820.3

MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION

THIS IS THE FIRST PWCAGEN RUN AND LOLP VALUES ARE MEANINGLESS

14 1 16820 \*\*\*\*\* \*\*\*\*\* \*\*\*\*\* 0.0 0.0 2 7 4 7 0 0 0 2 3

2 7 4 7 0 0 0 2 3

1 1 1 1 1 1 1 1

CONFIGURATIONS THIS YEAR 1

CONFIGURATIONS THROUGH THIS YEAR 14

\* \* \* \* \* END OF YEAR 1993 \* \* \* \* \*

INDEX READ 2  
INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1994

MINIMUM REQUIRED OF EACH ALTERNATIVE 2 9 4 7 0 0 0 2 3  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
OPTION FOR MODE OF GENERATION (LOPIN) 1

MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000

FIXED CAPACITY--OTHER, HYDRO, FHYD, PSTGE

1585 324 38 0  
1585 283 44 0

CRITICAL PERIOD IS 2 CAPACITY RANGE IS 14658 21987

INST. CAP DURING CRIT PER 18821.3

MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE IC CAP LOLP SEASONAL LOLP ACCEPTED CONFIGURATION

THIS IS THE FIRST PWCONGEN RUN AND LOLP VALUES ARE MEANINGLESS

15 1 18820 \*\*\*\*\* \*\*\*\*\* \*\*\*\*\* 0.0 0.0 2 9 4 7 0 0 0 2 3  
2 1 4 7 0 0 0 2 3  
1 1 1 1 1 1 1 1

CONFIGURATIONS THIS YEAR

CONFIGURATIONS THROUGH THIS YEAR 15

\* \* \* \* \* EAD OF YEAR 1994 \* \* \* \* \*

LIST OF > OF CONFIGURATIONS PER YEAR

1980  
 1981  
 1982  
 1983  
 1984  
 1985  
 1986  
 1987  
 1988  
 1989  
 1990  
 1991  
 1992  
 1993  
 1994

TOTAL 15

NUMBER OF PMCONGEN RUNS IS 2  
 NUMBER OF POINTS FOR ILDC REPRESENTATION IS 1000  
 PLANT AVAILABILITY CHANGES OPTION IN EFFECT

NUMBER OF ALTERNATIVES FROM WHICH TO CHOOSE IS 9  
 NUMBER OF PERIODS IN YEAR IS 2  
 NUMBER OF FOURIER COEFF. IS 50

NAME	SETS	MIN. LOAD MW	CAP- CITY MW	BASE LOAD HEAT RATE	AVG INCR HEAT RATE	FUEL COSTS CENTS/MILLION		TYPE	L C	FRCD OUT-AGE	DAYS SCHL	MAIN CLAS	EMRGY GWH	O?M (FIX)	O?M (VAR)	
						DMSTC	FORGN									
FIXED SYSTEM																
1	PHYD	1	159	374	0.	0.	0.0	0.0	5	0	0.0	0	0	2051.	0.300	0.0
2	FEMH	1	44	44	2262.	2262.	10.00	980.00	-1	99	0.0	0	0	0.	0.300	0.0
3	FOIH	5	34	100	2490.	2190.	10.00	700.00	2	10	3.00	28	100	0.	2.300	0.0
4	FO50	8	25	50	2618.	2326.	10.00	700.00	2	10	3.00	28	50	0.	3.000	0.0
5	FO25	3	20	25	2175.	1800.	10.00	980.00	4	20	1.00	14	25	0.	0.850	0.0
6	FGTH	5	29	57	6322.	2262.	10.00	980.00	1	72	2.50	14	50	0.	0.520	0.0
7	FPST	0	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.	0.325	0.0
VARIABLE SYSTEM																
8	N600	0	400	600	2568.	2363.	0.0	142.00	0	5	12.00	42	600	0.	0.990	0.0
9	N10H	0	667	1000	2566.	2361.	0.0	134.00	0	5	16.00	42	1000	0.	0.730	0.0
10	C300	0	100	300	2480.	2180.	450.00	0.0	3	10	7.00	35	300	0.	1.200	0.0
11	C600	0	200	600	2460.	2160.	450.00	0.0	3	10	12.00	42	600	0.	0.710	0.0
12	C10H	0	334	1000	2440.	2140.	450.00	0.0	3	10	16.00	42	1000	0.	0.560	0.0
13	O600	0	200	600	2440.	2140.	10.00	700.00	2	10	10.00	42	600	0.	0.670	0.0
14	GT2H	0	58	192	6322.	2262.	10.00	980.00	1	73	1.25	14	50	0.	0.520	0.0
15	VHYD	4	0	0	0.	0.	0.0	0.0	5	0	0.0	0	0	0.	0.0	0.0
16	VPST	5	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.	0.325	0.0
POSITION OF HYDRO EMERG.H. PUMPED STG																
		1	2	7												

INDEX	READ	7
INDEX	READ	6
INDEX	READ	5
INDEX	READ	4
INDEX	READ	3
INDEX	READ	2
INDEX	READ	1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1980  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (DPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTER, HYDR, ENYD, PSTGE  
 1660 324 38 0  
 1660 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 1647 2470  
 INST. CAP DURING CRIT PER 1987.0  
 MINIMUM NUMBER OF QUARTER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
1	1	1987	0.03973	0.0008	0.0787	0.0	0 0 0 0 0 0 0 0 0
0	0	0	0	0	0	0	0 0 0 0 0 0 0 0 0
1	1	1	1	1	1	1	1

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR \* \* \* \* \* END OF YEAR 1980 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1981  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 1 0 0 0 0 0 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1660 324 38 0  
 1850 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 1936 2904  
 INST. CAP DURING CRIT PER 2287.0  
 MINIMUM NUMBER OF EQUIPMENT COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION	
2	1	2287	0.0000	0.0	0.0000	0.0	0 0 1 0 0 0 0 0 0	
0	0	1	0	0	0	0	0 0 0 0 0 0 0 0 0	
1	1	1	1	1	1	1	1 1 1 1 1 1 1 1 1	
CONFIGURATIONS THIS YEAR							1	
CONFIGURATIONS THROUGH THIS YEAR							2	
* * * * *							END OF YEAR 1981	* * * * *

INDEX READ 2  
INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1982

MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 2 0 0 0 0 1 0  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000

OPTION FOR MODE OF GENERATION (OPTN)  
MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
FIXED CAPACITY--OTL, HYDRO, EHYD, PSTGE

1585 324 38 0  
1585 283 44 0  
CRITICAL PERIOD IS 2 CAPACITY RANGE IS 2274 3411  
INST. CAP DURING CRIT PER 2668.1  
MINIMUM NUMBER OF EQUIP. COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
3	1	2668	0.02315	0.0002	0.0461	0.0	0 0 2 0 0 0 0 1 0
0	0	2	0	0	0	0	
1	1	1	1	1	1	1	

CONFIGURATIONS THIS YEAR 1  
CONFIGURATIONS THROUGH THIS YEAR 3

\* \* \* \* \* END OF YEAR 1982 \* \* \* \* \*

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INDEX READ 2
INDEX READ 1
CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1983
MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 0 0 0 0 1 0
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000
OPTION FOR MODE OF GENERATION (LOP,NI) 1
MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000
FIXED CAPACITY--OTHER, HYDRG, EHYD, PSTGE
1535 324 38 0
1585 233 44 0
CRITICAL PERIOD IS 2 CAPACITY RANGE IS 2669 4003
INST. CAP DURING CRIT PER 3268.1
MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

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STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED CONFIGURATION										
4	1	3268	0.01293	0.0002	0.0257	0.0	0.0	0	0	4	0	0	0	0	1	0
0	0	4	0	1	0	1	0	1	1	1	1	1	1	1	1	1
CONFIGURATIONS THIS YEAR																
CONFIGURATIONS THROUGH THIS YEAR																
***** END OF YEAR 1983 *****																



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INDEX READ      2
INDEX READ      1
CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1984
MINIMUM REQUIRED OF EACH ALTERNATIVE      0  0  4  0  0  0  2  0
MAXIMUM ADDITIONAL EACH ALTERNATIVE      0  0  0  0  0  0  0  0
RESERVE RANGE PERMITTED CRITICAL PER.    0.0  50.0000
OPTION FOR MODE OF GENERATION (TOP IN)    1
MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000
FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE
1585 324 38 0
1585 233 44 0
CRITICAL PERIOD IS 2 CAPACITY RANGE IS 3129 4693
INST. CAP DURING CRIT PER 3700.3
MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE IC  CAP  LOLP  SEASONAL LOLP  ACCEPTED CONFIGURATION
5 1 3700 0.01562 0.0001 0.0311 0.0 0.0 0 0 4 0 0 0 0 2 0
0 0 4 0 0 0 0 2 0
1 1 1 1 1 1 1 1 1
CONFIGURATIONS THIS YEAR 1
CONFIGURATIONS THROUGH THIS YEAR 5
* * * * * END OF YEAR 1984 * * * * *

```

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1986  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 1 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 C 0 C 0 C 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (LOPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 4290 6435  
 INST. CAP DURING CRIT PER 5380.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP			ACCEPTED CONFIGURATION									
7	1	5380	0.01907	0.0023	0.0359	0.0	0.0	1	0	4	1	0	0	0	2	2
1	0	4	1	0	0	0	2	2								
1	1	1	1	1	1	1	1	1								
CONFIGURATIONS THIS YEAR 1																
CONFIGURATIONS THROUGH THIS YEAR 7																
* * * * * END OF YEAR 1986 * * * * *																

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1985  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 1 0 0 0 2 1  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (LOPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.0000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.0000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1565 324 38 0  
 1565 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 3666 5499  
 INST. CAP DURING CRIT PER 4540.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
6	1	4540	0.01621	0.0011	0.0313	0.0	0 0 4 1 0 0 0 2 1
0	0	4	1	0	1	1	
0	1	1	1	1	1	1	
CONFIGURATIONS THIS YEAR							1
CONFIGURATIONS THROUGH THIS YEAR							6
* * * * * END OF YEAR 1985 * * * * *							

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1987  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 2 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (LOPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, FHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 5017 7525  
 INST. CAP DURING CRIT PER 5980.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP			ACCEPTED CONFIGURATION									
8	1	5980	0.07653	0.0155	0.1375	0.0	0.0	1	0	4	2	0	0	0	2	2
1	0	4	2	0	1	2	2									

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 8  
 \* \* \* \* \* END OF YEAR 1987 \* \* \* \* \*

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INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1988  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 5 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, PSTGE  
 1585 324 38 0  
 1565 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 5863 8794  
 INST. CAP DURING CRIT PER 7780.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED CONFIGURATION
9	1	7780	0.01136	0.0021	0.0206	0.0 0.0 1 0 4 5 0 0 0 2 2
1	0	4	5	0	0	0 2 2
1	1	1	1	1	1	1

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 9  
 \* \* \* \* \* END OF YEAR 1988 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1989  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 7 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1565 324 28 0  
 1565 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 6845 10267  
 INST. CAP DURING CRIT PER 8980.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LPL	SEASONAL LPL	ACCEPTED CONFIGURATION
10	1	8980	0.02142	0.0043 0.0385 0.0	0.0 1 0 4 7 0 0 0 2 2
1	0	4	7	0 0 2 2	
1	1	1	1	1 1 1	
CONFIGURATIONS THIS YEAR					
CONFIGURATIONS THROUGH THIS YEAR 10					
* * * * * END OF YEAR 1989 * * * * *					

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1990  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 0 4 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 3 0 0 7 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 0 50.0000  
 OPTION FOR MODE OF GENERATION (LOPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY - OTHER, HYDRO, EHYD, PSTGE  
 1565 324 38 0  
 1565 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 7985 11977  
 INST. CAP DURING CRIT PER 9820.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION
11	1	9820	0.05163	0.0214 0.0819 0.0 0.0 2 0 4 7 0 0 0 2 3
2	0	4	7	0 0 0 2 3
1	1	1	1	1 1 1

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 11  
 \* \* \* \* \* END OF YEAR 1990 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1991  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 2 4 7 0 0 0 0 0 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0,0 50.0000  
 OPTION FOR MODE OF GENERATION (TOPIN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY - OTHER, HYDRO, FHYD, PSTGE  
 1585 324 0  
 1585 283 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 9307 13960  
 INST. CAP DURING CRIT PER 11820.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL LOLP			ACCEPTED CONFIGURATION									
12	1	11820	0.05676	0.0256	0.0880	0.0	0.0	2	2	4	7	0	0	0	2	3
2	2	4	7	0	0	3	2	3								
1	1	1	1	1	1	1	1									
CONFIGURATIONS THIS YEAR																
CONFIGURATIONS THROUGH THIS YEAR 12																
* * * * * END OF YEAR 1991 * * * * *																



INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1992  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 4 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (TOP IN)  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1565 324 38 0  
 1565 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 10837 16255  
 INST. CAP DURING CRIT PER 13820.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
13	1	13820	0.07103	0.0337	0.1084	0.0	0.0 2 4 4 7 0 0 0 2 3
2	4	4	7	0	0	0	2 3
1	1	1	1	1	1	1	1
CONFIGURATIONS THIS YEAR							
CONFIGURATIONS THROUGH THIS YEAR 13							
* * * * * END OF YEAR 1992 * * * * *							

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1993  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 7 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 28 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 12609 18913  
 INST. CAP DURING CRIT PER 16823.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL LOLP		ACCEPTED CONFIGURATION										
14	1	16820	0.33290	0.0151	0.0507	0.0	0.0	2	7	4	7	0	0	0	2	3
2	7	4	7	0	0	0	0	2	7	4	7	0	0	0	2	3
1	1	1	1	1	1	1	1									

CONFIGURATIONS THIS YEAR 14  
 CONFIGURATIONS THROUGH THIS YEAR 14  
 \* \* \* \* \* END OF YEAR 1993 \* \* \* \* \*

INDEX READ 2  
INDEX READ 1  
CONDITIONS GOVERNING ALTERNATIVE GENERATION YEAR 1994  
MINIMUM REQUIRED OF EACH ALTERNATIVE 2 9 4 7 0 0 0 2 3  
MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
OPTION FOR MODE OF GENERATION (IOPIN) 1  
MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
1585 324 30 0  
1585 283 44 0  
CRITICAL PERIOD IS 2 CAPACITY RANGE IS 14658 21987  
INST. CAP DURING CRIT PER 18820.3  
MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
15	1	18820	0.07498	0.0358	0.1141	0.0	0.0
2	9	4	7	0	0	2	9
1	1	1	1	1	1	4	7
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
2	3	0	0	0	0	2	3

CONFIGURATIONS THIS YEAR 1  
CONFIGURATIONS THROUGH THIS YEAR 15  
\* \* \* \* \* END OF YEAR 1994 \* \* \* \* \*

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LIST OF > OF CONFIGURATIONS PER YEAR.

1980	
1981	
1982	
1983	
1984	
1985	
1986	
1987	
1988	
1989	
1990	
1991	
1992	
1993	
1994	
TOTAL	15

THIS IS THE FIRST MERSIM RUN AND SIMULOLD FILE

WILL NOT BE CONSIDERED  
 FILE 10(FIXED SYS) SUCCESSFULLY OPENED  
 BASE YEAR FOR PRES.WORTH CALC.IS 1980  
 BASE YEAR FOR ESCALATION CALC.IS 1980

FILE 11(VARIABLES) SUCCESSFULLY OPENED  
 FILE 12(LOADS) SUCCESSFULLY OPENED  
 FILE 13(CONFIGURATIONS) SUCCESSFULLY OPENED

LOADING ORDER INPUT DATA:

GIVEN LOADING ORDER IS CONSTANT, READ FROM CARDS AND ON A PLANT BASIS

NORDER	9	8	12	11	10	1009
	1008	13	3	4	1012	1011
	1010	1013	1003	1004	5	14
	6	1005	1014	1006	7	

\*\*\*\*\* LOADING ORDER \*\*\*\*\*

N10H (BASE)	N600 (BASE)	C10H (BASE)	C600 (BASE)	C300 (BASE)	N10H (PEAK)
N600 (PEAK)	O600 (BASE)	F01H (BASE)	F050 (BASE)	C10H (PEAK)	C600 (PEAK)
C300 (PEAK)	O600 (PEAK)	F01H (PEAK)	F050 (PEAK)	FD25 (BASE)	GT2H (BASE)
FGTH (BASE)	FD25 (PEAK)	GT2H (PEAK)	FGTH (PEAK)	FPST (BASE)	

\*\*\*\*\*

SHADOW EXCHANGE RATE--LOCAL VS FOREIGN EXCHANGE  
 USED HERE TO INFLUENCE PUMPED STORAGE OPERATION ONLY 1.2000  
 TOPT = 0  
 RATE OF INTEREST APPLIED TO ALL DOMESTIC OPER COST = 0.0  
 RATE OF INTEREST APPLIED TO ALL FOREIGN OPER COST = 0.0  
 \*\*\*\*\* PERMITTED NUMBER FOR HYDRO IS 1. INPUT OF 3 WILL BE CHANGED TO 1  
 NUMBER OF HYDRO CONDITIONS CONSIDERED 1  
 NUMBER OF FOURIER COEFF. USED IN THIS SIMULATION 20

LOADING ORDER INPUT DATA:  
 CALCULATION OF LOADING ORDER ON A UNIT BASIS NOT PERMITTED IF A PUMPED STORAGE PLANT EXISTS  
 OPTION 1 BASE RESET TO 0 BY PROGRAM  
 LOADING ORDER CALCULATED ON A PLANT BASIS

CALCULATED LOADING ORDER BASED ON THE FOLLOWING SEQUENCE, READ FROM CARDS

NORDER	9	8	12	11	10	13
	3	4	5	14	6	7
NUMBER OF HYDRO CONDITIONS CONSIDERED			1			
LOCAL & FOREIGN INTEREST RATES ON OPERATION						
LOCAL	0.0	0.0	0.0	0.0	0.0	0.0
FORGN	0.0	0.0	0.0	0.0	0.0	0.0
LOCAL & FOREIGN ESCALATION RATES ON OPERATION						
LOCAL	1.00	1.00	1.00	1.00	1.00	1.00
FORGN	1.00	1.00	1.00	1.00	1.00	1.00

LOADING ORDER INPUT DATA:  
 LOADING ORDER CALCULATED ON A PLANT BASIS

LOADING ORDER INPUT DATA:  
 LOADING ORDER CALCULATED ON A PLANT BASIS

SEQU.	RELIABILITY	DAYS/YR	CONFIGURATIONS FOR YEAR ****													
1	0.39732F-03	0.14502	-1	0	0	0	0	0	0	0	0	0	0	0	1980	****
2	0.15557E-06	0.00006	-1	0	0	1	0	0	0	0	0	0	0	0	1981	****
3	0.23146E-03	0.08448	-1	0	2	0	0	0	0	0	1	0	0	1982	****	
4	0.12930E-03	0.04719	-1	0	4	0	0	0	0	0	1	0	0	1983	****	
5	0.15621F-03	0.05702	-1	0	4	0	0	0	0	0	2	0	0	1984	****	
6	0.16212E-03	0.05917	-1	0	4	1	0	0	0	0	2	1	0	1985	****	
7	0.19072E-03	0.06961	-1	1	4	1	0	0	0	0	2	2	0	1986	****	
8	0.76529E-03	0.27933	-1	1	0	4	2	0	0	0	2	2	0	1987	****	
9	0.11362E-03	0.04147	-1	1	0	4	5	0	0	0	2	2	0	1988	****	
10	0.21421E-03	0.07819	-1	1	0	4	7	0	0	0	2	2	0	1989	****	
11	0.51625E-03	0.18843	-1	2	0	4	7	0	0	0	2	3	0	1990	****	
12	0.56762E-03	0.20718	-1	2	2	4	7	0	0	0	2	3	0	1991	****	
13	0.71029E-03	0.25926	-1	2	4	4	7	0	0	0	2	3	0	1992	****	
14	0.32899E-03	0.12008	-1	2	7	4	7	0	0	0	2	3	0	1993	****	
15	0.74981F-03	0.27368	-1	2	9	4	7	0	0	0	2	3	0	1994	****	
			-1											1995	****	

7	1	2	7	15	2	7	1980
STATE	0	0	0	0	0	0	0
STATE	0	1	0	0	0	0	0
STATE	0	2	0	0	0	0	0
STATE	0	4	0	0	0	0	0
STATE	0	4	0	0	0	0	0
STATE	0	4	1	0	0	0	0
STATE	1	4	1	0	0	0	0
STATE	1	4	2	0	0	0	0
STATE	1	4	5	0	0	0	0
STATE	1	4	7	0	0	0	0
STATE	2	4	7	0	0	0	0
STATE	2	4	7	0	0	0	0
STATE	2	4	7	0	0	0	0
STATE	2	4	7	0	0	0	0
STATE	2	4	7	0	0	0	0
STATE	2	4	7	0	0	0	0

```

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BASE YEAR FOR PRFS. WORTH CALC. IS 1980
BASE YEAR FOR ESCALATION CALC IS 1980
DURATION OF STUDY IS 15 YEARS
TOPW = 0 NUM1 = 1
LAST YEAR THAT FOLLOWING RATES ARE TO BE USED. IYRL = 1994
(IIF IYRL = LAST YEAR OF STUDY, PROGRAM INCREASES IYRL BY CNEI)
RATE OF INTEREST APPLIED TO ALL LOCAL CAPITAL = 8.00
RATE OF INTEREST APPLIED TO ALL FOREIGN CAPITAL = 8.00
INDEX = 15
RATE OF INTEREST APPLIED TO ALL FOREIGN OPER COST = 8.00
INDEX = 14
RATE OF INTEREST APPLIED TO ALL DOMESTIC OPER COST = 8.00
INDEX = 3
SHADOW EXCHANGE RATE--LOCAL VS FOR. EX. 1.2000
INDEX = 17
LOCAL & FOREIGN MULTIPLYER ON COST OF OPERATION
LOCAL 1.00 1.00 1.00 1.00 1.10 1.00 1.00 1.00
FOREIGN 1.00 1.00 1.00 1.00 1.10 1.00 1.00 1.00
INDEX = 16
USE SINKING FUND DEPRECIATION FOR SALVAGE VALUE
INDEX = 2
OPLANT CAPITAL COST FUEL INV. PLANT LIFE
LOCAL FOREIGN LOCAL FOREIGN YRS
OH500 134.0 566.0 0.0 86.0 30.
OH100 108.0 480.0 0.0 79.0 30.
OC300 65.0 327.0 0.0 0.0 30.
OC600 51.0 261.0 0.0 0.0 30.
OC1000 43.0 227.0 0.0 0.0 30.
OC600 47.0 232.0 0.0 0.0 30.
OSTCH 33.0 132.0 0.0 0.0 20.
OVHYD 0.0 0.0 0.0 0.0 50.
3HYDRO PROJECT CAPITAL COSTS.
OVHYD 387.0 258.0
OVHYD 231.0 154.0
OVHYD 513.0 342.0
OVHYD 945.0 630.0
OVPS1 0.0 0.0 0.0 0.0 50.
PUMPED STORAGE PROJECT CAPITAL COSTS
OVPS1 364.0 78.0
OVPS1 91.0 78.0
OVPS1 91.0 78.0
OVPS1 1000.0 100.0
OVPS1 270.0 100.0
INDEX = 12
CRITICAL LOSS OF LOAD PROBABILITY IS 1.0000
INDEX = 13
NUMBER OF SOLUTIONS REQUESTED IS 5
INDEX = 18
OPTION FOR SUMMARY LIST = 0 ( IATA VERSION )
INDEX = 6
UPPER LIMIT ON NUMBER OF UNITS THAT CAN BE ADDED FOR EACH CANDIDATE IN EACH YEAR
INDEX = 19
LEVELIZED FIXED CHARGE RATES =
INDEX = 1
OBJECTIVE FUNCTION STATE 2 TO 2
184771
INDEX = 1

```

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INDEX = 1  
 OBJECTIVE FUNCTION STATE 4 TO 4  
 926130.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 5 TO 5  
 1306372.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 6 TO 6  
 1597599.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 7 TO 7  
 1965116.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 8 TO 8  
 2406457.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 9 TO 9  
 2715788.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 10 TO 10  
 3125289.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 11 TO 11  
 3455328.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 12 TO 12  
 3831580.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 13 TO 13  
 4286571.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 14 TO 14  
 4671695.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 15 TO 15  
 5030395.

INDEX = 1  
 OBJECTIVE FUNCTION STATE 16 TO 16  
 5296329.

SOLUTION #	CONFIGURATION	VARIABLE	ALTERNATIVES BY YEAR	INDEX
			FOR YEAR 1994	16
N600	0	2	600	1200
N13H	0	9	1000	9000
C300	3	4	300	1200
C600	3	7	600	4200
C10H	3	0	1000	0
G600	2	0	600	0
C724	1	0	192	0
V-VO	5	2	0	0
VPST	6	3	0	0

PWCONCST PWOPCST PHSALVAL OBJTVFTN PLOL

CONFIGURATION FOR YEAR 1993 INDEX				15
N600	0	2	600	1200
N100	0	4	1000	7000
C300	3	7	300	1200
C600	0	7	600	4200
C100	3	0	1000	0
O600	2	0	600	0
GT2H	1	2	192	0
VHYD	6	3	0	0
VPST	6	3	0	0
PWCONCST 859089 PWOPCST 224263 PWSALVAL 724622 OBJTVFTN 5090395 PLOL 0.0003				
CONFIGURATION FOR YEAR 1992 INDEX				14
N600	0	2	600	1200
N100	0	4	1000	4000
C300	3	7	300	1200
C600	0	7	600	4200
C100	3	0	1000	0
O600	2	0	600	0
GT2H	1	2	192	0
VHYD	6	3	0	0
VPST	6	3	0	0
PWCONCST 618523 PWOPCST 245241 PWSALVAL 478661 OBJTVFTN 4671694 PLOL 0.0007				
CONFIGURATION FOR YEAR 1991 INDEX				13
N600	0	2	600	1200
N100	0	4	1000	2000
C300	3	7	300	1200
C600	0	7	600	4200
C100	3	0	1000	0
O600	2	0	600	0
GT2H	1	2	192	0
VHYD	6	3	0	0
VPST	6	3	0	0
PWCONCST 668027 PWOPCST 260829 PWSALVAL 473865 OBJTVFTN 4286570 PLOL 0.0006				
CONFIGURATION FOR YEAR 1990 INDEX				12
N600	0	2	600	1200
N100	0	4	1000	0
C300	3	7	300	1200
C600	0	7	600	4200
C100	3	0	1000	0
O600	2	0	600	0
GT2H	1	2	192	0
VHYD	6	3	0	0
VPST	6	3	0	0
PWCONCST 281873 PWOPCST 277873 PWSALVAL 183494 OBJTVFTN 3831579 PLOL 0.0005				
CONFIGURATION FOR YEAR 1989 INDEX				11
N600	0	1	600	600
N100	0	4	1000	0
C300	3	7	300	1200
C600	0	7	600	4200
C100	3	0	1000	0
O600	2	0	600	0
GT2H	1	2	192	0
VHYD	6	2	0	0
VPST	6	2	0	0
PWCONCST 218628 PWOPCST 240261 PWSALVAL 128851 OBJTVFTN 3455328 PLOL 0.0002				
CONFIGURATION FOR YEAR 1988 INDEX				10
N600	0	1	600	600
N100	0	4	1000	0
C300	3	7	300	1200
C600	0	7	600	3000
C100	3	0	1000	0
O600	2	0	600	0

CONFIGURATION FOR YEAR 1987 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLDL
N600	0	0	600	600	354178	245724	193381	3125288	0.0001
N10H	0	0	1000	0					
C300	0	0	300	1200					
C600	0	0	600	1200					
C10H	0	0	1000	0					
O600	0	0	600	0					
GT2H	0	0	192	0					
VHYD	6	2	0	0					
VPST	6	2	0	0					
CONFIGURATION FOR YEAR 1986 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLDL
N600	0	0	600	600	127504	245245	62418	2715788	0.0008
N10H	0	0	1000	0					
C300	0	0	300	1200					
C600	0	0	600	600					
C10H	0	0	1000	0					
O600	0	0	600	0					
GT2H	0	0	192	0					
VHYD	6	2	0	0					
VPST	6	2	0	0					
CONFIGURATION FOR YEAR 1985 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLDL
N600	0	0	600	0	383485	231933	174078	2406456	0.0002
N10H	0	0	1000	0					
C300	0	0	300	1200					
C600	0	0	600	600					
C10H	0	0	1000	0					
O600	0	0	600	0					
GT2H	0	0	192	0					
VHYD	6	2	0	0					
VPST	6	2	0	0					
CONFIGURATION FOR YEAR 1984 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLDL
N600	0	0	600	0	223465	237876	93824	1965116	0.0002
N10H	0	0	1000	0					
C300	0	0	300	1200					
C600	0	0	600	0					
C10H	0	0	1000	0					
O600	0	0	600	0					
GT2H	0	0	192	0					
VHYD	6	2	0	0					
VPST	6	2	0	0					
CONFIGURATION FOR YEAR 1983 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLDL
N600	0	0	600	0	186653	228982	44418	1597599	0.0002
N10H	0	0	1000	0					
C300	0	0	300	1200					
C600	0	0	600	0					
C10H	0	0	1000	0					
O600	0	0	600	0					
GT2H	0	0	192	0					
VHYD	6	1	0	0					
VPST	6	1	0	0					
CONFIGURATION FOR YEAR 1982 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLDL
N600	0	0	600	0	217859	234405	72021	1306372	0.0001
N10H	0	0	1000	0					
C300	0	0	300	0					

C10H 0000  
 0600 1000  
 012H 6600  
 VHYD 1920  
 VPST 0000

PWCONCST 256795 PWOPCST 227010 PWSALVAL 84298 OBJTVFTN 926130 PLOL 0.0002

CONFIGURATION FOR YEAR 1981 INDEX 3

N600 0000  
 N10H 0001  
 C300 0000  
 C600 0000  
 C10H 0000  
 0600 0000  
 012H 0000  
 VHYD 0000  
 VPST 0000

PWCONCST 127055 PWOPCST 248000 PWSALVAL 34010 OBJTVFTN 526622 PLOL 0.0000

CONFIGURATION FOR YEAR 1980 INDEX 2

N600 0000  
 N10H 0000  
 C300 0000  
 C600 0000  
 C10H 0000  
 0600 0000  
 012H 0000  
 VHYD 0000  
 VPST 0000

PWCONCST 0 PWOPCST 184770 PWSALVAL 7 OBJTVFTN 184770 PLOL 0.0004

1980 0 0 0 0 0 0 0 0  
 1981 0 1 0 0 0 0 0 0  
 1982 0 2 0 0 0 0 1 0  
 1983 0 4 0 0 0 0 1 0  
 1984 0 4 0 0 0 0 2 0  
 1985 0 4 1 0 0 0 2 1  
 1986 1 4 1 0 0 0 2 2  
 1987 1 4 2 0 0 0 2 2  
 1988 1 4 5 0 0 0 2 2  
 1989 1 4 7 0 0 0 2 2  
 1990 2 4 7 0 0 0 2 3  
 1991 2 4 7 0 0 0 2 3  
 1992 2 4 7 0 0 0 2 3  
 1993 2 4 7 0 0 0 2 3  
 1994 2 4 7 0 0 0 2 3

ALL POSSIBLE PATHS TRACED

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NUMBER OF ALTERNATIVES FROM WHICH TO CHOOSE IS 9  
 NUMBER OF PERIODS IN YEAR IS 2  
 NUMBER OF FOURIER COEFF. IS 50

NO. OF SETS	NAME	MIN. LOAD MW	CAP. CITY MW	BASE LOAD RATE	AVGE INCR HEAT RATE	FUEL COSTS CENTS/MILLION		TYPE	I C T	FRCD OUT-AGE RATE	DAYS SCHL MAIN	MAIN CLAS	ENRGY GWH	D?M (FIX)	D?M (VAR)	
						DMSTC	FORGN									
FIXED SYSTEM																
1	FHYD	1	159	324	0.	0.	0.0	0.0	5	0	0.0	0	0	2051.	0.300	0.0
2	FEMH	1	44	44	2252.	2262.	10.00	980.00	-1	99	0.0	0	0	0.	0.300	0.0
3	FOLH	5	34	100	2490.	2193.	10.00	700.00	2	10	3.00	28	100	0.	2.300	0.0
4	F050	8	25	50	2618.	2326.	10.00	700.00	2	10	3.00	28	50	0.	3.000	0.0
5	FD23	3	20	25	2175.	1833.	10.00	980.00	4	20	1.00	14	25	0.	0.850	0.0
6	FGTH	5	29	97	6322.	2262.	10.00	980.00	1	72	2.50	14	50	0.	0.520	0.0
7	FPST	0	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.	0.325	0.0
VARIABLE SYSTEM																
8	H500	0	400	600	2588.	2363.	0.0	142.00	0	5	12.00	42	600	0.	0.990	0.0
9	N10H	0	667	1000	2566.	2361.	0.0	134.00	0	5	16.00	42	1000	0.	0.730	0.0
10	C300	0	100	300	2480.	2180.	450.00	0.0	3	10	7.00	35	300	0.	1.200	0.0
11	3600	0	200	600	2460.	2160.	450.00	0.0	3	10	12.00	42	600	0.	0.710	0.0
12	CTJH	0	334	1000	2440.	2140.	450.00	0.0	3	10	16.00	42	1000	0.	0.560	0.0
13	O600	0	200	600	2440.	2140.	10.00	700.00	2	10	10.00	42	600	0.	0.670	0.0
14	GT2H	0	58	192	6322.	2262.	10.00	980.00	1	73	1.25	14	50	0.	0.520	0.0
15	VHYD	4	0	0	0.	0.	0.0	0.0	5	0	0.0	0	0	0.	0.0	0.0
16	VPST	5	0	0	0.	0.	0.0	0.0	6	0	0.0	0	0	0.	0.325	0.0

POSITION OF HYDRO EMERG.H. PUMPF D STG  
 1 2 7

INDEX READ 7  
 INDEX READ 6  
 INDEX READ 5  
 INDEX READ 4  
 INDEX READ 3  
 INDEX READ 2  
 INDEX READ 1

CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1987  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000

OPTION FOR MODE OF GENERATION (IDPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000

FIXED CAPACITY--OTHER, HYDRO, ENHYD, STGE  
 1660 324 38 0  
 1663 263 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 1647 2470  
 INST. CAP DURING CRIT PER 1587.0  
 MINIMUM NUMBER OF FOURTER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED CONFIGURATION												
1	1	1987	0.00789	0.0072	0.0086	0.0	0.0	0	0	0	0	0	0	0	0	0	0	0

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 1  
 \* \* \* \* \* END OF YEAR 1980 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1981  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 1 0 0 0 0 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1660 324 38 0  
 1660 283 24 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 1936 2904  
 INST. CAP DURING CRIT PER 2287.0  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LCLP	SEASONAL LCLP	ACCEPTED CONFIGURATION												
2	1	2287	0.02512	0.0068	0.0434	0.0	0.0	0	0	1	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
CONFIGURATIONS THIS YEAR																	
CONFIGURATIONS THROUGH THIS YEAR																	
* * * * * END OF YEAR 1981 * * * * *																	

INDEX READ 2  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1982 0 0 0 0 0 0 0  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED EACH ALTERNATIVE 0 0 0 0 0 0 0  
 OPTION FOR MORE OF EACH ALTERNATIVE (OPTN) 0 0 50.0000  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT LAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00300 EQUIVALENT DAYS/YR = 365.300  
 FIXED CAPACITY 324  
 1585  
 283 44  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 2274 3411  
 INT. CAP DURING CRIT PER 2668.1  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
3	1	2668	0.03349	0.0077	0.0596	0.0	0 0 2 0 0 0 0 1 0
0	0	1	0	1	1	0	0 0 2 0 0 0 0 1 0
1	1	1	1	1	1	1	0 0 2 0 0 0 0 1 0
CONFIGURATIONS THIS YEAR 1							
CONFIGURATIONS THROUGH THIS YEAR 3							
* * * * * END OF YEAR 1982 * * * * *							



INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1983  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 0 0 0 1 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 2669 4003  
 INST. CAP DURING CRIT PER 3268.1  
 MINIMUM NUMBER OF EQUIP. COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION
4	1	3268	0.02177	0.0070	0.0365 0.0 0.0 0 0 4 0 0 0 0 1 0
C	0	4	0	0	0 0 1 0
1	1	1	1	1	1 1 1

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 4  
 \* \* \* \* \* END OF YEAR 1983 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1984  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 0 0 0 0 0 2 0  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (ICPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 28 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 3129 4693  
 INST. CAP DURING CRIT PER 3700.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	L0LP	SEASONAL L0LP			ACCEPTED CONFIGURATION									
5	1	3700	0.02411	0.0073	0.0410	0.0	0.0	0	0	4	0	0	0	0	2	0
0	0	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

CONFIGURATIONS THIS YEAR 1  
 CONFIGURATIONS THROUGH THIS YEAR 5  
 \* \* \* \* \* END OF YEAR 1984 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1985  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 0 0 4 1 0 0 0 2 1  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (IOPIN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 3666 5499  
 INST. CAP DURING CRIT PER 4540.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP.	LCLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
6	1	4540	0.02133	J.JJ51	J.JJ76	0.0	J.J J 0 4 1 0 0 0 2 1
0	0	4	1	0	0	2	1
CONFIGURATIONS THIS YEAR							
CONFIGURATIONS THROUGH THIS YEAR							
***** END OF YEAR 1985 *****							

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1986  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 1 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGF  
 1585 324 38 0  
 1585 283 44 J  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 4290 6435  
 INST. CAP DURING CRIT PER 5389.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION											
7	1	5380	0.02391	0.0062	0.0416	0.0	0.0	1	0	4	1	0	0	0	2	2
1	0	4	1	0	0	2	2	1	1	1	1	1	1	1	1	1

CONFIGURATIONS THIS YEAR  
 CONFIGURATIONS THROUGH THIS YEAR  
 \* \* \* \* \* END OF YEAR 1986 \* \* \* \* \*

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1987  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 2 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0,0 50.0000  
 OPTION FOR MODE OF GENERATION (LOPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, LYCRD, EHYD, PSTGE  
 1585 324 34 0  
 1585 323 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 5017 7525  
 INST. CAP DURING CRIT PER 5980.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP		ACCEPTED CONFIGURATION										
0	1	5980	0.08548	0.2256	0.1503	0.0	0.0	1	0	4	2	0	0	0	2	2
1	0	4	2	0	0	0	0	1	0	4	2	0	0	0	2	2
1	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
CONFIGURATIONS THIS YEAR																
CONFIGURATIONS THROUGH THIS YEAR																
* * * * * END OF YEAR 1987 * * * * *																

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1988  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 2 5 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGF  
 1585 374 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 5863 8794  
 INST. CAP DURING CRIT PER 7783.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	LOLP	SEASONAL LOLP		ACCEPTED CONFIGURATION										
9	1	7780	0.01581	0.0055	0.0261	0.0	0.0	1	0	4	5	0	0	0	2	2
1	0	4	5	0	0	0	2	2								
1	1	1	1	1	1	1	1	1								
CONFIGURATIONS THIS YEAR 1																
CONFIGURATIONS THROUGH THIS YEAR 9																
* * * * * END OF YEAR 1988 * * * * *																

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1989  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 1 0 4 7 0 0 0 2 2  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 3 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTM) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 6845 13267  
 INST. CAP DURING CRIT PER 8990.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 5

STATE	IC	CAP	L0LP	SEASONAL L0LP	ACCEPTED CONFIGURATION
10	1	8980	0.01975	0.3365	0.0330 0.0 3.0 1 0 4 7 0 0 0 2 2
1	0	4	7	0	0 2 2
1	1	1	1	1	1
CONFIGURATIONS THIS YEAR					1
CONFIGURATIONS THROUGH THIS YEAR					10
* * * * *					END OF YEAR 1989 * * * * *

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1990  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 0 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (IOPIN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 7985 11977  
 INST. CAP DURING CRIT PER 5820.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL LOLP			ACCEPTED CONFIGURATION										
11	1	5820	0.07559	0.0417	0.1095	0.0	0.0	2	0	4	7	0	0	0	2	3	
2	0	4	7	0	0	0	2	3									
1	1	1	1	1	1	1	1	1									
CONFIGURATIONS THIS YEAR																	
CONFIGURATIONS THROUGH THIS YEAR -11																	
* * * * * END OF YEAR 1990 * * * * *																	



INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1991  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 2 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER. 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 9307 13960  
 INST. CAP DURING CRIT PER 11820.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION											
12	1	11820	0.0794	0.0466	0.1124	0.0	0.0	2	2	4	7	0	0	0	2	3
2	2	4	7	0	0	0	2	3								
1	1	1	1	1	1	1	1	1								
CONFIGURATIONS THIS YEAR																
CONFIGURATIONS THROUGH THIS YEAR 12																
* * * * * END OF YEAR 1991 * * * * *																

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1992  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 4 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (OPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.300  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 10837 16255  
 INST. CAP DURING CRIT PER 13820.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL LOLP	ACCEPTED CONFIGURATION				
13	1	13820	0.09400	0.0547 0.1333 0.0 0.0	2 4 4 7 0 0 0 2 3				
2	4	4	7	0	0	0	2	3	
1	1	1	1	1	1				
CONFIGURATIONS THIS YEAR									
CONFIGURATIONS THROUGH THIS YEAR 13									
***** END OF YEAR 1992 *****									

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1993  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 7 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (TOPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, FHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 12609 18913  
 INST. CAP DURING CRIT PER 16820.3  
 MINIMUM NUMBER OF FOURIER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL	LOLP	ACCEPTED	CONFIGURATION
14	1	16820	0.05406	0.0350	0.0731	0.0	0.0
2	7	4	7	0	0	2	7 4 7 0 0 0 2 3
1	1	1	1	1	1	1	
CONFIGURATIONS THIS YEAR							
CONFIGURATIONS THROUGH THIS YEAR 14							
* * * * * END OF YEAR 1993 * * * * *							

INDEX READ 2  
 INDEX READ 1  
 CONDITIONS GOVERNING ALTERNATIVE GENERATION, YEAR 1994  
 MINIMUM REQUIRED OF EACH ALTERNATIVE 2 9 4 7 0 0 0 2 3  
 MAXIMUM ADDITIONAL EACH ALTERNATIVE 0 0 0 0 0 0 0 0 0  
 RESERVE RANGE PERMITTED CRITICAL PER 0.0 50.0000  
 OPTION FOR MODE OF GENERATION (TOPTN) 1  
 MAXIMUM PERIOD LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 182.500  
 ANNUAL LOSS OF LOAD PROBABILITY = 1.00000 EQUIVALENT DAYS/YR = 365.000  
 FIXED CAPACITY--OTHER, HYDRO, EHYD, PSTGE  
 1585 324 38 0  
 1585 283 44 0  
 CRITICAL PERIOD IS 2 CAPACITY RANGE IS 14658 21587  
 INST. CAP DURING CRIT PER 18820.3  
 MINIMUM NUMBER OF FOURTER COEFF. CORRESPONDING TO MAXIMUM RESERVE MARGIN IN CRIT PER IS 6

STATE	IC	CAP	LOLP	SEASONAL LOLP			ACCEPTED CONFIGURATION									
15	1	18820	0.09894	0.0572	0.1407	0.0	0.0	2	9	4	7	0	0	0	2	3
2	9	4	7	0	0	0	2	3								
1	1	1	1	1	1	1	1									
CONFIGURATIONS THIS YEAR																
CONFIGURATIONS THROUGH THIS YEAR 15																
* * * * * END OF YEAR 1994 * * * * *																

LIST OF > OF CONFIGURATIONS PER YEAR

1980	
1981	
1982	
1983	
1984	
1985	
1986	
1987	
1988	
1989	
1990	
1991	
1992	
1993	
1994	
TOTAL	15

THIS IS THE FIRST MERSIM RUN AND SIMULOLD FILE  
 WILL NOT BE CONSIDERED  
 FILE 10(FIXED SYS)SUCCESSFULLY OPENED  
 BASE YEAR FOR PRES.WORTH CALC.IS 1980  
 BASE YEAR FOR ESCALATION CALC.IS 1980

FILE 11(VAR.ALTS) SUCCESSFULLY OPENED  
 FILE 12(LOADS)SUCCESSFULLY OPENED  
 FILE 13(CONFIGURATIONS) SUCCESSFULLY OPENED

LOADING ORDER INPUT DATA:

GIVEN LOADING ORDER IS CONSTANT, READ FROM CARDS AND ON A PLANT BASIS

NORORDER	9	8	12	11	10	1009
	1008	13	3	4	1012	1311
	1010	1013	1003	1004	5	14
	6	1005	1014	1006	7	

\*\*\*\*\* LOADING ORDER \*\*\*\*\*

N10H (BASE)	N600 (BASE)	C10H (BASE)	3600 (BASE)	C300 (BASE)	N10H (PEAK)
N600 (PEAK)	C600 (BASE)	F01H (BASE)	F050 (BASE)	C10H (PEAK)	3600 (PEAK)
C300 (PEAK)	F060J (PEAK)	F01H (PEAK)	F050 (PEAK)	FD25 (BASE)	GT2H (BASE)
FGTH (BASE)	FD25 (PEAK)	GT2H (PEAK)	FGTH (PEAK)	FPST (BASE)	

\*\*\*\*\*

SHADOW EXCHANGE RATE--LOCAL VS FOREIGN EXCHANGE  
 USED HERE TO INFLUENCE PUMPED STORAGE OPERATION ONLY 1.2000  
 IOPT = 0  
 RATE OF INTEREST APPLIED TO ALL DOMESTIC OPER COST = 0.0  
 RATE OF INTEREST APPLIED TO ALL FOREIGN OPER COST = 0.0  
 \*\*\*\*\* PERMITTED NUMBER FOR HYDIS IS 1. INPUT OF 3 WILL BE CHANGED TO 1  
 NUMBER OF HYDRO CONDITIONS CONSIDERED 1  
 NUMBER OF FOURIER COEFF. USED IN THIS SIMULATION 20

LOADING ORDER INPUT DATA:  
 CALCULATION OF LOADING ORDER ON A UNIT BASIS NOT PERMITTED IF A PUMPED STORAGE PLANT EXISTS  
 OPTION LBASE RESET TO 0 BY PROGRAM  
 LOADING ORDER CALCULATED ON A PLANT BASIS

CALCULATED LOADING ORDER BASED ON THE FOLLOWING SEQUENCE, READ FROM CARDS

NORORDER	9	8	12	11	10	13
	3	4	5	14	6	7
NUMBER OF HYDRO CONDITIONS CONSIDERED	1					
LOCAL & FOREIGN INTEREST RATES ON OPERATION						
LOCAL	0.0	0.0	0.0	0.0	0.0	0.0
FORGN	0.0	0.0	0.0	0.0	0.0	0.0
LOCAL & FOREIGN ESCALATION RATES ON OPERATION						
LOCAL	1.00	1.00	1.00	1.00	1.00	1.00
FORGN	1.00	1.00	1.00	1.00	1.00	1.00

LOADING ORDER INPUT DATA:  
 LOADING ORDER CALCULATED ON A PLANT BASIS

LOADING ORDER INPUT DATA:  
 LOADING ORDER CALCULATED ON A PLANT BASIS



	7	1	2	7	15	2	7	1	15	2	7	1	15	2	7
STATE	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
STATE	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
STATE	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0
STATE	0	0	4	0	0	0	0	0	0	0	0	0	0	0	0
STATE	0	0	4	0	0	0	0	0	0	0	0	0	0	0	0
STATE	0	0	4	1	0	0	0	0	0	0	0	0	0	0	0
STATE	1	0	4	1	0	0	0	0	0	0	0	0	0	0	0
STATE	1	0	4	2	0	0	0	0	0	0	0	0	0	0	0
STATE	1	0	4	5	0	0	0	0	0	0	0	0	0	0	0
STATE	1	0	4	7	0	0	0	0	0	0	0	0	0	0	0
STATE	2	0	4	7	0	0	0	0	0	0	0	0	0	0	0
STATE	2	0	4	7	0	0	0	0	0	0	0	0	0	0	0
STATE	2	0	4	7	0	0	0	0	0	0	0	0	0	0	0
STATE	2	0	4	7	0	0	0	0	0	0	0	0	0	0	0
STATE	2	0	4	7	0	0	0	0	0	0	0	0	0	0	0



102 9  
 BASE YEAR FOR PRES. WORTH CALC. IS 1980  
 BASE YEAR FOR ESCALATION CALC IS 1980  
 DURATION OF STUDY IS 15 YEARS  
 IOP# = 0 NUM1 = 1  
 LAST YEAR THAT FOLLOWING RATES ARE TO BE USED. IYFL = 1994  
 (IF IYFL = LAST YEAR OF STUDY, PROGRAM INCREASES IYFL BY ONE)  
 RATE OF INTEREST APPLIED TO ALL LOCAL CAPITAL = 8.00  
 RATE OF INTEREST APPLIED TO ALL FOREIGN CAPITAL = 8.00  
 INDEX = 15  
 RATE OF INTEREST APPLIED TO ALL FOREIGN OPER COST = 8.00  
 INDEX = 14  
 RATE OF INTEREST APPLIED TO ALL DOMESTIC OPER COST = 8.00  
 INDEX = 3

SHADOW EXCHANGE RATE--LOCAL VS FOR. EX. 1.2000  
 INDEX = 17  
 LOCAL & FOREIGN MULTIPLYER ON COST OF OPERATION  
 LOCAL 1.00 1.00 1.00 1.00 1.10 1.00 1.00 1.00  
 FOREIGN 1.00 1.00 1.00 1.00 1.10 1.00 1.00 1.00  
 INDEX = 16

USE SINKING FUND DEPRECIATION FOR SALVAGE VALUE  
 INDEX = 2

JPLANT	CAPITAL COST		FUEL INV.		PLANT LIFE YRS
	LOCAL	FOREIGN	LOCAL	FOREIGN	
QN600	134.0	586.0	0.0	86.0	30.
QN104	108.0	480.0	0.0	79.0	30.
QC300	65.0	327.0	0.0	0.0	30.
J3600	51.0	261.0	0.0	0.0	30.
QC10H	43.0	227.0	0.0	0.0	30.
J0600	47.0	239.0	0.0	0.0	30.
OGT2H	33.0	132.0	0.0	0.0	50.
QVHYD	0.0	0.0	0.0	0.0	50.
JHYDRO	PROJECT CAPITAL COSTS				
QVHYD	387.0	258.0			
QVHYD	331.0	154.0			
JVHYD	513.0	342.0			
QVHYD	945.0	630.0			
JVPSST	0.0	0.0	0.0	0.0	50.
JPUMPED STORAGE	PROJECT CAPITAL COSTS				
JVPSST	364.0	78.0			
JVPSST	91.0	78.0			
JVPSST	91.0	78.0			
JVPSST	1000.0	100.0			
JVPSST	270.0	100.0			

INDEX = 12  
 CRITICAL LOSS OF LOAD PROBABILITY IS 1.0000

INDEX = 13  
 NUMBER OF SOLUTIONS REQUESTED IS 5

INDEX = 18  
 OPTION FOR SUMMARY LIST = 0 ( JAEA VERSION )

INDEX = 6  
 UPPER LIMIT ON NUMBER OF UNITS THAT CAN BE ADDED FOR EACH CANDIDATE IN EACH YEAR  
 10 10 10 10 10 10 10 10

INDEX = 19  
 LEVELIZED FIXED CHARGE RATES =  
 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

INDEX = 1  
 OBJECTIVE FUNCTION STATE 2 TO 2

184771

926130  
 INDEX = 2  
 OBJECTIVE FUNCTION STATE 4 TO 4

926130  
 INDEX = 3  
 OBJECTIVE FUNCTION STATE 5 TO 5

926130  
 INDEX = 4  
 OBJECTIVE FUNCTION STATE 6 TO 6

926130  
 INDEX = 5  
 OBJECTIVE FUNCTION STATE 7 TO 7

926130  
 INDEX = 6  
 OBJECTIVE FUNCTION STATE 8 TO 8

926130  
 INDEX = 7  
 OBJECTIVE FUNCTION STATE 9 TO 9

926130  
 INDEX = 8  
 OBJECTIVE FUNCTION STATE 10 TO 10

926130  
 INDEX = 9  
 OBJECTIVE FUNCTION STATE 11 TO 11

926130  
 INDEX = 10  
 OBJECTIVE FUNCTION STATE 12 TO 12

926130  
 INDEX = 11  
 OBJECTIVE FUNCTION STATE 13 TO 13

926130  
 INDEX = 12  
 OBJECTIVE FUNCTION STATE 14 TO 14

926130  
 INDEX = 13  
 OBJECTIVE FUNCTION STATE 15 TO 15

926130  
 INDEX = 14  
 OBJECTIVE FUNCTION STATE 16 TO 16

926130  
 INDEX = 15

CONFIGURATION	YEAR	INDEX	INDEX
N600	0	2	600
N10H	0	9	1000
C300	3	4	300
C600	3	7	600
C10H	3	0	1000
D600	2	0	600
GTZ	1	0	100
VHYD	0	0	0

N600	0	2	600	1200
N10H	0	0	1000	4000
C300	3	4	300	1200
3600	3	7	600	4200
C10H	2	0	1000	0
O600	2	0	600	0
GT2H	5	2	192	0
VHYD	5	2	0	0
VPST	6	3	0	0

PWCONCST 859089 PWOPCST 224263 PWSALVAL 724652 OBJTVFTN 5030395 PLOL 0.0005

CONFIGURATION FOR YEAR 1992 INDEX 14				
N600	0	2	600	1200
N10H	0	0	1000	4000
C300	3	4	300	1200
3600	3	7	600	4200
C10H	2	0	1000	0
O600	2	0	600	0
GT2H	5	2	192	0
VHYD	5	2	0	0
VPST	6	3	0	0

PWCONCST 618543 PWOPCST 245241 PWSALVAL 478661 OBJTVFTN 4671695 PLOL 0.0009

CONFIGURATION FOR YEAR 1991 INDEX 13				
N600	0	2	600	1200
N10H	0	0	1000	4000
C300	3	4	300	1200
3600	3	7	600	4200
C10H	2	0	1000	0
O600	2	0	600	0
GT2H	5	2	192	0
VHYD	5	2	0	0
VPST	6	3	0	0

PWCONCST 668027 PWOPCST 260825 PWSALVAL 473865 OBJTVFTN 4286571 PLOL 0.0008

CONFIGURATION FOR YEAR 1990 INDEX 12				
N600	0	2	600	1200
N10H	0	0	1000	0
C300	3	4	300	1200
3600	3	7	600	4200
C10H	2	0	1000	0
O600	2	0	600	0
GT2H	5	2	192	0
VHYD	5	2	0	0
VPST	6	3	0	0

PWCONCST 281873 PWOPCST 277072 PWSALVAL 183494 OBJTVFTN 3831280 PLOL 0.0008

CONFIGURATION FOR YEAR 1989 INDEX 11				
N600	0	1	600	600
N10H	0	0	1000	0
C300	3	4	300	1200
3600	3	7	600	4200
C10H	2	0	1000	0
O600	2	0	600	0
GT2H	5	2	192	0
VHYD	5	2	0	0
VPST	6	2	0	0

PWCONCST 218628 PWOPCST 240261 PWSALVAL 128851 OBJTVFTN 3455328 PLOL 0.0002

CONFIGURATION FOR YEAR 1988 INDEX 10				
N600	0	1	600	600
N10H	0	0	1000	0
C300	3	4	300	1200
3600	3	7	600	4200
C10H	2	0	1000	0
O600	2	0	600	0

157

WHY 1	5	2	0	0						
VPST	6	2	0	0						
CONFIGURATION FOR YEAR 1987 INDEX					9	PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
						354178	242704	193381	3125289	0.0002
N600	0	1	600	600						
N10H	0	1	1000	0						
C300	0	4	300	1200						
3600	0	1	600	1700						
C10H	0	0	1000	0						
O600	0	0	600	0						
GT2H	0	0	192	0						
VHYD	0	0	0	0						
VPST	6	2	0	0						
CONFIGURATION FOR YEAR 1986 INDEX					8	PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
						127504	244245	62418	2715788	0.0009
N600	0	1	600	600						
N10H	0	1	1000	0						
C300	0	4	300	1200						
3600	0	1	600	600						
C10H	0	0	1000	0						
O600	0	0	600	0						
GT2H	0	0	192	0						
VHYD	0	0	0	0						
VPST	6	2	0	0						
CONFIGURATION FOR YEAR 1985 INDEX					7	PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
						383485	231933	174078	2406457	0.0002
N600	0	1	600	600						
N10H	0	1	1000	0						
C300	0	4	300	1200						
3600	0	1	600	600						
C10H	0	0	1000	0						
O600	0	0	600	0						
GT2H	0	0	192	0						
VHYD	0	0	0	0						
VPST	6	1	0	0						
CONFIGURATION FOR YEAR 1984 INDEX					6	PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
						223465	237876	93824	1965116	0.0002
N600	0	0	600	0						
N10H	0	0	1000	0						
C300	0	0	300	1200						
3600	0	0	600	0						
C10H	0	0	1000	0						
O600	0	0	600	0						
GT2H	0	0	192	0						
VHYD	0	0	0	0						
VPST	6	0	0	0						
CONFIGURATION FOR YEAR 1983 INDEX					5	PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
						106663	228982	44418	1597599	0.0002
N600	0	0	600	0						
N10H	0	0	1000	0						
C300	0	0	300	1200						
3600	0	0	600	0						
C10H	0	0	1000	0						
O600	0	0	600	0						
GT2H	0	0	192	0						
VHYD	0	0	0	0						
VPST	6	0	0	0						
CONFIGURATION FOR YEAR 1982 INDEX					4	PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
						217859	234405	7200		0.000
N600	0	0	600	0						
N10H	0	0	1000	0						

36.7	3	1	1	1	1	1	1	1
C10H	3	0	0	0	0	0	0	0
O600	3	0	0	0	0	0	0	0
GT2H	3	0	0	0	0	0	0	0
VHYD	3	0	0	0	0	0	0	0
VPST	3	0	0	0	0	0	0	0

PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
256796	227010	84298	926130	0.0003

CONFIGURATION FOR YEAR 1981 INDEX 3

N600	0	0	0	0	0	0	0	0
N10H	0	0	0	0	0	0	0	0
C300	0	0	0	0	0	0	0	0
3600	0	0	0	0	0	0	0	0
C10H	0	0	0	0	0	0	0	0
O600	0	0	0	0	0	0	0	0
GT2H	0	0	0	0	0	0	0	0
VHYD	0	0	0	0	0	0	0	0
VPST	0	0	0	0	0	0	0	0

PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
127055	248807	3401C	526622	0.2033

CONFIGURATION FOR YEAR 1980 INDEX 2

N600	0	0	0	0	0	0	0	0
N10H	0	0	0	0	0	0	0	0
C300	0	0	0	0	0	0	0	0
3600	0	0	0	0	0	0	0	0
C10H	0	0	0	0	0	0	0	0
O600	0	0	0	0	0	0	0	0
GT2H	0	0	0	0	0	0	0	0
VHYD	0	0	0	0	0	0	0	0
VPST	0	0	0	0	0	0	0	0

PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLOL
0	18477C	C	184770	0.0001

1980	1	0	0	0	0	0	0	0
1981	1	0	0	0	0	0	0	0
1982	2	0	0	0	0	1	0	0
1983	4	0	0	0	0	1	0	0
1984	4	0	0	0	0	2	0	0
1985	4	1	0	0	0	2	1	0
1986	4	1	0	0	0	2	2	0
1987	4	2	0	0	0	2	2	0
1988	4	5	0	0	0	2	2	0
1989	4	7	0	0	0	2	2	0
1990	4	7	0	0	0	2	3	0
1991	4	7	0	0	0	2	3	0
1992	4	7	0	0	0	2	3	0
1993	4	7	0	0	0	2	3	0
1994	4	7	0	0	0	2	3	0

ALL POSSIBLE PATHS TRACED

CONFIGURATION	FOR YEAR	INDEX	PWCONCST	PWOPCST	PWSALVAL	OBJTVFTN	PLQL
N600	1992	14	238812	224263	C	6365604	3.3333
N10H							
C300							
3600							
C10H							
O600							
GT2H							
VHYD							
VPST							
N600	1991	13	248487	242241	0	5402578	0.0007
N10H							
C300							
3600							
C10H							
O600							
GT2H							
VHYD							
VPST							
N600	1990	12	344908	260829	C	5408799	3.0006
N10H							
C300							
3600							
C10H							
O600							
GT2H							
VHYD							
VPST							
N600	1989	11	183187	277873	C	4803261	0.0005
N10H							
C300							
3600							
C10H							
O600							
GT2H							
VHYD							
VPST							
N600	1988	10	157551	240261	0	4342000	0.0002
N10H							
C300							
3600							
C10H							
O600							

CONFIGURATION FOR YEAR 1987 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTFTN	PLQL
VPST	6	2	C	0	287448	245704	0	3944187	0.0001
N600	0	1		600					
N10H	0	0		1000					
C300	3	4		300				1200	
3600	3	2		600				1200	
C10H	3	0		1000				0	
O600	2	0		600				0	
GT2H	1	0		192				0	
VHYD	5	2		0				0	
VPST	6	2		0				0	
CONFIGURATION FOR YEAR 1986 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTFTN	PLQL
N600	0	0		600	114219	244245	C	3411034	0.0008
N10H	0	0		1000				0	
C300	3	4		300				1200	
3600	3	1		600				600	
C10H	3	0		1000				0	
O600	2	0		600				0	
GT2H	1	0		192				0	
VHYD	5	2		0				0	
VPST	6	2		0				0	
CONFIGURATION FOR YEAR 1985 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTFTN	PLQL
N600	0	0		600	374167	231933	C	3052569	0.0002
N10H	0	0		1000				0	
C300	3	4		300				1200	
3600	3	1		600				600	
C10H	3	0		1000				0	
O600	2	0		600				0	
GT2H	1	0		192				0	
VHYD	5	1		0				0	
VPST	6	1		0				0	
CONFIGURATION FOR YEAR 1984 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTFTN	PLQL
N600	0	0		600	230306	237876	C	2446468	0.0002
N10H	0	0		1000				0	
C300	3	4		300				1200	
3600	3	0		600				0	
C10H	3	0		1000				0	
O600	2	0		600				0	
GT2H	1	0		192				0	
VHYD	5	0		0				0	
VPST	6	0		0				0	
CONFIGURATION FOR YEAR 1983 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTFTN	PLQL
N600	0	0		600	118700	228982	C	1978286	0.0002
N10H	0	0		1000				0	
C300	3	4		300				1200	
3600	3	0		600				0	
C10H	3	0		1000				0	
O600	2	0		600				0	
GT2H	1	0		192				0	
VHYD	5	0		0				0	
VPST	6	0		0				0	
CONFIGURATION FOR YEAR 1982 INDEX					PWCONCST	PWOPCST	PWSALVAL	OBJTFTN	PLQL
N600	0	0		600	255931	234405	C	1630602	0.0001
N10H	0	0		1000				0	

C10H	0	1000	0
O600	0	600	0
CT2H	0	192	0
VHYD	6	0	0
VPST	0	0	0

PWCONCST	PWOPCST	PMSALVAL	OBJTVFTN	PLDL
316392	227010	C	1140266	0.0002

CONFIGURATION FOR YEAR 1981 INDEX 3

N500	0	600	0
N10H	0	1000	0
C300	1	300	300
C600	0	600	0
C10H	0	1000	0
O600	0	600	0
CT2H	0	192	0
VHYD	6	0	0
VPST	0	0	0

PWCONCST	PWOPCST	PMSALVAL	OBJTVFTN	PLDL
163285	248807	C	596863	0.0002

CONFIGURATION FOR YEAR 1980 INDEX 2

N500	0	600	0
N10H	0	1000	0
C300	0	300	0
C600	0	600	0
C10H	0	1000	0
O600	0	600	0
CT2H	0	192	0
VHYD	6	0	0
VPST	0	0	0

PWCONCST	PWOPCST	PMSALVAL	OBJTVFTN	PLDL
0	184770	0	184770	0.0000

1980	0	0	0	0	0	0	0
1981	0	1	0	0	0	0	0
1982	0	2	0	0	0	1	0
1983	0	4	0	0	0	1	0
1984	0	4	0	0	0	2	0
1985	0	4	1	0	0	2	1
1986	0	4	1	0	0	2	2
1987	0	4	2	0	0	2	2
1988	0	4	5	0	0	2	2
1989	0	4	7	0	0	2	2
1990	0	4	7	0	0	2	3
1991	0	4	7	0	0	2	3
1992	0	4	7	0	0	2	3
1993	0	4	7	0	0	2	3
1994	0	4	7	0	0	2	3
1995	0	4	7	0	0	2	3

ALL POSSIBLE PATHS TRACED



## APPENDIX E

### On-Site Test of Modified WASP-2B

On-site technical assistance was provided to the FPSC during the week of May 14, 1979.

The NRRI representative worked with project coordinator from FPSC's engineering department and scientific programmer from the computer applications department. The following is a brief description of the on-site technical assistance provided by NRRI.

#### Monday, May 14, 1979

All WASP modifications were outlined to FPSC's staff. The basic functions of each module of the WASP package were identified and the major effects of the modifications were briefly analyzed.

The work schedule suggested by the NRRI representative for his stay at FPSC was discussed. Arrangements were made to assure accessibility of computer facilities all times the FPSC computer was on-line.

Mounting the WASP tape and loading the card-decks on disk required a visit to the Florida State University's central computer terminal. The WASP modules were then copied from the tape on disk so that they could be more easily accessible.

An attempt to compile the VARSYS module showed that IBM and CDC Fortran compilers were slightly different. Some minor modifications of the source statements were necessary in order to compile VARSYS on the CDC computer. The same changes were subsequently performed on all programs transformed to FPSC. VARSYS test runs proved successful.

Tuesday, May 15, 1979

FIXSYS and LOADSY modifications were presented to FPSC's staffs. The LOADSY module was analyzed in detail and the modified fortran statements were explained. Data preparation procedures were outlined and sample test data were analyzed.

FIXSYS and LOADSY modules were compiled after the necessary source modifications. Test runs with sample data were successful.

Wednesday, May 16, 1979

A source listing of NATURE and CATCH22\* programs showed that several character changes were necessary before compilation. These character differences appeared only in programs transferred by card decks and not in those transferred by tape. This occurred because the tape was written after the IBM's EBCPIC character system was translated to BCD system for use by the CDC computer.

CATCH22 was successfully run and binary file LOADDATA (created by LOADSY through logical unit 22) was retrieved and listed. Careful examination of the file's contents showed no flaws in the piecewise representation of the inverted load duration curve.

MATURE program was run successfully with test data.

Thursday, May 17, 1979

The modifications made in CONGEN were analyzed. Sample data were presented. The program was compiled and run successfully after the necessary source character changes.

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\* CATCH22 is an auxiliary program that is used to retrieve binary files LOADDATA or FIXELDC for debugging purposes.

PWCONGEN was expounded to FPSC's staff. Subroutines PWLOLP, PWADD and function PWFUN were analyzed and detailed fortran programming information was provided. Data compilation procedures were explained and sample data analyzed. The proper method of using PWCONGEN in conjunction with MATURE was emphasized.

The necessary changes of source characters were made before successfully compiling PWCONGEN. Running procedures were established and the results from the test runs were checked for errors and analyzed in detail.

Since the CDC's single precision accuracy is compatible to IBM's double precision, it was decided to change all double-precision variables to single precision. This required extensive source changes in the LOADSY and PWCONGEN modules. Both modules were then compiled and the test runs showed no accuracy differences in LOLP calculations. Hence, the same changes were performed in MERSIM and DYNPRO sources.

Friday, May 18, 1979

MERSIM and DYNPRO modifications were explained and data compilation procedures were analyzed. The DYNPRO depreciation algorithm was extensively discussed in both the salvage value and fixed change rate options. The proper running procedures were presented.

Compilation and test runs of MERSIM and DYNPRO modules were successful. The results were analyzed and properly interpreted.

The results of the test runs of all modified WASP modules were checked again and compared to those obtained at OSU. The changes from double to single precision in LOADSY and PWCONGEN did not affect the accuracy of loss-of-load probability calculations as was expected.

The test runs were also compared to those listed in the WASP procedures manual. The comparison showed no inconsistencies.

Saturday, May, 19, 1979

NRRI and FPSC's staffs met to discuss the modified WASP applicability in rate cases and power pooling studies. The NRRI representative extensively analyzed the proper procedures for data compilation for both of the above cases. Supplemental instructions were provided for the use of two auxiliary load forecasting models that FPSC had acquired and intends to use for load forecasting.

Several suggestions were made by FPSC staffs for further minor modifications of WASP. These were later implemented and are included in a tape that will be sent to FPSC along with the final report. After lengthy discussion on DYNPRO depreciation algorithm, it was agreed that although the currently available options (salvage value or fixed charge rate) are reasonably accurate, further research is needed in this subject in order to increase the efficiency of calculations.